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P seismograms from explosions in the S Pacific recorded at four arrays

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SUMMARY

The report presents short period, broad band and deconvolved P seismograms from 108 known or presumed underground explosions that took place during the period 1975-1989 at Tuamotu in the S Pacific. The explosions were fired at two sites separated by 50 kms: Mururoa atoll (where the majority of the tests took place) and Fangataufa. The recordings used are short period seismograms at four arrays: Yellowknife, Canada (YKA); Eskdalemuir, Scotland (EKA); Warramunga, Australia (WRA); and Gauribidanur, India (GBA). The broad band and deconvolved seismograms are derived from the short period; the deconvolved seismograms being broad band seismograms corrected for attenuation. The nearest of the four arrays (WRA) is at a distance of about 80° and two of the arrays (EKA and GBA) lie in the PKP range. Most of the data is from YKA, WRA and GBA.

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The detection thresholds for Tuamotu explosions reported in the Bulletin of the International Seismological Centre (ISC) is $\approx m_b 4.5$. The detection threshold for the arrays is below the ISC threshold and many of the presumed explosions are not reported in the Bulletins but are detected by the arrays.

As well as the seismograms the report lists estimates of various characteristics of the initial P pulse such as the long term level of the reduced displacement potential (ψ_{∞}), duration and rise time, and various measures of explosion size including conventional magnitude m_b and rms signal amplitudes in several time windows. The correlation of these observations with m_b^{ML} is investigated; m_b^{ML} being the maximum likelihood magnitude of the explosions derived from the amplitude and period observations given in the ISC bulletins. m_b^{ML} is taken to be the best estimate of explosion size.

The most striking features shown by the seismograms presented here is that whereas those for Mururoa explosions recorded at YKA and those from the Fangataufa explosions are relatively simple, the seismograms from Mururoa explosions recorded at WRA and GBA are complex. The complexity appears to be due to a reduction in the amplitude of the first arrival at WRA and GBA rather than an increase in the coda amplitude. It seems clear that near source effects are responsible for the reduction in the first arrival at WRA and GBA. For WRA seismograms for Mururoa explosions for example, the apparent pP (A_{pP}) is poorly developed whereas A_{pP} is identifiable on almost all YKA seismograms. On WRA seismograms for Fangataufa explosions A_{pP} is clearly seen. It may also be significant that at least 4 of the 5 explosions at Fangataufa appear to have been fired at a greater depth (A_{pP} -P time, 0.8s) than those at Mururoa (A_{pP} -P time, 0.4-0.6s). However, at this stage it is not possible to give a convincing explanation of the variations in complexity.

The main conclusions come from the analysis of the YKA and WRA observations. These are given below.

(i) The lines relating ψ_{∞} and m_b^{ML} for YKA and WRA observations have slopes close to 1.0 implying that m_b^{ML} is a measure of amplitude at or below the corner frequency of the source pulse.

(ii) The predominant period of the initial arrival on the SP seismograms - particularly the unfiltered version - increases slowly with m_b^{ML} from about 0.8 to 1.0s presumably due to a decrease in the corner frequency of the source pulse with magnitude.

(iii) The measures of source size $(\log A_o, \log A, \log A/T \text{ and rms amplitudes})$ are highly correlated with m_b^{ML} . (A_o is the ½ peak-to-peak amplitude as read from the seismogram and A the amplitude corrected for the gain at period T of a system with a gain of unity at 1 Hz). However, apart from logA, the slope of the lines relating observation to m_b^{ML} are usually significantly less than 1.0. The departure of the slope from 1.0 is due to the lack of a correction to A_o and rms amplitudes to allow for changes in period with m_b^{ML} and over-correction for period when using logA/T to compute magnitude. With A allowance is made for departures in T from 1 Hz.

(iv) The variance of the rms observations against m_b^{ML} are similar to and often less than the variance of station magnitudes. This is particularly true for WRA where the seismograms are more complex than those for YKA. The results suggest that at least as a measure of the relative size of explosions, rms amplitudes might give estimates with smaller variance than conventional magnitudes.

1. INTRODUCTION

Since 1968 France has carried out nuclear tests in the Tuamotu Archipelago in the South Pacific at two sites separated by about 50 kms: Mururoa atoll (where the majority of the tests took place) and Fangataufa. The early tests were in the atmosphere but since 1975 all tests have been underground. In this report we present array recordings of the P waves from some of the underground explosions at Tuamotu. The arrays are at Yellowknife, Canada (YKA); Eskdalemuir, Scotland (EKA); Warramunga, Australia (WRA) and Gauribidanur, India (GBA).

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The report is one of a series that present array seismograms recorded from explosions at the main test sites. The main purpose of the report is to provide a catalogue of the short period (SP) seismograms together with broad band (BB) and deconvolved seismograms derived from the SP; the deconvolved seismograms being BB seismograms corrected for attenuation. It is hoped that such seismograms will help in characterising the explosion source and in understanding how explosions generate seismic waves. The SP, BB and deconvolved seismograms and the measurements made on them are given in appendices. The main text describes the processing of the data and the principal characteristics of the seismograms and gives the results of some analyses of the measurements.

2. <u>THE TUAMOTU TEST SITES</u>

The Tuamotu test sites are remote from most of the world's seismological stations: there are few stations in the teleseismic zone at distances of less than 60°. Figure 1 is a map showing the position of the arrays relative to the test site. The detection thresholds for Tuamotu explosions reported in the Bulletin of the International Seismological Centre (ISC) is $\approx m_b 4.5$, where m_b is body wave magnitude. The detection threshold for the arrays is below the ISC threshold and many signals have been recorded from presumed explosions of low magnitude at the test sites that are not reported in the Bulletins.

The archipelago has little or no natural seismic activity so that any seismic disturbance in the area must be treated as a possible explosion. Positive identification of the disturbances as explosions is difficult using the ratio of m_b to surface wave magnitude, M_s - usually the most reliable identification criterion. The surface waves are only detected from the largest yield explosions. However, T phases recorded at the seismic station at Rarotonga from known explosions at Tuamotu have a characteristic form. The detection of such a T phase from a disturbance at Tuamotu can thus be used to identify the source as an explosion. In recent years France has announced many of the explosions.

Data are presented here from 108 known or presumed underground explosions at Tuamotu that occurred during the period 1975-1989. Douglas et al [1] give estimates of the relative locations of the 71 underground explosions reported by the ISC. The results presented by Douglas et al [1] (Figure 2) show that only three of the explosions took place at Fangataufa. Of the 37 known or presumed explosions not reported by the ISC there is no travel time data that can be used to determine whether the explosions were at Mururoa or Fangataufa. However, newspaper and other reports [2,3] state that two of the 37, which were the first two underground tests at Tuamotu (5 June and 26 November, 1975), were fired at Fangataufa. Inspections of the seismograms presented in this report support this view (see later). For the other presumed explosions not reported by the ISC what evidence there is suggests they were fired at Mururoa and this is assumed to be so in what follows. Table 1 lists the explosions by test site (Mururoa or Fangataufa) and shows the arrays which recorded each explosion. Also given for the explosions reported by the ISC are the bodywave magnitude (m_b) taken from the bulletin and the maximum-likelihood magnitude (m_{b}^{ML}) estimated by Douglas et al [1]. In this report m^{ML}_b is taken to be the best estimate of explosion size. The average distances, azimuths and backbearing of the arrays from Mururoa and Fangataufa are given in Tables 2 & 3 respectively. The nearest of the four arrays (WRA) is at a distance of about 80° and two of the arrays (EKA and GBA) lie in the PKP range. Most of the data comes from YKA, WRA and GBA.

The shallow geological structure of Mururoa is roughly that of a layer over a half space (Crusem [4]). The layer thickness varies from 1.9-2.4 kms and the P-wave speed in the layer from 3.3-3.8 km s⁻¹. The P-wave speed in the half space is 5.05-5.25 km s⁻¹. Evidence from refraction surveys in the area show the crust to be about 30 kms thick and the P_n wave speed to be 8.1 km s⁻¹ (Talandier & Okal [5]). No information is available on the structure of Fangataufa but as it is an atoll it has presumably a similar structure to that of Mururoa.

3. DATA AND PROCESSING METHODS

The data used here are SP array recordings. Figure 3 shows the layout of the arrays. All the arrays have 19 or 20 vertical-component Willmore Mk II seismometers in two lines which are roughly at right angles. Recording at the arrays was initially on analogue tape but over the period 1976-1989 each array in turn has been converted to digital recording. The sampling rate of both the digitally recorded and digitised analogue data is 20 samples per second. The frequency response of the SP recording system of one array (YKA) is shown in Figure 4. The responses of the other arrays differ slightly from the response shown but these differences and variations in the system gain have been taken into account in the processing.

The main processing carried out is the derivation of BB and deconvolved seismograms. When SP array recordings are available the P signals for each seismometer channel are time shifted to correct for the travel time of the signal across the array and the channels are summed. The BB seismogram is obtained by multiplying the spectrum of the array sum by $a_2(\omega)/a_1(\omega)$ and transforming back to the time domain. $a_1(\omega)$ and $a_2(\omega)$ are the responses at frequency ω of the SP and BB instruments respectively. In addition to the instrument conversion each seismogram is filtered to attenuate noise outside the pass band of the instrument. The seismogram is also filtered using a single channel Wiener filter designed by making some simple assumptions about the signal, and using the noise preceding the signal as the noise model.

The deconvolved seismogram is obtained by dividing the spectrum of the BB seismogram by the spectrum of the attenuation operator of Carpenter [6] before transforming into the time domain. The amplitude spectrum of the operator has the form $exp(-\omega t^*/2)$ and the phase spectrum is specified using the theory of Futterman [7]. t* is the ratio of travel time to the specific quality factor Q. To carry out the deconvolution requires an estimate of t*. Douglas et al [8] argue that t* is around 0.35s for the Mururoa-YKA path and this value is also used for the paths to WRA and GBA. Figure 5 shows an example of the output (analysis sheet) from the analysis of each observed seismogram. The figure shows the array sum, the BB seismogram and the deconvolved seismogram for the explosion of 25 May 1988 recorded at YKA. Also shown are two filtered versions of the SP seismogram; one version being filtered in the 0.5-4 Hz band, the other in the 1.0-4.0 Hz band. The additional filtering is applied to improve the signal-to-noise ratio and so it is hoped reduce the errors in the observations; the predominant noise having frequencies below 1 Hz.

Appendices A and B show SP, BB and deconvolved seismograms for all the available recordings of the Tuamotu explosions at the four arrays. Observations from these seismograms are listed in Appendices C and D. The observations from the unfiltered and filtered SP seismograms are principally half peak-to-peak amplitude, period, and rms amplitudes. The amplitudes and periods are used to compute magnitudes. The rms amplitudes are used to investigate the relationship between such amplitudes and body wave magnitudes (see section 5). Appendices E & F show the analysis sheets for all the observed seismograms.

The observations from the unfiltered SP seismograms are $A_o \& T$; A_o being half the range between the first negative deflection (for a system with a gain of unity at 1 Hz) and the succeeding positive deflection and T the corresponding period (see Figure 5). The position where $A_o \& T$) is read is picked by the analyst. Amplitudes and periods of the signals are also measured on the two filtered versions of the SP seismograms together with measurements of the rms amplitudes in seven time windows (0-3s, 0-6s, 0-9s, 0-15s, 3-9s, 3-15s and 9-18s, where time zero is the onset of the signal). The rms amplitude of the noise preceding the signal is also measured. All the measurements on the filtered SP seismograms are made automatically without analyst intervention. The value of A_o measured is half the maximum peak-to-peak amplitude within the first three seconds after the onset of the signal. Station magnitudes are computed from A_o , A & A/T; where A is $A_o/g(T)$ and g(T) is the gain of the recording system at period T. All the magnitudes are computed using the amplitude-distance curve of Lilwall [9] which covers the distance range 20-180°. This allows magnitudes to be computed for GBA and EKA which lie at PKP distances.

No measurements are made from the deconvolved seismograms for EKA and GBA. The EKA seismograms have too low a signal-to-noise ratio to give useful results and those from GBA show multiple arrivals, at least one of which appears to have been Hilbert transformed (which is not unexpected) on the path from source to receiver and this makes reliable measurements difficult to obtain. The measurements made from the deconvolved YKA and WRA seismograms are: the area under the initial positive pulse; the rise and fall times of the pulse; and the duration of the pulse. If an apparent surface reflection (A_{pP}) can be identified the A_{pP} -P time is also estimated; the time used being that between maximum positive deflection of the P pulse

and maximum negative deflection of A_{pP} . The rise time is defined following Gladwin & Stacey [10] as $u_{max}/(du/dt_{max})$, where u_{max} is the maximum amplitude of the initial pulse and $(du/dt)_{max}$ is the maximum gradient of the leading edge of P. Fall-time is measured in a similar way on the trailing edge of the P pulse (see Figure 5). From the area (H) of the P pulse it is possible to estimate ψ_{∞} and the seismic moment of the explosion. Thus ψ_{∞} is given by

$$\psi_{\infty} = \{2KG(\Delta)\}^{-1} H$$

where $G(\Delta)$ corrects for loss of amplitude due to geometrical spreading on the path between test-site and station. The values for $G(\Delta)$ listed by Carpenter [11] are used here. K allows for loss of amplitude at discontinuities in the crust at source and at the receiver and for the effects of differences between the acoustic impedence at the source and receiver. The moment M_0 is given by

$$M_0 = 4\pi\rho\alpha^2\psi_\infty$$

where ρ and α are respectively the density and P wave speed in the firing medium. More details on the computation of ψ_{∞} and M_o are given in Appendix C.

4. <u>THE SEISMOGRAMS</u>

Figure 6 shows the SP and deconvolved P seismograms for two explosions at Mururoa and two at Fangataufa as recorded at the three stations YKA, WRA and GBA. Most of the signals are too weak to be recorded above noise at EKA: a few signals are detected but these have very low signal-to-noise ratio and are considered later. At all stations other phases in addition to P are predicted to arrive within about 10s of signal onset. These phases and their relative arrival times are listed in Table 4 and the predicted times are indicated in Figure 6. (The travel times assumed throughout this report are as predicted by the IASPEI 1991 Seismological Tables, Kennett [12]).

Inspection of the seismograms shows clear variation with station and test site. The YKA seismograms for the two test sites though differing in detail are typical simple explosion seismograms. The core reflected phase PcP is expected to arrive just over two seconds after onset but none of the YKA seismograms in Figure 6 show clear evidence of any such arrival. A few YKA seismograms (see for example those of the explosions of 8 December 1981, 19 April 1983 and 31 October 1989, Appendix A) do show a prominent arrival within 4 seconds of the P onset which has about the right arrival time to be PcP. However, further evidence is required before the arrival can be accepted as being PcP. In particular it remains to be explained why the observed arrival is so clear on some YKA seismograms and absent on others.

The deconvolved YKA seismograms show P and an apparent pP (A_{pP}) with A_{pP} -P time for the Mururoa explosions of about 0.5s and for the Fangataufa explosions about 0.8s. This difference in the A_{pP} -P time between explosions at the two test sites produces an observable difference in the SP seismograms. For the Fangataufa explosions the P pulse is complete before the onset of A_{pP} and this results in an inflexion on the second positive deflection of the SP seismogram. For the Mururoa explosions the trailing edge of P and the leading edge of A_{pP} merge so that the pulses interfere constructively around 1 Hz and there is no inflexion. The effect of the difference on the way P and A_{pP} interfere is to enhance the maximum peak-to-peak amplitude of the SP seismograms for Mururoa explosions relative to those for the Fangataufa explosions. This shows up in the ratio of the first motion to peak-to-peak amplitude which is 0.15 or less for the Mururoa explosions whereas for the Fangataufa explosions the ratio is greater than 0.25.

Whereas the YKA seismograms of Mururoa and Fangataufa explosions are similar, with the main differences arising because of the differences in the A_{pP} -P time for the two test sites, the seismograms recorded at WRA from the two sites are strikingly different (Figure 6). Thus the Fangataufa seismograms usually show P & A_{pP} and have a coda that falls-off in roughly the same way as those for YKA but the WRA seismograms for Mururoa are significantly more complex than those of YKA and show no clear evidence of A_{pP} . Note that it is not that the absolute amplitude of the WRA coda is large that makes the WRA seismograms for Mururoa explosions complex - the YKA coda amplitudes are in fact larger than at WRA - but that the first arrival is small. This is illustrated in Figure 7 which shows a comparison of station magnitudes, coda rms and ψ_{∞} for the two stations. Figure 7a shows the YKA and WRA magnitudes against m_b^{ML} and Figure 7b the YKA and WRA rms amplitudes for the 3-15s window against m_b^{ML} . (0.05 has been subtracted from the log of the WRA rms amplitudes to allow for differences in the distance correction factors for YKA and WRA).

From the Mururoa explosions it is clear that whereas the rms amplitude of the coda for the two stations differ by about a factor of 2 the YKA station magnitudes are almost one unit larger than those at WRA. For ψ_{∞} (Figure 7c) the YKA estimates are only about 3 times larger than those for WRA.

The explosions of 30 November 1988 and 10 June 1989 shown in Figure 6 are known to have been fired at Fangataufa because the estimated epicentres fall close to the island. The two explosions of 1975 (5 June and 26 November) are also reported [2,3] to have been fired at Fangataufa. This is consistent for the 26 November 1975 explosion with the evidence that WRA seismograms of Mururoa and Fangataufa explosions are significantly different (Figure 6). (There is no WRA seismogram for the 5 June 1975 explosion). Thus the WRA seismograms for the 27 November 1975 explosion (Appendix B) is both simple and has a maximum amplitude that is only about a factor of 2 less than that at YKA which is typical of Fangataufa explosions. Had the explosion been fired at Mururoa the WRA seismogram would be expected to be complex and have an amplitude at least a factor of 4 less than that observed at YKA.

GBA lies very near the PKP focus. Travel time tables predict (Table 4) there will be a series of arrivals with very similar onset times. Inspection of the GBA seismograms from the Fangataufa explosions (Figure 6) shows that there are indeed several arrivals. Taking the first arrival to be $PKP_{BC} + PKP_{AB}$ two of the later arrivals coincide roughly with the predicted times of PKP_{DF} and PKiKP. Further, the onset of the signal does not show the typical first motion of explosion seismograms: although first motion on the SP does appear to be positive it is of low amplitude and emergent. This is to be expected if PKP_{AB} predominates as the first arrival because this is a mini-max phase and should approximate to the Hilbert transform of the P phase. This produces an emergent onset.

The seismograms from the Mururoa explosions recorded at GBA (Figure 6) are more complex than those from the Fangataufa explosions. Following the first arrival, which is predicted to be PKP_{DF} , several arrivals are observed. One of these arrivals usually coincides roughly with the calculated time for PKiKPwhich is the only other phase predicted from travel time tables. Comparison of the seismograms with those from WRA suggests that in fact the prominence at GBA of many arrivals in the coda not predicted by tables is again due to the first arrival being weak rather than the coda arrivals being strong. This is supported by Figure 7 where YKA and GBA magnitudes and rms amplitudes (3-15s window) are plotted against m_b^{ML} . (0.21 has been subtracted from the log of the GBA rms amplitudes to allow for differences in the distance correction factor for YKA and GBA.) Thus the GBA magnitudes are one unit lower than at YKA whereas the rms amplitudes differ by a factor of only about 3. These differences for WRA and YKA. Similarity in the complexity of the GBA seismograms to the WRA seismograms is perhaps to be expected as the rays to the two stations take-off in similar directions, there being only 10° difference in the azimuths to the two stations.

As with the GBA recordings from the Fangataufa explosions the recordings from the Mururoa explosions have a relatively low amplitude, emergent first motion suggesting that the first arrival at Mururoa is a minimax phase. However, it is only arrivals from the PKP_{AB} branch that are expected to be mini-max phases and this branch is only predicted to exist for ranges of 144.55° and beyond, which is just slightly greater than the GBA-Mururoa distance but less than the GBA-Fangataufa distance. Thus if the first arrival at GBA from Mururoa explosions is PKP_{AB} and not PKP_{DF} the travel time tables for this distance range are incorrect. The observations of Tuamotu explosions at GBA provide important data to enable the tables to be corrected. However, detailed study is needed to disentangle the various PKP branches. Such a study is outside the scope of this report.

Figure 8 shows 7 of the clearest detections at EKA of Mururoa explosions - these are SP array beams. There seems to be no doubt that the signals are seen but the signal-to-noise is poor. Summing the signals (top trace) confirms the presence of the signals showing the typical explosion shape but with low predominant frequency suggesting that high frequencies have been lost from the signal either through scattering or anelastic attenuation.

5. <u>ANALYSIS OF OBSERVATIONS</u>

Figures 9-14 show the various measurements made from the YKA seismograms of the Mururoa explosions plotted against m_b^{ML} . Figures 15-20 and 21-25 show the results for WRA and GBA respectively.

The lines through the data are least squares lines estimated assuming that there is no error in m_b^{ML} . In general the YKA observations are less scattered than those for WRA and GBA presumably because the YKA seismograms have higher signal-to-noise ratios and are simpler than the corresponding WRA and GBA seismograms. (No graphs are shown of the measurements from the Fangataufa explosions as the number of explosions at that site is too small.)

The durations, rise times and fall times at YKA and WRA all increase with m_b^{ML} but the correlation coefficients are not all significant at the 5% level. Comparison of the rise times shows that although the results for WRA are more scattered than at YKA, on average there is little difference between the two stations. The durations of the pulses do appear to differ with station: the average duration for WRA is around 0.9s whereas that for YKA is around 0.6s. Further, the fall times at WRA are greater than those at YKA. These differences can be understood if the effect of A_{pP} is taken into account. At YKA A_{pP} is identifiable on almost all the seismograms whereas at WRA A_{pP} is usually absent. Also the measured A_{pP} -P time for YKA is very similar to the apparent pulse duration. Thus it appears that the P pulse of YKA is truncated by the arrival of A_{pP} so the apparent pulse duration is reduced relative to the pulses observed at WRA. The pulse observed at WRA is thus a better estimate of P than that at YKA. The interference of P & A_{pP} at YKA apparently produces a P pulse with a sharper trailing edge than the WRA pulse, ie the apparent fall time of the YKA P is shorter than the true fall time.

The least squares lines relating the estimates of source size to m_b^{ML} have slopes in the range 0.60-1.15. For ψ_{∞} against m_b^{ML} the slope of the line relating the two variables is close to 1.0 (Figure 9a). This implies that m_b^{ML} is measuring the amplitude at a roughly constant period and that this period is at or below the corner frequency of the explosion source. As most of the observations contributing to m_b^{ML} probably come from very narrow band SP systems the suggestion that there is little variation in T with magnitude is plausible: that is m_b^{ML} is proportional to amplitude A, with T, being independent of magnitude, having no effect on the slope of the least squares line.

For the YKA SP observations T increases with m_b^{ML} (Figure 10a) consequently the station magnitude for YKA which depends on log(A/T) has a slope (0.86) that is significantly less than 1.0. This is confirmed if magnitude is computed using logA (Figure 11a) when the slope of the line (0.93) is now close to 1.0. Similar effects are seen for the WRA observations (Figure 16a) although the results are more scattered and in fact the slope of WRA station magnitude (Figure 16b) against m_b^{ML} is not significantly different from 1.0. For GBA on the other hand the slope of the least squares line relating station magnitude to m_b^{ML} (Figure 21b) is significantly less than 1.0 and T appears to be independent of m_b^{ML} (Figure 21a). At around $m_b^{ML4.5}$ the observed period of about 0.8s is similar to that observed at YKA and WRA but whereas at the latter two stations period increases to around 1.0 at $m_b^{ML6.0}$, the period for GBA remains constant at around 0.8s. It might be possible to account for the lack of variation in period at GBA by source effects. However, one significant difference between the GBA seismograms and those from YKA and WRA is that the main arrival on the GBA seismograms has probably been Hilbert transformed on propagation from source to receiver and it may be that the effect of this is to make the observed period appear more uniform. An investigation of the effect of Hilbert transformation on the measured period is being carried out and will be reported elsewhere.

Turning now to the station magnitudes measured on the band-pass filtered seismograms. On the unfiltered YKA and WRA seismograms the average period at around $m_b^{ML}4.5$ is 0.8s whereas that at $m_b^{ML}6.0$ is about 1.0 Hz. The effect of the additional filtering is to attenuate those signals with the largest predominant period and to make the observed period over the range $m_b^{ML}4.5-6.0$ more nearly constant. The result of this is that station magnitudes calculated from the filtered seismograms (Figures 10d & f and 16d & f) increase more slowly with m_b^{ML} than do the magnitudes estimated from the unfiltered seismograms. (The effect for the GBA seismograms where the period on the unfiltered versions is almost uniform is to produce apparently, a slight decrease in period with magnitude although the estimated slope of the period-magnitude lines are not significantly different from zero). The results for YKA and WRA suggest that the corner frequency varies from just above 1 Hz at $m_b^{ML}4.5$ to just below at $m_b^{ML}6.0$ and the effect of band pass filtering is to confine the measurements to a pass band above the corner.

For the explosions not reported in the ISC no estimate of m_b^{ML} is available. However, an estimate of m_b^{ML} can be obtained for these explosions if they have been recorded at YKA by using the relationship between the station and maximum likelihood magnitudes. Estimates of m_b^{ML} derived in this way, m_b^{ML} (YKA), are listed in Table 1. For the explosions at Mururoa the m_b^{ML} (YKA) estimates were obtained using the relation between

 m_b^{ML} and the YKA m_b given in Figure 10b. For the Fangataufa explosion m_b^{ML} (YKA) is calculated by subtracting 0.04 from the YKA m_b ; 0.04 being the average difference between m_b^{ML} and the station m_b for the three Fangataufa explosions recorded by YKA and reported in the ISC bulletins. The results suggest that the detection threshold for YKA for Mururoa explosions is below m_b^{ML} 3.5.

The rms observations are all highly correlated with m_b^{ML} . The slopes of the least squares lines are similar to those relating station magnitudes measured on the filtered SP seismograms to m_b^{ML} but often the scatter of the observations about the least squares line is less for the rms observations than for the magnitudes. This is particularly true for WRA where the variance of magnitude observations is 2-3 times that of the rms observations.

6. <u>DISCUSSION</u>

All the deconvolved seismograms have been derived on the assumption that the value of t* (0.35s) suggested by Douglas et al [8] for the Mururoa-YKA path applies to the other paths studied. From the results presented here at least for paths to YKA and WRA there is no evidence that t* for paths to these two stations are widely different. The rise times on the deconvolved seismograms are similar for both stations for example. It seems unlikely then that the large differences in the station magnitudes of YKA and WRA for Mururoa explosions can be attributed to differences in anelastic attenuation on the paths to these stations. If the anelastic attenuation on the path to WRA were greater than on the path to YKA the region of high attenuation would have to be very localised; on the paths from Mururoa and Fangataufa to WRA, GBA and YKA the only paths that can cross the region are those from Mururoa to WRA and GBA.

Ignoring the amplitudes it would appear from inspection of the SP seismograms that if anything the WRA recordings of Tuamotu explosions show higher predominant frequencies than YKA recordings. This is particularly true for the Fangataufa explosions recorded at WRA and YKA (Figure 6).

The rms (3-15s) amplitudes and the station magnitudes of the Fangataufa explosions suggests that the differences in the WRA and YKA station magnitudes for Mururoa (and Fangataufa) explosions in the absence of near source effects is about a factor of 2. The ψ_{∞} observations for WRA and YKA show that the total differences for the P pulse between the two paths is a factor of 3 which suggests that because of near source effects the P pulse radiated to WRA is about a factor of 1.5 smaller than that radiated to YKA. The large differences in WRA and YKA station magnitudes for Mururoa explosions (equivalent to a factor of about 6 in amplitude) can thus be roughly accounted for by a difference of a factor of 1.5 in the amplitude of the radiated P pulse, a factor of 2 for differences in path effects and a factor of 2 from the absence of A_{pP} at WRA. What the mechanisms are that result in the P pulse radiated to WRA having on average two thirds the amplitude of that radiated to YKA and the lack of A_{pP} is not clear and remains to be investigated.

7. <u>CONCLUSIONS</u>

The most striking features shown by the seismograms presented here is that whereas those for Mururoa explosions recorded at YKA and those from the Fangataufa explosions are relatively simple, the seismograms from Mururoa explosions recorded at WRA and GBA from Mururoa explosions are complex. The complexity appears to be due to a reduction in the amplitude of the first arrival at WRA and GBA rather than an increase in the coda amplitude. It seems clear that near source effects are responsible for the reduction in the first arrival at WRA and GBA. For WRA seismograms for Mururoa explosions for example A_{pP} is poorly developed whereas A_{pP} is identifiable on almost all YKA seismograms. On WRA seismograms for Fangataufa explosions A_{pP} is clearly seen. It may also be significant that at least 4 of the 5 explosions at Fangataufa appear to have been fired at a greater depth (A_{pP} -P time, 0.8s) than those at Mururoa (A_{pP} -P time, 0.4-0.6s). However, at this stage it is not possible to give a convincing explanation of the variations in complexity.

Numerous conclusions can be drawn from the analysis of the observations. The main conclusions from the analysis of the observations from the YKA and WRA seismograms are given below.

(i) The lines relating ψ_{∞} and m_b^{ML} for YKA and WRA observations have slopes close to 1.0 implying that m_b^{ML} is a measure of amplitude at or below the corner frequency of the source pulse.

(ii) The predominant period of the initial arrival on the SP seismograms - particularly the

unfiltered versions - increases slowly with m_b^{ML} from about 0.8 to 1.0s presumably due to a decrease in the corner frequency of the source pulse with magnitude;

(iii) The measures of source size (logA_o, logA, logA/T and rms amplitudes) are highly correlated with m_b^{ML} . However, apart from logA, the slope of the lines relating observation to m_b^{ML} are usually significantly less than 1.0. The departure of the slope from 1.0 is due to the lack of a correction to A_o and rms amplitudes to allow for changes in period with m_b^{ML} and over-correction for period when using logA/T to compute magnitude. With A allowance is made for departures in T from 1 Hz.

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(iv) The variance of the rms observations against m_b^{ML} are similar to and often less than the variance of station magnitudes. This is particularly true for WRA where the seismograms are more complex than those for YKA. The results suggest that at least as a measure of the relative size of explosions, rms amplitudes might give estimates with smaller variance than conventional magnitudes.

ACKNOWLEDGEMENTS

We thank the operators of the arrays for their conscientious work over many years, which has produced a large library of high quality recordings from which the seismograms presented here are taken.

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Table 1 Mururoa Explosions

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Date	YKA	EKA	WRA	GBA		m _b (ISC)	n ^{mL}	m ^{ML} (YKA)
770219	*	-	N N	* N	ISC	5.0	4.93	4.83
770319	0	*	Ň	*	ISC	5.8	5,92	0.00
770706	*	-	*	*	ISC	5.2	4.81	4.81
771124	* N	-	N N	*	150	0+0	0.00	4.51
771217	Ň	-	Ň	*	100	0.0	0.00	0.00
780227	*	-	-	-		0.0	0.00	3.48
780322	*	-	*	*	ISC	4.8	4.73	4.66
780726	*	-	-	-		0.0	0.00	4+20
781102	*	-	Ν	¥		0.0	0.00	4.38
781130	õ	*	*	*	ISC	5.8	5.86	0.00
781217	*	-	N *	*	150	4.9	5.01	4.65
790301	*	-	*	*	100	0.0	0.00	4.64
790309	*	-	*	*	_	0.0	0.00	4.69
790324	*	-	*	*	ISC	4.9	4.93	4.90
790404	*	-	*	*	ISC	4.7	4.69	4.66
790629	*	-	*	¥	ISC	5.4	5.21	5.16
790725	õ	*	*	*	ISC	6.0	6.11	0.00
790728	*	-	*	-	150	4.4	4.73	4.58
800223	*	-	*	¥		0.0	0,00	4.11
800303	*	-	*	*		0.0	0,00	4.22
800323	*	-	*	*	ISC	5.7	5.63	5.60
800401	*	-	-	×	ISC	3.1 4.5	4.30	4.37
800616	*	-	*	Ν	ISC	5.4	5.30	5.32
800621	*	-	*	*	100	0.0	0.00	4.53
800705	* N	*	*	- *	130	4.6	4.34	4.51
801203	N	-	*	*	ISC	5.6	5.58	0.00
810227	*	-	*	¥		0.0	0.00	4.20
810306	*	-	*	*	100	0.0	0.00	4.31
810328	*	-	*	÷	ISC	4.8	4.76	4.78
810708	*	-	*	*	ISC	5.3	5.14	5.08
810711	*	-	N	-		0.0	0.00	3.86
810/18	*	-	*	-	150	5.3	5.09	4.20
811111	*	-	*	¥	ISC	4.5	4.71	4.74
811205	¥	-	*	*	ISC	4.6	4.68	4.58
811208	*	-	*	*	ISC	5.2	5-14	4.94
820224	*	_	¥	-		0.0	0.00	3.59
820320	*	-	¥	*	ISC	4.9	4.96	4.96
820627	*	-	-	-	100	0.0	0.00	3.75
820701	÷	*	Ň	÷	ISC	5.7	5.60	5.58
830419	*	¥	*	¥	ISC	5.6	5,70	5.63
830425	*	-	-	-		0.0	0.00	3,22
830525	N ¥	*	*	*	ISC	5.9	5.87	0.00
830628	*	-	¥	×	ISC	5.4	5.32	5.36
830720	¥	-	¥	-		0.0	0,00	4.44
830804	*	-	*	*	ISC	5.3	5.13	5.06
831203	*	_	*	*	ISC	5.0	4.89	4.85
840508	¥	-	Ν	*		0.0	0.00	4.51
840512	*	*	*	*	ISC	5.7	5.57	5.61
840612	*	-	*	*	150	0.0 5.3	5.28	4.04
841027	*	-	*	-	ISC	4.5	4.49	4,43
841102	*	¥	*	¥	ISC	5.6	5.64	5.49
841201	*	-	-	-	190	0.0	0.00	3.57
850430	*	-	*	-	ISC	4.5	4.51	4.54
850508	*	-	*	*	ISC	5.6	5.64	5.57
850603	*	-	*	*	ISC	5.1	4.83	4.73
851024	*	-	* 	-		0.0	0.00	4.43
851026	*	-	*	¥	ISC	5.3	5.30	5.31
851124	*	-	*	*	ISC	4.7	4.55	4.65
851126	U *	-	*	*	ISC	5.9	5.76	4.43
860506	*	-	*	-	100	0.0	0.00	4.46
860527	*	-	*	-		0.0	0.00	4.62
860530	*	*	*	*	ISC	5.6	5.58	5.60

861112 861206 861210 870505 870520 870606 870621 871023 871105 871129 880511 880525 880616 880105	N*******O****		*******	**********	ISC ISC ISC ISC ISC ISC ISC ISC ISC ISC	50545671548046035 5.5.5.5.5.5.5.5.5.5.5.5.5.5.5.5.5.5.5	5.28 5.25 5.551 5.540 5.540 5.540 5.540 5.540 5.500 5.500 5.500 5.30	0816451
880623	*	Ξ	*	*	ISC ISC	5.3	5.18 5.30	5.35
881123 890511	*	-	* N	N ¥	ISC ISC	5.4	5.29 5.16	5.41 5.21
890520	*	-	Ň	-		0.0	0.00	4.49
890603	*	-	*	*	ISC	5.4	5.37	5.29
891031	*	-	*	*	ÎSC	5.2	5.30	5.16
891120	Ν	-	*	*	ISC	5.3	5.19	0.00

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Fangataufa Explosions

Date 750605 751126 881130 890610	YKA * * *	EKA - - *	WRA N * *	GBA - * * *	ISC ISC	m _b (ISC) 0.0 0.0 5.5 5.5	mb 0.00 0.00 5.58 5.51 5.59	m ^{ML} (YKA) 4.51 4.72 5.62 5.57 5.48
891127	*	*	N	*	ISC	5.6	5.59	5.48

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* Signal detected. - Signal not detected or tape not processed. N No tape available. O Signal overloaded.

Table 2

Epicentral distances, azimuths and backbearings of arrays from Mururoa*

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Distance (°)	Azimuth (°)	Backbearing (°)
86.24	11.0	202.5
133.14	33.1	297.3
79.91	252.5	109.6
144.49	262.8	108.5
	Distance (°) 86.24 133.14 79.91 144.49	Distance (°)Azimuth (°)86.2411.0133.1433.179.91252.5144.49262.8

*Angles measured from centre of Mururoa, taken to be: 21.835°S 138.91°W

Table 3

Epicentral distances, azimuths and backbearings of arrays from Fangataufa*

Station	Distance (°)	Azimuth (°)	Backbearing (°)
YKA	86.6	11.0	202.3
EKA	133.38	33.4	296.8
WRA	79.95	252.6	110.0
GBA	144.60	262.2	109.2

*Angles measured from centre of Fangataufa, taken to be: 22.233S 138.74W

Fangataufa lies 0.43° (47.25 km) from Mururoa on a bearing of 158.3°. The bearing of Fangataufa from Mururoa is 338.3°

TABLE 4

Relative arrival times of P phases for the four arrays

		Time after onset(s)			
Station	Phase	Mururoa	Fangataufa		
YKA	Р	0.0	0.0		
	PcP	2.37	2.19		
EKA	PKP _{DF}	0.0	0.0		
	PKiKP	1.48	1.52		
WRA	Р	0.0	0.0		
	PcP	7.32	7.27		
GBA	PKP _{BC}	Not predicted	0.0		
	PKPAB	Not predicted	0.0		
	PKP	0.0	1.61		
	PKiKP	4.23	5.87		

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The times are as predicted by the IASPEI 1991 Seismological Tables (Kennett [12])

FIGURE CAPTIONS

- Figure 1 Azimuthal-great circle projection of the earth centred on Tuamotu showing the positions of the four arrays.
- Figure 2 Map showing Mururoa and Fangataufa and the estimated epicentres of the 71 underground explosions which were reported by the ISC.
 - (a) Epicentres of the 71 explosions estimated relative to that of 25 July 1979 which is restrained to the position 21.88°S 138.94°W.

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- (b) Epicentres of the three Fangataufa explosions estimated relative to that of the 30 November 1988 which is restrained to the centre of the island (22.233°S 138.74°W).
- Figure 3 Plans of the arrays showing seismometer positions.
- Figure 4 Relative amplitude response of short period and broad band systems.
- Figure 5 Example of the output (analysis sheet) for an observed seismogram. The observed short period (array sum), the filtered short periods, the broad band and the deconvolved seismograms (for t*=0.35s) are shown at the top of the figure. The shaded area on the deconvolved seismogram is used to estimate ψ_{∞} . The insets at the bottom of the figure shows how the rise and fall times of the pulse and A_o and T/2 on the unfiltered SP are measured. The table at the bottom of the figure give the observations made on the seismograms.
- Figure 6 Short period and deconvolved seismograms for two Mururoa and two Fangataufa explosions as recorded at YKA, WRA and GBA.
- Figure 7 Comparison of some WRA and GBA estimates of source size with those for YKA.
 - (a) YKA & WRA station m_b against m_b^{ML} .
 - (b) YKA & WRA rms (3-15s) amplitudes against m_b^{ML} .
 - (c) YKA & WRA ψ_{∞} against m_{b}^{ML} .
 - (d) YKA & GBA station m_b against m_b^{ML} .
 - (e) YKA & GBA rms (3-15s) amplitudes against m_h^{ML} .
- Figure 8 Observed EKA short period seismograms for the 7 Mururoa explosions with the largest signalto-noise ratios at the station. The top trace is the sum of the 7 observed seismograms. For each seismogram the station m_b and m_b^{ML} are given.
- Figure 9 Graphs of various observations taken from the YKA seismograms against maximum likelihood m_b . (a) ψ_{∞} ; (b) Pulse duration; (c) Pulse rise time; (d) Pulse fall time. The lines are least squares estimates obtained assuming no errors in the abscissa. The equations of the lines are given at the top of each figure with 95% confidence limits on the slopes and intercepts. x and y stand for the abscissa and ordinate respectively of the graphs.
- Figure 10 Graphs of various observations taken from the YKA seismograms against maximum-likelihood m_b . (a) Period; (b) Station m_b ; (c) Period (0.5-4.0 Hz); (d) Station m_b (0.5-4.0 Hz); (e) Period (1.0-4.0 Hz); (f) Station m_b (1.0-4.0 Hz).

The lines are least squares estimates obtained assuming there are no errors in the abscissa. The equations of the lines are given at the top of each figure with the 95% confidence limits on the slope and intercepts. x and y stand for the abscissa and ordinate respectively of the graphs.

Figure 11 Graphs of various observations taken from the YKA seismograms against maximum likelihood m_b.

- (a) Station m_h computed using logA rather than logA/T;
- (b) Station m_b computed using logA_o where A_o is the ½ peak-to-peak amplitude for a system with a gain of unity at 1 Hz;
- (c) Station m_b (0.5-4.0 Hz) computed using logA (0.5-4.0 Hz) rather than logA/T (0.5-4.0 Hz);
- (d) Station m_b (0.5-4.0 Hz) computed using logA_o (0.5-4.0 Hz) where A_o (0.5-4.0 Hz) is the $\frac{1}{2}$ peak-to-peak amplitude for a system with unit gain at 1 Hz;
- (e) Station m_b (1.0-4.0 Hz) computed using logA (1.0-4.0 Hz) rather than logA/T (1.0-4.0 Hz);
- (f) Station m_b (1.0-4.0 Hz) computed using logA_o (1.0-4.0 Hz) where A_o (1.0-4.0 Hz) is the $\frac{1}{2}$ peak-to-peak amplitude for a system with unit gain at 1 Hz.

The lines are least squares estimates obtained assuming there are no errors in the abscissa. The equations of the lines are given at the top of each figure with the 95% confidence limits on the slope and intercepts. x and y stand for the abscissa and ordinate respectively of the graphs.

Figure 12 Graphs of YKA rms amplitudes in the 0.5-4 Hz band and a number of time windows, against m_b^{ML} (squares). The time windows are: (a) 0-3s; (b) 0-6s; (c) 0-9s; (d) 0-15s; (e) 3-9s; (f) 3-15s. Time zero is the onset of the signal. The asterisks show the rms noise amplitude measured in a window before signal onset.

The lines are least squares estimates obtained assuming there are no errors in the abscissa. The equations of the lines are given at the top of each figure with the 95% confidence limits on the slope and intercepts. x and y stand for the abscissa and ordinate respectively of the graphs.

Figure 13 Graphs of YKA rms amplitudes in the 1.0-4 Hz band and a number of time windows, against m_b^{ML} (squares). The time windows are: (a) 0-3s; (b) 0-6s; (c) 0-9s; (d) 0-15s; (e) 3-9s; (f) 3-15s. Time zero is the onset of the signal. The asterisks show the rms noise amplitude measured in a window before signal onset.

The lines are least squares estimates obtained assuming there are no errors in the abscissa. The equations of the lines are given at the top of each figure with the 95% confidence limits on the slope and intercepts. x and y stand for the abscissa and ordinate respectively of the graphs. Triangles show where noise observations fall below the bottom of the graph.

Figure 14 Graphs of various observations taken from the YKA seismograms against m^{ML}_b. (a) rms amplitudes 9-18s (0.5-4.0 Hz) (squares); (b) rms amplitudes 9-18s (1.0-4.0 Hz) (squares); (c) pP-P times. The asterisks show the rms noise amplitude measured in a window before signal onset.

The lines are least squares estimates obtained assuming there are no errors in the abscissa. The equations of the lines are given at the top of each figure with the 95% confidence limits on the slope and intercepts. x and y stand for the abscissa and ordinate respectively of the graphs. Triangles show where noise observations fall below the bottom of the graph.

Figure 15 Graphs of various observations taken from the WRA seismograms against m_b^{ML} . (a) ψ_{∞} ; (b) Pulse rise time; (c) Pulse duration; (d) Pulse fall time. The lines are least squares estimates obtained assuming no errors in the abscissa. The equations of the lines are given at the top of each figure with 95% confidence limits on the slopes and intercepts. x and y stand for abscissa and ordinate respectively of the graphs.

Figure 16 Graphs of various observations taken from the WRA seismograms against m_{h}^{ML} . (a) Period; (b) Station m_b; (c) Period (0.5-4.0 Hz); (d) Station m_b (0.5-4.0 Hz); (e) Period (1.0-4.0 Hz); (f) Station m_{b} (1.0-4.0 Hz). The lines are least squares estimates obtained assuming there are no errors in the abscissa. The equations of the lines are given at the top of each figure with the 95% confidence limits on the slope and intercepts. x and y stand for the abscissa and ordinate respectively of the graphs. Figure 17 Graphs of various observations taken from the WRA seismograms against maximum-likelihood m_b. (a) Station m_b computed using logA rather than logA/T; Station m_b computed using logA_o where A_o is the ½ peak-to-peak amplitude for a (b) system with a gain of unity at 1 Hz; (c) Station m_b (0.5-4.0 Hz) computed using logA (0.5-4.0 Hz) rather than logA/T (0.5-4.0 Hz); (d) Station m_b (0.5-4.0 Hz) computed using logA_o (0.5-4.0 Hz) where A_o (0.5-4.0 Hz) is the ½ peak-to-peak amplitude for a system with a gain of unity at 1 Hz; (e) Station m_b (1.0-4.0 Hz) computed using logA (1.0-4.0 Hz) rather than logA/T (1.0-4.0 Hz); Station m_h (1.0-4.0 Hz) computed using logA_o (1.0-4.0 Hz) where A_o (1.0-4.0 Hz) is (f) the ½ peak-to-peak amplitude for a system with unit gain at 1 Hz. The lines are least squares estimates obtained assuming there are no errors in the abscissa. The equations of the lines are given at the top of each figure with the 95% confidence limits on the slope and intercepts. x and y stand for the abscissa and ordinate respectively of the graphs. Figure 18 Graphs of WRA rms amplitudes in the 0.5-4 Hz band and a number of time windows, against m_{h}^{ML} (squares). The time windows are: (a) 0-3s; (b) 0-6s; (c) 0-9s; (d) 0-15s; (e) 3-9s; (f) 3-15s. Time zero is the onset of the signal. The asterisks show the rms noise amplitude measured in a window before signal onset. The lines are least squares estimates obtained assuming there are no errors in the abscissa. The equations of the lines are given at the top of each figure with the 95% confidence limits on the slope and intercepts. x and y stand for the abscissa and ordinate respectively of the graphs. Figure 19 Graphs of WRA rms amplitudes in the 1.0-4 Hz band and a number of time windows, against m_{h}^{ML} (squares). The time windows are: (a) 0-3s; (b) 0-6s; (c) 0-9s; (d) 0-15s; (e) 3-9s; (f) 3-15s. Time zero is the onset of the signal. The asterisks show the rms noise amplitude measured in a window before signal onset. The lines are least squares estimates obtained assuming there are no errors in the abscissa. The equations of the lines are given at the top of each figure with the 95% confidence limits on the slope and intercepts. x and y stand for the abscissa and ordinate respectively of the graphs. Triangles show where noise observations fall below the bottom of the graph. Figure 20 Graphs of various observations taken from the WRA seismograms against $m_{\rm b}^{\rm ML}$. (a) rms amplitudes 9-18s (0.5-4.0 Hz); (b) rms amplitudes 9-18s (1.0-4.0 Hz). The asterisks show the

rms noise amplitude measured in a window before signal onset.

The lines are least squares estimates obtained assuming there are no errors in the abscissa. The equations of the lines are given at the top of each figure with the 95% confidence limits on the slope and intercepts. x and y stand for the abscissa and ordinate respectively of the graphs. Triangles show where noise observations fall below the bottom of the graph.

Figure 21 Graphs of various observations taken from the GBA seismograms against m_b^{ML} . (a) Period; (b) Station m_b ; (c) Period (0.5-4.0 Hz); (d) Station m_b (0.5-4.0 Hz); (e) Period (1.0-4.0 Hz); (f) Station m_b (1.0-4.0 Hz).

The lines are least squares estimates obtained assuming there are no errors in the abscissa. The equations of the lines are given at the top of each figure with the 95% confidence limits on the slope and intercepts. x and y stand for the abscissa and ordinate respectively of the graphs.

Figure 22 Graphs of various observations taken from the GBA seismograms against m_{h}^{ML} .

- (a) Station m_b computed using logA rather than logA/T;
- (b) Station m_b computed using logA_o where A_o is the $\frac{1}{2}$ peak-to-peak amplitude for a system with a gain of unity at 1 Hz;
- (c) Station m_b (0.5-4.0 Hz) computed using logA (0.5-4.0 Hz) rather than logA/T (0.5-4.0 Hz);
- (d) Station m_b (0.5-4.0 Hz) computed using logA_o (0.5-4.0 Hz), where A_o (0.5-4.0 Hz) is the $\frac{1}{2}$ peak-to-peak amplitude for a system with a gain of unity at 1 Hz;
- (e) Station m_b (1.0-4.0 Hz) computed using logA (1.0-4.0 Hz) rather than logA/T (1.0-4.0 Hz);
- (f) Station m_b (1.0-4.0 Hz) computed using logA_o (1.0-4.0 Hz), where A_o (1.0-4.0 Hz) is the $\frac{1}{2}$ peak-to-peak amplitude for a system with unit gain at 1 Hz.

The lines are least squares estimates obtained assuming there are no errors in the abscissa. The equations of the lines are given at the top of each figure with the 95% confidence limits on the slope and intercepts. x and y stand for the abscissa and ordinate respectively of the graphs.

Figure 23 Graphs of GBA rms amplitudes in the 0.5-4 Hz band and a number of time windows, against m_b^{ML} . The time windows are: (a) 0-3s; (b) 0-6s; (c) 0-9s; (d) 0-15s; (e) 3-9s; (f) 3-15s. Time zero is the onset of the signal. The asterisks show the rms noise amplitudes measured in a window before signal onset.

The lines are least squares estimates obtained assuming there are no errors in the abscissa. The equations of the lines are given at the top of each figure with the 95% confidence limits on the slope and intercepts. x and y stand for the abscissa and ordinate respectively of the graphs.

Figure 24 Graphs of GBA rms amplitudes in the 1.0-4 Hz band and a number of time windows, against m_b^{ML} . The time windows are: (a) 0-3s; (b) 0-6s; (c) 0-9s; (d) 0-15s; (e) 3-9s; (f) 3-15s. Time zero is the onset of the signal. The asterisks show the rms noise amplitude measured in a window before signal onset.

The lines are least squares estimates obtained assuming there are no errors in the abscissa. The equations of the lines are given at the top of each figure with the 95% confidence limits on the slope and intercepts. x and y stand for the abscissa and ordinate respectively of the graphs.

Figure 25 Graphs of various observations taken from the YKA seismograms against m_b^{ML} . (a) rms amplitudes 9-18s (0.5-4.0 Hz); (b) rms amplitudes 9-18s (1.0-4.0 Hz). The asterisks show the rms noise amplitude measured in a window before signal onset.

The lines are least squares estimates obtained assuming there are no errors in the abscissa. The equations of the lines are given at the top of each figure with the 95% confidence limits on the slope and intercepts. x and y stand for the abscissa and ordinate respectively of the graphs.



FIGURE 1





(b) EKA









Short period

Deconvolved





Figure 8



Figure 9

29

9 MY













Figure 15

35

15MW








Figure 20

20MW

40



 $10^{2} y = (0.81 \pm 0.06) x - (4.05 \pm 0.30)$ Corr. coeff=0.97 $\sigma^{2} = 0.0081$









24MG

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Figure 25

25MG

<u>APPENDIX A</u>

SEISMOGRAMS FOR THE MURUROA EXPLOSIONS



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CBASSP MANY Y Y YUMMAY YUMMAY WWW WWW WWW WWW WWW

GBA



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NO TAPE NOT PROCESSED WRA Short period, broad band and deconvolved P seismograms from the Mururoa explosion of 11 July 1976. Figure A1



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GBA



EKA

EKA NOT PROCESSED

WRA NOT PROCESSED NO TAPE

Short period, broad band and deconvolved P seismograms from the Mururoa explosion of 19 February 1977. Figure A2



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SEEN

YKA PROCESSED

YKA

WRA NOT PROCESSED NO TAPE

EKA PROCESSED PKP DETECTED

Short period, broad band and deconvolved P seismograms from the Mururoa explosion of 19 March 1977. Figure A3

49

WRA











Figure A4 Short period, broad band and deconvolved P seismograms from the Mururoa explosion of 6 July 1977.

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WRA

EKA

EKA NOT PROCESSED

WRA NOT PROCESSED NOT AVAILABLE

Short period, broad band and deconvolved P seismograms from the Mururoa explosion of 12 November 1977. Figure A5



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WRA NOT PROCESSED NOT AVAILABLE

CKA PROCESSED PKP NOT DETECTED

Short period, broad band and deconvolved P seismograms from the Mururoa explosion of 24 November 1977. Figure A6

WWWWWWWWWWWWWWWWWWWW CBA PROCESSED SEEN SWALL 3 130 125 GBA ⁵⁰ 15 seconds 110 CBA SP

YKA NOT PROCESSED NOT AVAILABLE

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Short period, broad band and deconvolved P seismograms from the Mururoa explosion of 17 December 1977. Figure A7

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CAN WWWWWWWWWWWWW BA PROCESSED NOT SEEN GBA YA PROCESSED SEEN SWALL

yka

YKA BB

NOT PROCESSED EKA

EKA

NOT SEEN

WRA PROCESSED

Short period, broad band and deconvolved P seismograms from the Mururoa explosion of 27 February 1978.

Figure A8





Short period, broad band and deconvolved P seismograms from the Mururoa explosion of 22 March 1978.

Figure A9



EKA

EKA NOT PROCESSED



Short period, broad band and deconvolved P seismograms from the Mururoa explosion of 19 July 1978. Figure A10

Short period, broad band and deconvolved P seismograms from the Mururoa explosion of 26 July 1978. Figure A11

WRA PROCESSED NOT SEEN

WRA

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115

15 seconds 10

YKA BB

EKA

NOT AVAILABLE WRA NOT PROCESSED

EKA NOT PROCESSED

Short period, broad band and deconvolved P seismograms from the Mururoa explosion of 2 November 1978. Figure A12

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Short period, broad band and deconvolved P seismograms from the Mururoa explosion of 30 November 1978. Figure A13

EKA PROCESSED PKP DETECTED

LARGE SEEN

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www.

YKA

YKA SP

YKA BB



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15 seconds 110

YKA BB+t*=0.35s

EKA

EKA NOT PROCESSED

NO TAPE WRA NOT PROCESSED Short period, broad band and deconvolved P seismograms from the Mururoa explosion of 17 December 1978. Figure A14

YKA SP YKA SP YKA BB YKA BB+t*=0.35s YKA BB+t*

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CBA PROCESSED SEEN SWALL

EKA NOT PROCESSED



YKA BB+t*=0.35s

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YKA SP

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Short period, broad band and deconvolved P seismograms from the Mururoa explosion of 9 March 1979. Figure A17





CBA PROCESSED SEEN SMALL





EKA NOT PROCESSED



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> NOT AVAILABLE WRA NOT PROCESSED

Short period, broad band and deconvolved P seismograms from the Mururoa explosion of 4 April 1979. Figure A19



Short period, broad band and deconvolved P seismograms from the Mururoa explosion of 18 June 1979. Figure A20



Short period, broad band and deconvolved P seismograms from the Mururoa explosion of 29 June 1979. Figure A21







EKA PROCESSED PKP DETECTED

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Figure A22 Short period, broad band and deconvolved P seismograms from the Mururoa explosion of 25 July 1979.

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EKA NOT PROCESSED

Short period, broad band and deconvolved P seismograms from the Mururoa explosion of 28 July 1979. Figure A23

Short period, broad band and deconvolved P seismograms from the Munuroa explosion of 22 November 1979. Figure A24

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YVAN BB+10=0.355 YKA PROCESSED SEEN 33 8 ŝ YKA ଟ୍ଟ <u>r</u> 5 seconds 10 YKA SP

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WRA PROCESSED SEEN VERY SWALL

Short period, broad band and deconvolved P seismograms from the Mururoa explosion of 3 March 1980. Figure A26


Short period, broad band and deconvolved P seismograms from the Mururoa explosion of 23 March 1980. Figure A27



Short period, broad band and deconvolved P seismograms from the Mururoa explosion of 1 April 1980. Figure A28

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WRA PROCESSED SEEN

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15 seconds 110



Short period, broad band and deconvolved P seismograms from the Mururoa explosion of 4 April 1980. Figure A29

EVENT 034 04 MPR 1980

EVENT 034 04 PPR 1980



Short period, broad band and deconvolved P seismograms from the Mururoa explosion of 16 June 1980. Figure A30

TIVNS KAAS GASSA •

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Short period, broad band and deconvolved P seismograms from the Mururoa explosion of 21 June 1980. Figure A31

WRA PROCESSED SEEN VERY SMALL

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15 seconds 110

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 GBA
 SP

 GBA
 SP

 GBA
 BB

 GBA
 BB+t*=0.35%

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 Jump

 Jump
 Jump

EKA

EKA NOT PROCESSED



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YKA PROCESSED SEEN VBB ONLY

Short period, broad band and deconvolved P seismograms from the Mururoa explosion of 19 July 1980. Figure A33

EXA PROCESSED PKP DETECTED

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EKA BB WWWWWWWWWWWW EKA BB+ty=0.15s EKA SP Mary Mary Mary Mary Mary Mary Mary area ~~~ mmmmml/mm//hmm \sim SCEN CBA PROCESSED 130 135 EKA GBA GBA BB+t*=0.35s **GBA BB GBA** SP

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Short period, broad band and deconvolved P seismograms from the Mururoa explosion of 3 December 1980. Figure A34

EKA PROCESSED PKP NOT DETECTED

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Short period, broad band and deconvolved P seismograms from the Mururoa explosion of 6 March 1981. Figure A36

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CBA PROCESSED NOT SEEN

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NO TAPE NOT PROCESSED WRA Short period, broad band and deconvolved P seismograms from the Mururoa explosion of 11 July 1981. Figure A40







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EKA NOT PROCESSED



Short period, broad band and deconvolved P seismograms from the Mururoa explosion of 24 February 1982. Figure A47

PROCESSED SEEN VERY SWALL













Short period, broad band and deconvolved P seismograms from the Mururoa explosion of 20 March 1982. Figure A48

WRA PROCESSED SEEN VERY SWALL

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Short period, broad band and deconvolved P seismograms from the Mururoa explosion of 27 June 1982. Figure A49







EKA NOT PROCESSED

Short period, broad band and deconvolved P seismograms from the Mururoa explosion of 1 July 1982. Figure A50

SWALL

SEEN

WRA PROCESSED







WRA

WRA NOT PROCESSED NO TAPE

Short period, broad band and deconvolved P seismograms from the Mururoa explosion of 25 July 1982. Figure A51





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Short period, broad band and deconvolved P seismograms from the Mururoa explosion of 25 April 1983. Figure A53

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15 seconds 110

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Short period, broad band and deconvolved P seismograms from the Mururoa explosion of 18 June 1983. Figure A55

VRA PROCESSED NOT SEEN





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Short period, broad band and deconvolved P seismograms from the Mururoa explosion of 20 July 1983. Figure A57

TRA PROCESSED SEEN VERY SWALL





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Short period, broad band and deconvolved P seismograms from the Mururoa explosion of 3 December 1983. Figure A59

VRA PROCESSED SEEN SWALL

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YKA BB+te=0.35s May w Jay w

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YKA BB

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YKA SP



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EKA NOT PROCESSED



WRA PROCESSED SEEN



GBA

WRA

CBA PROCESSED SEEN SWALL

EKA

EKA NOT PROCESSED

NO TAPE NOT PROCESSED WRA Short period, broad band and deconvolved P seismograms from the Mururoa explosion of 8 May 1984. Figure A61





YKA

YKA SP

Short period, broad band and deconvolved P seismograms from the Mururoa explosion of 12 May 1984. Figure A62

108

EXA PROCESSED PKP DETECTED

RA PROCESSED SEEN COMPLEX
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YKA BB

YKA

YKA SP

YKA BB+t*=0.355 Price BB+t*=0.3

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Short period, broad band and deconvolved P seismograms from the Mururoa explosion of 12 June 1984. Figure A63

WRA PROCESSED NOT SEEN



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WRA PROCESSED SEEN VERY SMALL

Short period, broad band and deconvolved P seismograms from the Mururoa explosion of 27 October 1984.

Figure A65

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WRA

WRA SP

YKA BB

YKA BB+t*=0.35s

YKA

YKA SP



WRA BB

WRA BB+t*=0.35s

EKA NOT PROCESSED

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113

Short period, broad band and deconvolved P seismograms from the Mururoa explosion of 1 December 1984. Figure A67

WRA PROCESSED NOT SEEN



15 seconds 110

YKA BB+t*=0.35s

YKA BB

YKA SP



114

WRA BB

WRA SP

WRA BB+t*=0.35s





Short period, broad band and deconvolved P seismograms from the Mururoa explosion of 30 April 1985. Figure A69

TRA PROCESSED SEEN VERY SMALL

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NOT PROCESSED EKA



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YKA BB+t*=0.35s

YKA BB

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YKA SP





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15 seconds 110

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Short period, broad band and deconvolved P seismograms from the Mururoa explosion of 24 October 1985. Figure A73

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15 seconds 110

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WRA BB+t*=0.35s

Short period, broad band and deconvolved P seismograms from the Mururoa explosion of 24 November 1985. Figure A75



Short period, broad band and deconvolved P seismograms from the Mururoa explosion of 26 November 1985. Figure A76

122

WRA BB

WRA SP

YKA BB

YKA SP



Short period, broad band and deconvolved P seismograms from the Mururoa explosion of 26 April 1986. Figure A77



Short period, broad band and deconvolved P seismograms from the Mururoa explosion of 6 May 1986. Figure A78



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YKA

YKA SP

mmmmmmm

YKA BB+t*=0.35s

YKA BB

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Short period, broad band and deconvolved P seismograms from the Mururoa explosion of 27 May 1986. Figure A79



WRA

WRA SP

YKA BB+t*=0.35s

YKA BB

YKA

YKA SP



126

WRA BB

WRA BB+t*=0.35s







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PROCESSED SEEN

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YKA

YKA SP



FRA PROCESSED SEEN VERY SWALL

EKA NOT PROCESSED

EKA

Short period, broad band and deconvolved P seismograms from the Mururoa explosion of 5 May 1987. Figure A84



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YKA BB+t*=0.35s

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YKA BB

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γka

YKA SP



EKA PROCESSED PKP NOT DETECTED

TRA PROCESSED SEEN COMPLEX

131

WRA BB

WRA BB+t*=0.35s

WRA SP



VERY SWALL SEEN PROCESSED 2 Short period, broad band and deconvolved P seismograms from the Mururoa explosion of 6 June 1987.

Figure A86





NOT PROCESSED EKA

132



143.2M

YKA BB

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YKA

YKA SP



Short period, broad band and deconvolved P seismograms from the Mururoa explosion of 21 June 1987. Figure A87

EKA NOT PROCESSED



Short period, broad band and deconvolved P seismograms from the Mururoa explosion of 23 October 1987. Figure A88

WRA BB

WRA SP

YKA BB

YKA SP

EKA PROCESSED PKP DETECTED

TRA PROCESSED SEEN COMPLEX



Short period, broad band and deconvolved P seismograms from the Mururoa explosion of 5 November 1987. Figure A89



WRA

WRA SP

YKA BB+t*=0.35s

YKA BB

5 seconds

YKA

YKA SP



EKA PROCESSED PKP DETECTED

FRA PROCESSED SEEN

136

VRA BB

WRA BB+t*=0.35s



Short period, broad band and deconvolved P seismograms from the Mururoa explosion of 29 November 1987.

Figure A91







Short period, broad band and deconvolved P seismograms from the Mururoa explosion of 11 May 1988. Figure A92 3

ICA PROCESSED PKP NOT DETECTED



Figure A93 Short period, broad band and deconvolved P seismograms from the Mururoa explosion of 25 May 1988.

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Short period, broad band and deconvolved P seismograms from the Mururoa explosion of 16 June 1988. Figure A94

WRA PROCESSED SEEN

140







YKA BB+t*=0.35s

YKA BB

YKA SP



142

WRA BB

WRA SP

WRA BB+t*=0.35s

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Short period, broad band and deconvolved P seismograms from the Mururoa explosion of 23 November 1988. Figure A97





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Short period, broad band and deconvolved P seismograms from the Mururoa explosion of 11 May 1989. Figure A98

EKA PROCESSED PKP NOT DETECTED

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WRA NOT PROCESSED NOT AVAILABLE

EKA NOT PROCESSED

Short period, broad band and deconvolved P seismograms from the Mururoa explosion of 20 May 1989. Figure A99











TRA PROCESSED SEEN





WRA BB

WRA BB+t*=0.35s

WRA

WRA SP

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YKA BB

YKA BB+t*=0.35s

YKA

YKA SP





Figure A103

WRA BB

<u>APPENDIX B</u>

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SEISMOGRAMS FOR THE FANGATAUFA EXPLOSIONS



Short period, broad band and deconvolved P seismograms from the Fangataufa explosion of 5 June 1975. Figure B1





Short period, broad band and deconvolved P seismograms from the Fangataufa explosion of 30 November 1988. Figure B3





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EXA PROCESSED PRP DETECTED

WRA PROCESSED SEEN

154

WRA SP

YKA BB

YKA SP

WRA BB



Short period, broad band and deconvolved P seismograms from the Fangataufa explosion of 27 November 1989. Figure B5

EKA PROCESSED PIC DETECTED

seconds 10

APPENDIX C

TABLES OF MURUROA OBSERVATIONS

All the observations given in the tables are as measured except for ψ_{∞} , moment M_0 , and magnitude m_b . ψ_{∞} is calculated from the measured area H using the relation

$$\psi_{\infty} = \{2KG(\Delta)\}^{-1} H$$

where $K = [\rho_1 v_1 / \rho_0 v_0]^{4}$. $\rho_1 \& v_1$ are the density and P wave speed respectively for the material in which the explosion was fired and $\rho_0 \& v_0$ are the corresponding quantities for the material on which the recording station is sited. $G(\Delta)$ is the geometrical spreading effect and is listed by Carpenter [11]. M_0 is calculated from ψ_{∞} using the relation:

$$M_{o} = 4\pi\rho_{1}v_{1}^{2}\psi_{\infty}$$

All amplitudes listed are as measured and are for a system of unit gain at 1 Hz. Magnitude m_b , is thus given by

$$m_{\rm b} = \log(A/T) + B(\Delta)$$

where A is the $\frac{1}{2}$ peak-to-peak amplitude divided by the gain at period T, T is the period and B(Δ) is the distance correction term given by the table of Lilwall [9].

The values of B(Δ), G(Δ), ρ_0 , v_0 , ρ_1 & v_1 used are given in this appendix and in Appendix D.

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ê		5.54 5.54 5.73 73
Gain	489898989898989898989898989898989898989	1.61 0.90 1.53 1.00
Frequency (Hz)	10,000 884 88,000 89,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000 80,000	1.33 0.95 1.29
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servation pP-P time	48888888888888888888888888888888888888	0.38 0.57 0.59
period ob Fall time		0.12 0.17 0.22 0.22
d short Rise time	20000000000000000000000000000000000000	0.25 0.25 0.20
bad band ar Duration (s)	00000000000000000000000000000000000000	0.51 0.60 0.54
e array - Bro Moment (N m)	0.30 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.329 0.3	0.3537E+15 0.2477E+16 0.3862E+15 0.4067E+16
Yellouknif Vg (m ³ )	2493.45 3331.19 3331.19 3331.19 3331.19 539.70 739.70 739.70 739.70 739.71 739.71 739.71 739.71 739.71 739.71 739.72 777.21 777.22 777.21 777.22 777.22 777.21 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 777.22 7777.22 7777.22 777.22 777.22 777.22 77	904.84 6336.72 987.95 10405.86
Table IA Date	750711 770219 770219 770219 770219 7803227 7803227 7803227 7803227 7803227 7803201 7803227 7903201 7903201 8003223 8003223 8003223 8003223 8003223 8003223 8003223 8003223 8003223 8003223 8003223 810328 8103228 8103228 8103228 8103228 8103228 8103228 8103228 8103228 8103228 8103228 8103228 8103228 8103228 8103228 8103228 8103228 8103228 8103228 8103228 8103228 8103228 8103228 8103228 8103228 8103228 8103228 8103228 8103228 8103228 8103228 8103228 8103228 8103228 8103228 8103228 8103228 8103228 8103228 8103228 8103228 8103228 8103228 8103228 8103228 8103228 8103228 8103228 8103228 8103228 8103228 8103228 8103228 8103228 8103228 8103228 8103228 8103228 8103228 8103228 8103228 8103228 8103228 8103228 8103228 8103228 8103228 8103228 8103228 8103228 8103228 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 810328 81038 81038 81038 81038 81038 81038 81038 81038 81038 81038 81038 81038 81038 81038 81038 81038 81038 81038 81038 810038 810038 810038 810038 8100038 8100038 8100038 81000	840612 840616 841027 841102

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Table 2A	Yellowknife	annay -	Observations	in the	0.5-4.0Hz	band							
Date	1/2 Pk-Pk	Period	Frequency	Gain	т _ь		r.m.s.						
	(1111)	(5)	(HZ)			(DD)	0-65	(00)	(00)	3-95	3-135	9-185	noise
760711	18.64	0.82	1.21	1.40	5.13	9,00	7.51	6.26	4.88	4.26	3.08	0.93	0.24
770219	25.13	Õ.7Õ	1.43	1.75	5.23	9,65	7.31	6.07	4.77	2.94	2.27	1.12	0.29
770706	17.57	0.82	1.21	1.40	5.10	8.26	6.47	5.38	4.25	3.06	2.36	1.27	0.31
771112	10.35	0.77	1.29	1.53	4.86	4.88	3,90	3.20	2.67	1.87	1.73	1.50	1.41
700227	1.67	0.70	1.43	1.00	4+03	0.13	4.92	2.95	2.10	0.37	0.33	0.30	0.27
780719	5.17	1.17	0.85	0.70	4.72	2,69	2.05	1.72	1.40	0.89	0.80	0,63	0.30
780726	3.29	0.73	1.38	1.68	4.35	1.38	1.02	0.87	0.72	0.44	0.41	0.34	0.27
781102	9.73	0.63	1.60	2.00	4.81	3.78	2.87	2.50	2.00	1.50	1.19	0.85	1.10
781130	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
781219	23.26	0.77	1.33	1.53	5.21	10.58	8.48	7.14	2.50	4.53	3.36	1.40	0.26
790301	13.16	0.75	1.33	1.61	4.96	5.70	4.20	3.52	2.77	1.52	1.22	0.95	0.24
790309	15.07	0.77	1.29	1.53	5.02	6.82	5.29	4.43	3.51	2.47	1.95	1.17	0.23
790324	23.83	0.77	1.29	1.53	5.22	10.98	8.00	6.60	5.14	2.26	1.71	0.94	0.22
790404	18.95	0.73	1.43	1.68	5.02	6.07	5.43	4.03	3.60	1.22	1.05	1+12	0+28
790629	36.45	0.90	1.11	1.22	5.44	17.43	12,81	10.59	8.30	4.05	3.17	2,23	0.78
790725	0.00	õ.õõ	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	ō.ōō	0.00
790728	12.95	0.73	1.38	1.68	4.95	5.43	3.91	3.27	2.63	1.12	1.11	1.07	0.43
(91122	(+38	0.15	1.33	1.93	4.60	3.31	2.50	2.14	1.18	1+18	1.10	1.11	0.83
800303	5.88	0.80	1.25	1.47	4.62	2.61	1.94	1.62	1.30	0.72	0.64	0.53	0.24
800323	67.26	1.13	0.89	0.77	5.81	33.33	25.45	20.93	16.46	10.07	7.80	3.81	0.26
800401	35.48	0.77	1.29	1.53	5.39	15.20	10.97	9.01	7.10	2.47	2.30	2.03	0.27
800404	7.64	0.82	1.21	1.40	4.74	3.66	2.77	2.31	1.80	1.14	0.85	0.38	0.28
800621	12.09	0.38	1.38	1.68	4.92	5.19	4.02	3.37	2.66	1.89	1.45	0.92	0.31
800706	9,69	0.82	1.21	1.40	4.84	4.15	3.13	2.63	2.09	1.33	1.08	0.84	0.33
810227	6.30	0.77	1.29	1.53	4.64	2.82	2.06	1.72	1.35	0.68	0.53	0.39	0.29
810306	7-11	0.68	1.48	1.83	4.68	3.06	2.30	1.94	1.52	0.97	0.75	0.41	0.28
810328	14.84	0.15	1.05	1.10	5.09	7.01	5.11	4.22	3.30	1.45	1.16	0.76	0.30
810708	26.82	1.00	1.00	1.00	5.35	12.66	9.81	8.10	6.36	4.29	3.24	1.43	0.74
810711	3.12	0.75	1.33	1.61	4.33	1.36	1.03	0.87	0.71	0.46	0.42	0.40	0.29
810718	6.59	0.70	1.43	1.75	4.65	2.80	2.07	1.76	1.44	0.86	0.79	0.66	0.60
810803	33-47	0.82	1.33	1.61	5.10	7,89	5.73	4.80	3.80	1.85	1.60	1.28	1.16
811205	11.96	0.77	1.29	1.53	4.92	5.03	3.67	3.05	2.44	1.13	1.07	ō.99	0.51
811208	24.40	0.85	1.18	1.34	5.25	12.77	9.50	7.80	6.09	3.09	2.37	1.21	0.35
820220	1.95	0.70	1.43	1.75	4.12	0,96	0.72	0.65	0.56	0.41	0.41	0.39	0.39
820224	21.32	0.90	1.08	1.16	5.22	9,91	7.12	5.85	4.59	1.47	1.32	1.15	0.33
820627	2,60	0.70	1.43	1.75	4.25	1.09	0.82	0.68	0.56	0.31	0.30	0.32	0.26
820701	31.69	0.90	1.11	1.22	5.38	15.82	11.67	9.60	7.50	3.60	2.79	1.49	0.46
820725	73.78	0.98	1.03	1.05	5.78	37.34	26.97	22.25	17.44	6.74	5.63	3.88	0.43
830413	89.84	0.82	1.38	1.68	3.71	44+45	34+13	28.12	22+33	13+(8	0.25	3.45	0.44
830618	3.50	0.13	1.21	1.40	4.40	1.53	1.14	0.96	0.77	0.47	0.39	0.31	0.32
830628	56.64	Õ.77	1.29	1.53	5.60	25.43	18.69	15.36	12.07	5.54	4.51	2.94	0.20
830720	8.52	0.80	1.25	1.47	4.78	4.14	3.04	2.52	1.99	0.97	0.81	0.65	0.24
830804	29.80	0.93	1.08	1.16	5.36	15.21	11.25	9-32	7.29	3.85	2.94	1.60	0.86
831203	17.09	0.80	1.11	1.22	4.08	2.33	1.73	1+41	3.83	1.58	1.45	1.36	0.38
840508	11.23	0.73	1.38	1.68	4.89	4.95	3.62	2.99	2.37	1.09	0.94	0.81	0.20
840512	77.10	0.98	1.03	1.05	5.80	37.24	27.50	22.73	17-84	9.04	7.16	4.58	0.20
840612	12.66	0.75	1.33	1.61	4.94	5.86	4.24	3.52	2.75	1.18	0.92	0.61	0.28
840616	40.03	0.95	1.05	1.10	5.50	19-86	15.37	12-81	10-12	6.99	5.42	2.65	U-18
8411027	57.02	0.77	1.29	1.53	5.60	27.74	21.09	17.37	13.69	8.24	6.48	3.69	1.21

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Date	1/2 Pk-Pk	Period	Frequencu	Gain		r.m.s.	C+D+S+	r.m.s.	C+8+5+	r.m.s.	r.m.s.	r.m.s.	r.m.s.
	(mm)	(5)	(Hz)			0-35	0-65	0-95	0-15s	3-95	3-155	9-185	noise
						(nm)	ົດຫຼັ	( ຕາຫຼັງ	(nm)	(nm)	(nm)	(nm)	(חח)
841201	1.04	1.02	0,98	0.95	3,95	0.47	0.37	0.32	0.30	0.20	0.24	0.26	0.27
841206	79.26	0.88	1.14	1.28	5.77	35.74	26.39	21.74	16.94	8.39	6.26	3.13	0.39
850430	10.90	0.88	1.14	1.28	4.91	5.24	3.87	3.20	2.53	1.29	1.06	0.67	0.15
850508	72.24	0.80	1.25	1.47	5.71	36.78	26.56	22.14	17.65	7.70	7.17	6.49	0.21
850603	17.26	0.88	1.14	1.28	5.11	7.59	5.52	4.54	3.55	1.45	1.15	0.71	0.20
850607	9.19	0.68	1.48	1.83	4.79	3.73	2.83	2.35	1.89	1.16	0.99	0.67	0.30
851024	5.93	0.65	1.54	1.91	4.60	2.54	1.95	1.63	1.33	0.86	0.77	0.58	0.67
851026	45.57	0.98	1.03	1.05	5.57	22.97	17.65	14.88	11.63	8.28	6.11	2.34	0.82
851124	11.73	0.93	1.08	1.16	4.96	5.38	3.97	3.27	2.58	1.26	1.05	0.79	0.26
851126	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
860426	7.28	0.85	1.18	1.34	4.73	3.51	2.68	2.27	1.78	1.24	0.94	0.50	0.17
860506	9.73	0.68	1.48	1.83	4.82	4.20	3.20	2.65	2.08	1.29	0.99	0.50	0.21
860527	14.60	0.85	1.18	1.34	5.03	6.79	4.92	4.05	3.19	1.23	1.10	0.83	0.23
360530	71.07	1.02	0.98	0.95	5.78	34.31	25.33	20.85	16.86	7.99	7.83	6.54	0.21
861206	14.70	0.75	1.33	1.61	5.01	6.37	4.71	3.87	3.03	1.47	1.16	0.63	0.32
861210	34.89	1.02	0.98	0.95	5.47	17.46	13.10	10.85	8.62	4.94	4.09	2.65	0.19
70505	8,90	0.90	1.11	1.22	4.83	4.65	3.47	2.88	2.28	1.26	1.03	0.68	0.27
370520	69.99	0.82	1.21	1.40	5.70	32.53	23.80	19.68	15.45	7.21	5.80	3.71	0.18
370606	13.18	0.77	1.29	1.53	4.96	5.75	4.43	3.70	2.93	2.00	1.58	0.88	0.38
870621	41.28	0.93	1.08	1.16	5.51	20.32	14.79	12.17	9.53	3.98	3.21	2.38	0.30
871023	76.44	1.00	1.00	1.00	5.80	37.81	28.31	23.18	18.23	9.57	7.63	5.24	2.03
371105	65.97	0.77	1.29	1.53	5.66	27.92	20.20	16.64	13.11	5.07	4.46	3.45	0.73
871119	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
871129	10.68	0.90	1.11	1.22	4.91	5.54	4.11	3.38	2.67	1.35	1.10	0.75	0.37
880511	52-08	1.00	1.00	1.00	5.64	24.90	18.31	15.10	11.84	5.66	4.49	2.62	0.25
880525	60.43	1.13	0.89	0.11	5.76	29.61	22.36	18.37	14.70	8.22	7-13	5.16	0.29
880616	8.10	0.82	1.21	1.40	4.((	3.81	3.02	2.52	1.98	1.49	1.12	0.52	0.28
880623	51.85	0.85	1.18	1.34	2.28	23.24	16.85	13.89	10.90	4.40	3.68	2.61	0.54
881105	38.85	0.13	1.38	1.68	5.42	21.01	15.20	12.95	10.26	2.33	4.61	3.05	0.48
881123	41.09	1+10	0.91	0.82	5.64	21.67	16.08	13.19	10.53	5.12	4.50	3.39	0.52
890311	40.97	0.80	1.20	1.47	3.40	11.39	12.60	10.31	0.10	3-18	2.33	1.33	0.28
830320	10.80	0.00	1.29	1.00	4.88	4.64	3.38	2.98	2.30	1.61	1.20	0.10	0.25
030603	40.33	1 00	1.14	1.20	5 60	19 90	15 22	13.23	10.31	4.02	3.33	2.01	0.28
031024	29.76	0.77	1 29	1 62	5 42	13.30	14 64	12.04	3.02	7 00	++•04 5 14	2.34	1.11
031031	33.10	0+1+	1.23	1.03	J+42	10.23	14+04	12+04	3.30	1+08	J. 14	1+31	0.08

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Table 38	Vellouknife	arrau -	Observations	in the	1.0-4.0Hz	band								
Date	1/2 Pk-Pk	Period	Frequency	Gain	m _b	r.m.s.	r.m.s.	r.m.s.	r.m.s.	r.m.s.	r+m+5+	r.m.s.	r•m•s•	
	(שרו)	(5)	(Hz)		-	0-3s	0-6s	0-9s	0-155	3-9s	3-15s	9-18s	noise	
700711	12 60	0.75	1 22	1 61	4 94	(nm) 5 21	(nn) 4.14	(nm) 2 40	(nm) 2 72	(nm) 1 97	(nn) 1 47	(nm) 0 c2	(nm) 0 15	
770219	19.84	0.15	1.54	1.91	5,12	7.73	5.84	4.82	3.77	2.23	1.68	0.03	0.12	
770706	12.35	0.75	1.33	1.61	4.93	5.39	4.05	3.37	2.64	1.56	1.21	0.72	0.22	
771112	7.73	0.70	1.43	1.75	4.72	3.61	2.85	2.35	1.98	1.33	1.29	1.28	1.06	
780227	1.37	0.63	1.60	2.00	3.96	0.55	0.43	0.38	0.31	0.25	0.21	0.16	0.15	
780322	12.40	0.70	1.43	1.75	4.92	5.37	3.88	3.18	2.49	0.88	0.76	0.58	0.17	
780726	2.54	0.73	1.38	1.68	4.41	1.04	0.76	0.65	0.00	0.53	0.28	0.24	0.28	
781102	8.54	0.63	1.60	2.00	4.75	3.37	2,50	2.17	1.72	1.17	0.92	0.66	0.80	
781130	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
781217	11.48	0.70	1.43	1.75	4.89	4.84	3.52	2.89	2.26	0.91	0.73	0.50	0.13	
790201	9.46	0.68	1.48	1.83	4.80	4.08	3-13	4.35	3.43	2.41	1.88	0.91	0.13	
790309	11.39	0.73	1.38	1.68	4.89	5.09	3.91	3.25	2.56	1.69	1.32	0.76	0.11	
790324	17.53	0.73	1.38	1.68	5.08	7.72	5.71	4.71	3.66	1.85	1.36	0.66	0.11	
790404	15.23	0.65	1.54	1.91	5.01	6-17	4.48	3.70	2.90	1.23	1.01	0.63	0.15	
790618	12.38	0.68	1.48	1.83	4.92	5.09	3.61	3.03	2.38	0.91	0.11	0.64	0.19	
790725	23:01	0,00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
790728	9.77	0.70	1.43	1.75	4.82	4.05	2.97	2.47	1.96	0,99	0.83	0.63	0.31	
791122	5.55	0.65	1.54	1.91	4.57	2.42	1.86	1.57	1.32	0.89	0.84	0.85	0.60	
800223	2.10	0.65	1.54	1.91	4.03	2.07	1.48	1.12	0.95	0.50	0.30	0.22	0.10	
800323	31.36	1.05	0.95	0.90	5.44	16.40	12.84	10.73	8,56	6.18	4.95	2.77	0.09	
800401	26.59	0.70	1.43	1.75	5.26	11.39	8.33	6.84	5.34	2.28	1.81	1.20	0.11	
800404	6.13	0.68	1.48	1.83	4.61	2.57	2.03	1.67	1.31	0.95	0.70	0.28	0.12	
800616	29+20	0.93	1.38	1.58	3.33 4.80	12.22	3,04	9.34 2.52	1.98	3+15	2.42	1.20	0.16	
800706	6,96	0.68	1.48	1.83	4.67	2,97	2.24	1.87	1.49	0.92	0.75	0.64	0.21	
810227	4.87	0.77	1.29	1.53	4.53	2.12	1.58	1.32	1.03	0.60	0.46	0.28	0.18	
810306	5.75	0.65	1.54	1.91	4.58	2.26	1.73	1.45	1.14	0.77	0.59	0.29	0.15	
810410	11.59	0.60	1.67	2.09	4.89	5.02	3.63	3.00	2.35	0.95	0.33	0.52	0.18	
810708	15.04	0.85	1.18	1.34	5.04	7.30	5.78	4.81	3.82	2.85	2.22	1.20	0.60	
810711	2.36	0.77	1.29	1.53	4.22	0.99	0.75	0.63	0.51	0.32	0.29	0.28	0.19	
810718	5.61	0.68	1.48	1.83	4.58	2.35	1.(2	1.45		0.62	0.58	0.51	0.49	
811111	13.74	0.73	1.38	1.68	4.97	5.91	4.33	3.62	2.88	1.48	1.26	1.02	0.96	
811205	9.08	0.65	1.54	1.91	4.78	3.74	2.73	2.26	1.83	0.82	0.83	0.73	0.36	
811208	16.37	0.77	1.29	1.53	5.06	8.03	6.31	5-17	4.05	2.81	2.10	0.85	0.23	
820220	1.53	0.88	1.14	1.28	4.06	0.69	0.52	0.44	0.38	0.23	0.24	0.25	0.20	
820320	14.18	0.75	1.33	1.61	4.99	7.04	5.08	4.18	3.28	1.20	1.01	0.81	0.20	
820627	2.07	0.68	1.48	1.83	4.14	0.83	0.63	0.52	0.41	0.23	0.19	0.14	0.12	
820701	18.67	0.77	1.29	1.53	5.12	9.43	7.12	5.93	4.65	2.88	2.20	1.14	0.35	
820725	49.64	0.75	1.38	1.61	5.53	24.61	22.02	14.75	11.51	4.84	4.12	3.05	0.32	
830425	0.62	0.75	1.33	1.61	3.63	0.33	0.28	0.25	0.21	0.20	0.17	0.14	0.11	
830618	2.65	0.68	1.48	1.83	4.25	1.18	0.89	0.75	0.61	0.39	0.33	0.25	0.21	
830628	43.37	0.73	1.38	1.68	5.47	19.88	14.44	11.86	9.31	3.64	3.10	2.30	0.10	
830720	6+22 19.04	0.15	1.33	1.10	4.63	2.15	2.02	1.67	1.32	0.65	0.54	0.49	0.74	
831203	4.07	0.70	1.43	1.75	4.44	1.82	1.34	1-14	0,90	0.54	0.45	0.33	0.27	
831207	11.22	0.88	1.14	1.28	4.92	5.56	4-07	3.34	2.66	1.14	1.05	0.91	0.52	
840508	8.45	0.70	1.43	1.75	4.76	3.82	2.82	2.33	1.86	0.94	0.81	0.61	0.11	
840512	47+32	0,70	1.43	1.75	5.51	22.81	16-83	13.93	11.00	5.56	4.61	3.22	0.10	
840612	22.41	0.88	1.43	1.28	5.22	11.46	9.37	7.76	6,10	4.95	3.70	1.50	0.11	
841027	7.31	0.65	1.54	1.91	4.69	3.24	2.44	2.03	1.72	0.96	1.03	1.06	0.68	
841102	39.65	0.60	1.67	2.09	5.42	16.67	12.53	10.35	8.22	4.66	3.87	2.66	0-88	

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7.m.s. 10ise	0.11	0.03	0.15	0.51	0.56	.00	0.07	0.13		0.15	010	0.19	0.12	0.29	0-13	0.37	0.00	0.26	0.15	0.12		0.32	0.34	0.17	0.15	0.20	0.41
7.m.S. 9-185	2-34	0.40 3.79	0.61 0.42	0.38	1.72	00.0	0.35	0.34	0.48 843	0.47	1.53	0.49	2.43	0.0	1.81	2.07	00.0	0.55	2.11	3•13	0° 20	2.31	2.00	1.13	0.51	1.59	1.03
7.8.5. 3-15s ()	0-12	5.28 5.28	0.86	0.47	3.81 0.67	00.0	0.65	0.67	0.69		2.22	0.72	4.09	1.02	- 04 - 04	3.07	0.00	0.96	2.62	4.89	20.00	3.37	3.19	2.00	0.85	2.44	2.48 3.78
7.m.S. 3-95	0.13	1.08 6.15	1.03 D.90	0.50	5.09 75	00.00	0.85	0.87	58°0	1.16	2.60	0.86	5.09	1.24	2.19	3.78	0.00	1.23	2.84	5.97		3.91	3.86	2.54	1.08	3.04	3.01 5.23
7.m.S. 0-155	0-19	10.30	2.65	0.97	6.66 1 70	0.0	1.22	1.52	01 . 02 01	5.0	4.97	1.49	10.58	00.2	0.81 10.81	9.22 9.22	0.0	1.78	7.80	8.73		5.89	6.54	6.09	1.63	6.96	6.51
-9s 0-9s	0.23	2.15	3.38	1.21	8•48	0.00	1.55	1.94		2.87	6.25	1.88	13.47	2.50	1.38	11.77	0.00	2.26	9.89	10.90	10.10	7.27	8.23	7.80	2.06	8.88	6.36 8.36
band r.m.s. 0-6s	19.01	15.21	<b>4.10</b>	1.45	10.20	0.00	1.87	2•35	00.00	3.50	7.58	2.27	16.32	3.01	8.90 90.01	14.34	0.00	2.75	11.96	13.16	12,10	8.43	9.96	9.45	2.49	10.78	9.60
1.0-4.0Hz r.m.s. 0-35	25.50	3.42 20.46	5.66 3.12	1.97	12.79	0.00	2.40	3.13	21.50	4.70	10.19	3.02	22.20	3.36	12-41	19.67	0.00	3.50	16.64	16.88	15.75 15.75	11.31	13.16	13.02	3.22	14.78	12.45
ons in the Mo	3.80	5.50	4.94	4.49	5.26	0.00	4.53	4.70	4 U 4 U 4 U	4.88	5.16	4.64	5.51 	4.82 0.02	ה יי איי	ດ ເດີຍ ເບີຍ	0.00	4.70	288 198	5.39	5.40	5.23	5.31	5.32	4.71	ດ. ເ	5.26
Observatic 1 Gain	1.61 1.83	1.61	1.83 2.00	1.83	1.40	00.00	1.68	1.83		52.1	1.16	1.34	1-75	1.68	1.4~	1.68	00.0	1.53	1.83	1.01	52	1.83	2.09	1.75	1.61	1.68	2.38
e array - Frequency (Hz)	1.33	1.33	1.48 1.60	1.48	1.21	0.00	1.38	1.48	57.1	64.1	1.08	1.18	1.43	1.38	دی. دی.	1.38	0.00	1.29	1.48	1.54		1.48	1.67	1.43	1.33	1.38	1.67
Yellowknif Period (s)	0.75	5.0 57.0	0.68	0.68	0.82	0.00	0.73	0.68		0.70	0.93	0.85	0- 10	62 °D		0.73	0.00	0.77	0.68	0.65	04.0	0.68	0.60	0.70	0.75	0.73	0.73
(cont`d) 1/2 Pk-Pk (nm)	55.89 55.89	45.32	12.97	4.62	25.02 9.19	0.0	4.98	7.53		11.08	18.79	5.95	47.97	9.57	24.50	47.21	0.00	7.16	36.00	36.39		25.04	30.46	31.00	7.47	31.12	28.56
Table 3A Date	841201 841206	850508	850603 850607	851024	851026	851126	860426	860506		861206	861210	870505	870520	870606	810521	871105	871119	871129	880511	880525 880525	880523	881105	881123	890511	890520	830603	891031 891031

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Table 4A Date	Warramun ∳_	ga array - Bro Moment	bad band ar Duration	nd short Rise	period ob: Fall	servation pP-P	ns 1/2 Pk-Pk	Period	Frequency	Gain	m _b	
	(m³)	(N m)	(s)	time	time	time	(mn)	(5)	(Hz)		-	
770706 780227 780322 780719	726.10 0.00 417.33 197.84	0.2838E+15 0.0000E+00 0.1631E+15 0.7733E+14	0.75 0.00 0.52 0.52	0.28 0.00 0.20 0.15	0.23 0.00 0.17 0.15	0.75 0.00 0.36 0.64	3.64 0.00 3.68 0.88	1.40 0.00 0.75 0.50	0.71 0.00 1.33 2.00	0.45 0.00 1.61 2.51	4.64 0.00 4.35 3.71	36 36 26
780726 781130	0.00	0.0000E+00 0.5171E+16	0.00	0.00	0.00	0.00	0.00 31.76	0.00	0.00	0.00	0.00	36 36
781219 790301	775-99 436-69	0.3033E+15 0.1707E+15	0.84 0.60	0.28 0.15	0.24 0.15	0.00	3.08 2.57	0.80	1.25 1.48	1.47 1.83	4.29 4.19	36 36
790309 790324	752.71 526.83	0.2942E+15 0.2059E+15	0.81 0.75	0.24 0.35	0.21 0.20	0.00	3.42 3.19	0.77	1.29 1.33	1.53	4.33 4.29	36 36
790618 790629	803.46 961.52	0.3140E+15 0.3758E+15	0.75	0.22	0.20	0.00	3.25 4.07	0.75	1.33	1.60	4.30 4.46	36 36
790728	612.59	0.2394E+15 0.2092E+14	0.73	0.32	0.24	0.00	3.26	0.82	1.21	1.40	4.32	36
800223	280.73 229.51	0.1097E+15 0.8971E+14	0.76	0.22	0.27	0.00	1.44	0.85	1.18	1.34	3.97 3.91	36 36
800323 800401	3568.50 1617.79	0.1395E+16 0.6323E+15	0.76 0.73	0.26 0.23	0.27	0.70 0.00	14.99 9.10	1.08	0.93	0.86 1.34	5.08 4.77	36 36
800404 800616	0.00 1082.66	0.0000E+00 0.4232E+15	0.00	0.00 0.23	0.00	0.00	0.00	0.00	0.00	0.00	0.00	26 36
800621 800706	129.16 524.45	0.2050E+14 0.2050E+15	0.35	0.11 0.24	0.10	0.00	2.04	0.57	1.74	2.19	4.08	36
801203	5289-31 346-55	0.2067E+16 0.1355E+15	0.88	0.22	0.34	0.00	14.34	1.15	0.87	0.74	5.10	36 36
810306 810328	0.00	0.0000E+00 0.2562E+15	0.00	0.00 0.21	0.00 0.21	0.00	1.01 3.18	0.80	1.25	1.47	3.80 4.30	36 36
810410 810708	812.62 697.39	0.3176E+15 0.2726E+15	0.90 0.59	0.24 0.17	0.26 0.14	0.00	2.76 4.91	1.08 1.17	0.93 0.85	0.86 0.70	4.35 4.64	36 36
810718 810803	87+61 1728-45	0.3425E+14 0.6756E+15	0.46	0.18	0.09	0.00	1.77 4.81	0.82	1.21	1.40	4.06	36 36 20
811205	536.09	0.2095E+15 0.5134E+15	0.13	0.29	0.22	0.00	2.68	0.73	1.38	1.68	4.21	36
820220 820224	0.00 82.51	0.0000E+00 0.3225E+14	0.00 0.49	0.00 0.11	0.00 0.19	0.00	0.00 0.64	0.00 0.82	0.00	0.00	0.00 3.61	36 36
820320 820627	0.00	0.0000E+00 0.0000E+00	0.00	0.00	0.00	0.00	1.74 0.00	0.98	1.03	1.05	4.10 0.00	36 36
820701 830419	784.38 5087.09	0.3066E+15 0.1988E+16	0.80	0.28	0.21	0.00	3.66 21.63	1.08	0.93	0.86	4.47 5.16	36 36
830425 830525 830618	8285+48	0.3238E+16	0.00	0.00	0.00	0.00	22.39	1.02	0.98	0.95	5.23	36
830628 830720	1326-86 0-00	0.5186E+15 0.0000E+00	0.68	0.19	0.20	0.52	7.91 1.97	0.95 0.90	1.05	1.10	4.75	36 36
830804 831203	931.00 83.82	0.3639E+15 0.3276E+14	0.71 0.45	0.19 0.14	0.19 0.12	0.00 0.00	4.62 1.02	0.95 0.82	1.05 1.21	1.10 1.40	4.51 3.82	36 36
831207 840512	680.22 3827.95	0.2659E+15 0.1496E+16	0.77	0.14 0.26	0.24	0.00	2.96 9.54	1.00	1.00	1.00	4.34	36 36
840612 840616 841027	2220+65	0.8680E+15	1.04	0.00	0.00	0.00	6.06	1.38	0.73	0.00	4.84	36
841102 841201	4560.54	0.1783E+16 0.0000E+00	1.00	0.22	0.27	0.00	15.15	0.93	1.08	1.16	5.02	36 36
841206 850430	4157.05 228.36	0.1625E+16 0.8926E+14	1.00	0.23 0.19	0.29 0.15	0.00 0.46	12.43	0.98 0.95	1.03	1.05	4.95 4.07	36 36
850508 850603	7788.50 314.12	0.3044E+16 0.1228E+15	0.89 0.50	0.26 0.11	0.25 0.09	0.00 0.47	23.80 2.69	1.10 0.95	0.91 1.05	0.82	5.29 4.28	36 36
850607	0.00	U.0000E+00	0.00	0.00	0,00	0.00	1.80	0,90	1.11	1.22	4.09	36

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Date	(	Moment (N m)	array - pro Duration (s)	rau uanu Rise time	fall time	pP-P time	1/2 Pk-Pk (nm)	Period (s)	Frequency (Hz)	Gain	Ê
				(<)	(>)	(>)					
851024	00.00	0.0000E+00	0.00	00.00	0.00	00.0	0.00	0.00	00.00	0.00	0.00
851026	2265.49	0.8855E+15	1.09	0.31	0.36	0.0	5.14	1.52	0.66	0.35	4.85
851124	624.51	0.2441E+15	0.89	0.21	0.20	0.0	2,92	1.10	0.91	0.82	4.38
851126	6587.55	0.2575E+16	0.98	0.30	0.33	00.0	15.77	1.00	1.00	1.00	5.07
860426	86.86	0.3395E+14	0.39	0.12	0.14	0.39	1.79	0.75	1.33	1.60	4.04
860506	216.44	0.8460E+14	0.47	0.13	0.08	0.00	1.89	0.75	1.33	1.60	4.07
860527	199.08	0.7781E+14	0.56	0.11	0.12	0.00	1.82	0.82	1.21	1.40	4.07
860530	4350.69	0.1701E+16	0.89	0.24	0.35	0.00	13.58	0.98	1.03	1.05	4.99
861112	1209.53	0.4728E+15	0.80	0.26	0.28	0.00	6.27	0.00	1.11	1.22	4.63
861206	213.10	0.8329E+14	0.56	0.17	0.11	0.00	1.76	0.70	1.43	1.75	4.03
861210	1706.51	0.6670E+15	1.15	0.31	0.34	0.0	4.80	1.35	0.74	0.49	4.73
870505	151.86	0.5936E+14	0.45	0.17	0.10	0.00	1.57	0.77	1.29	1.53	3.99
870520	3002-84	0.1174E+16	0.95	0.21	0.30	0.00	9.98	1.05	0.95	0.90	4.89
870606	0.00	D.0000E+00	0.0	0.0	0.00	0.0	0.39	0.75	1.33	1.60	3.78
870621	1182.82	0.4623E+15	0.85	0.21	0.22	00.00	4.10	0.95	1.05	1.10	4.46
871023	3325.26	0.1300E+16	0.96	0.28	0.28	0.00	9.75	0.93	1.08	1.16	4.83
871105	2357.06	0.9213E+15	0.88	0.26	0.25	0.0	8.93	0.88	1.14	1.27	4.77
871119	5868.32	0.2294E+16	1.00	0.26	0.33	00.0	18.73	0.98	1.03	1.05	5.13
871129	363.53	0.1421E+15	0.63	0.27	0.13	0.0	1.64	0.95	1.05	1.10	4.06
880511	1995.53	0.7800E+15	0.93	0.17	0.24	0.00	7.70	0.98	1.03	1.05	4.75
880525	6059.10	0.2368E+16	0.98	0.25	0.23	0.0	15.16	1.17	0.85	0.70	5.13
880616	202.61	0.7919E+14	0.52	0.16	0.11	0.00	1.02	0.80	1.25	1.47	3.81
880623	1193.31	0.4664E+15	0.69	0.26	0.17	0.00	7.30	0.85	1.18	1.34	4.68
881105	1782.82	0.6968E+15	0.80	0.24	0.20	0.0	7.02	1.13	0.89	0.78	4.78
881123	2320.81	0.9071E+15	0.81	0.23	0.18	0.0	8.15	1.15	0.87	0.74	4.85
890603	1735.12	0.6782E+15	0.81	0.24	0.20	0.00	6.30	0.98	1.03	1.05	4.66
891024	2413.34	0.9433E+15	0.94	0.18	0.28	0.0	8.69	1.05	0.95	0.90	4.83
891031	1862.94	0.7282E+15	0.80	0.25	0.22	0.00	8.19	0.82	1.21	1.40	4.72
891120	1100.79	0.4303E+15	0.73	0.23	0.21	0.00	4.64	0.95	1.05	1.10	4.52
*	0 - 147 0 24	CONF_11				7					
			P0-000-04	102 II D		•					

K=0.77 *p*1=2400.0kg m⁻¹ v1=3600.0km s⁻¹ 4

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r.m.s. noise	-0000 	0.00 0.200	0.42	0.35	0.27	.00 .00 .00 .00	0.36	0.00	0.61	0.39	0.40		0.34	0.24	0.26	0.29				0.4.0	- 43 - 643 - 643			- 00 - 00 - 00		0.27	0.32
7.a.s. 9-185	0.00 0.00 17.0 0.02 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.00 4.59	0.62 0.73 0.87	1.36	6.91 0.79		9.99 9.99 9.99	0.00	0.77	5.12 3.99	0.35	0.40	- 38 - 38 - 36 - 36		1.37	0.34	80	4.83			1.22	26.0		- 0. 98. 98.		0.49 0.49	0.48
7.m.s. 3-155	0.033 0.033 0.022	9.15 9.15	0.85 0.97	0.71	14.63		2.13 2.13	5000 5000	1.11 0.72	6.18 4.62	0.48 0.33	0.55	0.39			0.41	0.00	- <del>-</del>	9.58 8.58	385		80. 10	200 00	0.49	4.84 0.00 70	0.48 6.40	0.67
7.8.5 3-95	0.00 1.064 1.06	0.00 12.07	1.13	0.84	19.36 1.15	0.62	5.70 2.42	0.00	1.38 0.89	7.18	0.52	0.01	1	- 20	288	0.52	0.00	- <del>-</del>		200 200 200		6.00		- <u>-</u>	100	0.48	0.78
ſ.m.s. 0-15s	0.00 1.11 0.00 0.00 0.00	1.22	0.92 1.09 80.1	0.90	17.09	0.50	0.40 0.40 0.40	0.00 2.32	1.11 0.76	5.99 5.21	0.56	0.73	1.67 0.44 0.0	0.71		0.45 645	0.00	800	8.24 8.24	0.00 0.00 0.00		1.08		0.54		0.56	0.94
г.ш.s. 0-95	0.00 1.28 1.28 0.00	1.20 1.20	1.06 1.26	1.07	21.24	0.51	6.41 2.81	0.00 2.63	1.30 0.89	8.06 6.03	0.51	0.82			8 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	0.51	0.00	6.14		5. 28 2		1.05	4.0 7.00 7.00	0.62	0.00	0.61	1.04 0.86
r.m.s. 0-65	(mc) 1.71 1.43 0.80	0.00 14.33 1.26	1.21	2.13	22.84 1.36	200 200 200 200 200	2.92	0.00 2.96	1.29	8.02 10 10 10	0.71	80.1 96.0 96.0	9255 0-20 0-20			0.51		20.7	885	000 000 000 000 000 000 000 000 000 00	212			0.02 0.02	200	0.40	1.19
band r.m.s. 0-3s	(m) 10000 1000 1000 1000 1000 1000 1000 1	0.00 15.01 1.44	1.17	2.27	24.58 1.40	0.57 2.0	3.45	3.07	1.13 0.90	9.58 7.10	0.63	1.20	0.59 0.59	, 00 00 00		0.48	0.00	8. 9. 9. 9. 9. 9. 9. 9. 9. 9. 9. 9. 9. 9.	02.00	0 8 9 8 9 8 9 8 9 8 9 8 9 8 9 8 9 8 9 8				4-0-1 10-69		0.80	1.42 0.96
0.5-4.0Hz   mb	4.66 0.00 4.37	5.25 4.18	4.23 4.30 4.30	4.57	5.66 4.33	3.93 100 100 100	5.13	0.00	4.18 4.16	ນ. ເບີ້ອງ ເບີ້ອງ	4.11 3.84	4.67 4.67	3.84	4.41 4.04	4 4 C	3.84	00.00	600	20 20 20 20 20 20 20 20 20 20 20 20 20 2		4 4 c	4.62		3.91		4 30 4 30	4.16
ns in the Gain	0.39 0.00 1.54	0.00	1.53	1.53	1.34	1.54 1.47 7.43	0.52	0.00	1.60	0.41	1.27	0.20	1.68 1.68		1.47				01.0				200 -00	60-2 - 50-2	0.00	0.25	0.21
Observatio Frequency (Hz)	0.68 0.00 1.29	0.00	1.38	1.129	0.78 1.18	1.25	0.75	0.00	1.33	0.63	1.14	0.54	0.66 1.38 0.1	1.48		1.00	00.00	1.25	1.05	.21	0.77	0.56	800-0 00-0 00-0	1.67	81.1 00.0	0.58	0.55
a array - Period (s)	1.48 0.00 0.77 0.77	0.00	0.73	0.88	1.27 0.85	0.80 80.0 74.1	1.33 0.80	0.75	0.75	1.45 1.48	0.88		267.0					800	500	0.04		28; 28;		- 0.0		1.73	1.00
Warramung. 1/2 Pk-Pk (nm)	3.48 0.00 3.74	0.00 27.24 2.46	2.77 3.17 2.92	5.61 0.61	44.62 3.24		12.60 8.07	0.00 5.59	2.43 2.35	16.37 12.49	1.94	2.82 2.83 2.83	3. 43 1. 13	••••• •••• ••••	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0.03	0.00	19.56	18.68			2.18	, 00 , 00 , 00 , 00 , 00 , 00 , 00 , 00	1.38	0.00 0.00	1.41	2.65
Table 5A Date	770706 780227 780322 780322	780726 781130 781219	790301 790309 790324	790618	790725	800223 800223	800323 800323	800404 800616	800621 800706	800719 801203	810227 810306	810410	810718 810718	811803 811111	811208 811208	820224 820224	820627	830419	830525	830628 830628	830804 830804	831207 831207	840612	841027 841027	841102 841201	850430 850430	850603 850603

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Table 5A	(cont`d)	Warramun	ga annay - Ö	bservatio	ns in the	0.5-4.0Hz	band						
Date	1/2 Pk-Pk	Period	Frequency	Gain	мъ	r.m.s.	C.M.S.	r.m.s.	r.m.s.	r•m•s•	r.m.s.	r.m.s.	r.m.s.
	(mm)	(5)	(Hz)			0-3s	0-6s	0-9s	0-15s	3-9s	3-15s	9-18s	noise
						(mm)	(nm)	(הח)	(mm)	(mm)	(nm)	(nm)	(nm)
851024	0.00	0.00	0.00	D.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
851026	5.65	0.85	1.18	1.34	4.57	3.07	2.58	2.52	2.33	2.20	2.11	2.01	0.27
851124	2.39	0.95	1.05	1.10	4.23	1.13	1.13	0.98	0.80	0.89	0.69	0.38	0.28
851126	13.78	1.48	0.68	0.39	5.25	8.11	7.51	6.54	6.05	5.60	5.41	4.41	0.30
860426	1.45	0.85	1.18	1.34	3.98	0.82	0.83	0.72	0.64	0.66	0.59	0.48	0.37
860506	1.49	0.82	1.21	1.40	3.98	0.76	0.67	0.63	0.53	0.55	0.46	0,36	0.29
860527	1.32	1.77	0.56	0.23	4.39	0.67	0.57	0.65	0.62	0.64	0.60	0.53	0.37
860530	12.06	0.82	1.21	1.40	4.89	6.17	5.80	5.51	4.71	5.14	4.27	3.16	0.28
861112	5.87	0.82	1.21	1.40	4.58	2.78	2.68	2.48	2.08	2.32	1.86	1.22	0.27
861206	1.74	1.02	0.98	0.95	4.12	0.93	0.85	0.74	0.69	0.63	0.61	0.65	0.28
861210	3.88	1.10	0.91	0.82	4.51	2.28	2.02	1.87	1.88	1.62	1.77	1.69	0.36
870505	1.45	0,80	1.25	1.47	3.96	0,60	0.55	0.57	0.57	0.55	0.57	0.55	0.43
870520	8.57	0,93	1.08	1.16	4.77	4.78	4.56	3.95	3.77	3.45	3.46	2,95	0.26
870606	1.34	0.85	1.18	1.34	3.94	0,63	0.61	0.59	0.55	0.57	0.53	0.50	0.31
870621	3.26	0.77	1.29	1.53	4.31	1.90	1.70	1.52	1.47	1.28	1.34	1.26	0.27
871023	8.01	0.85	1.18	1.34	4.72	4.67	4.31	3.88	3.75	3,42	3.48	3.13	0.27
871105	8.06	0.75	1.33	1.60	4.70	3.92	3.52	3.12	2.71	2.63	2.31	1.68	0.24
871119	16.96	0.85	1.18	1.34	5.04	8.19	8.03	7.14	6.20	6,56	5.60	4.01	0.37
871129	1.60	0.85	1.18	1.34	4.02	0.73	0.68	0.68	0.65	0.66	0.63	0.56	0.33
880511	6.02	0.90	1.11	1.22	4.61	2.92	2.82	2.65	2.64	2.51	2.57	2.55	0.45
880525	11.56	1.00	1.00	1.00	4.93	6.95	6.66	5.99	5.04	5.45	4.43	2.79	0.37
880616	1.13	0.80	1.25	1.47	3.85	0.57	0.46	0.50	0.49	0.47	0-47	0.43	0.32
880623	5.65	0.77	1.29	1.53	4.55	2.67	2.44	2.23	2.07	1.97	1.89	1.54	0.46
881105	6.20	0.65	1.54	1.91	4.57	3.32	2.71	2.53	2.08	2.02	1.62	1.02	0.23
881123	6.66	1.02	0.98	0.95	4.70	4.01	3.78	3.48	2.93	3.17	2.59	1.73	0.23
890603	5.39	0.75	1.33	1.60	4.52	2.82	2,59	2,30	2.19	1.99	2.00	1.74	0.37
891024	6.82	0.95	1.05	1.10	4.68	3.75	3.66	3.48	3.18	3.34	3.03	2.76	0.32
891031	7.26	0.80	1.25	1.47	4.66	3.36	2.62	2.41	2.11	1.76	1.65	1.53	0.24
891120	4.40	0.75	1.33	1.60	4.43	2.36	2.06	2.01	1.89	1.81	1.75	1.43	0.42

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Date   L/2   Press   Pr	Table 6A	Warramunga	array -	Observations	in the	1.0-4.0Hz	band							
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	Date	1/2 Pk-Pk	Period	Frequency	Gain	mb	r.m.s.	r.m.s.	r.m.s.	r.m.s.	r.m.s.	r.m.s.	r.m.s.	r.m.s.
TYTOTE   L.63   L.54   L.91   L.63   L.84   L.84 <thl.84< th="">   L.84   L.84   <t< td=""><td></td><td>(nn)</td><td>(s)</td><td>(Hz)</td><td></td><td></td><td>0-3s</td><td>0-6s</td><td>0-9s</td><td>0-15s</td><td>3-9s</td><td>3-15s</td><td>9-18s</td><td>noise</td></t<></thl.84<>		(nn)	(s)	(Hz)			0-3s	0-6s	0-9s	0-15s	3-9s	3-15s	9-18s	noise
1   1   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0   0	770700		0.05	1 54	1 01	4 05	(0m)		()		(0, m)	(nm)	(∩m)	(nm)
196352   0.75   0.75   0.75   0.75   0.77   0.657   0.677   0.677   0.677   0.677   0.677   0.677   0.677   0.677   0.677   0.677   0.677   0.677   0.677   0.677   0.677   0.677   0.677   0.677   0.677   0.677   0.677   0.677   0.677   0.677   0.677   0.677   0.677   0.677   0.677   0.677   0.677   0.677   0.677   0.677   0.677   0.677   0.677   0.677   0.677   0.677   0.677   0.677   0.677   0.677   0.677   0.677   0.677   0.677   0.677   0.677   0.677   0.677   0.677   0.677   0.677   0.677   0.677   0.677   0.677   0.677   0.677   0.677   0.677   0.677   0.677   0.677   0.677   0.677   0.677   0.677   0.677   0.677   0.677   0.677   0.677   0.677   0.677   0.677   0.677   0.677   0.677   0.6	700007	1.89	0.65	1.54	1.91	4.05	0.90	0.00	0.88	0.74	0.87	0.69	0.41	0.25
180716   1.23   0.653   0.54   0.47   0.40   0.44   0.58   0.24   0.78     180716   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   <	780227	0.00	0.00	1 22	1 61	4 22	1 27	1.19	1 00	0.00	0.00	0.00	0.57	0.00
180726   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   <	780322	2.13	0.65	1.54	1.91	3.90	0 53	0.54	0.47	0.32	0.90	0.26	0.25	0.10
$ \begin{array}{c} 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 \\ 16113 $	780726	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.20	0.13
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	781130	16.13	0.95	1.05	1.10	5.06	7.71	8,25	7.36	5.97	7.17	5.45	2.84	0.12
193001 2.09 0.75 1.33 1.60 4.11 0.86 0.74 0.64 0.67 0.57 0.41 0.16   193039 2.12 0.70 1.43 1.75 4.01 0.88 0.180 0.178 0.178 0.178 0.175 0.175 0.175 0.175 0.175 0.175 0.175 0.175 0.175 0.175 0.175 0.175 0.175 0.175 0.175 0.175 0.175 0.175 0.175 0.175 0.175 0.175 0.175 0.175 0.175 0.175 0.175 0.175 0.175 0.175 0.175 0.175 0.175 0.171 0.174 0.163 0.183 0.183 0.183 0.183 0.183 0.183 0.183 0.183 0.183 0.183 0.183 0.183 0.183 0.183 0.183 0.183 0.183 0.168 0.176 0.111 0.133 0.168 0.176 0.124 0.423 0.433 0.229 0.30 0.151 0.333 0.233 0.249 0.333 0.249 0.30 0.151 <t< td=""><td>781219</td><td>1.88</td><td>0.70</td><td>1.43</td><td>1.75</td><td>4.05</td><td>0.89</td><td>0.85</td><td>0.79</td><td>0.80</td><td>0.73</td><td>0.78</td><td>0.73</td><td>ŏ. oš</td></t<>	781219	1.88	0.70	1.43	1.75	4.05	0.89	0.85	0.79	0.80	0.73	0.78	0.73	ŏ. oš
T93039   2.12   0.70   1.43   1.75   4.11   1.01   0.65   0.79   0.63   0.75   0.75   0.75   0.75   0.75   0.75   0.75   0.75   0.75   0.75   0.75   0.75   0.75   0.75   0.75   0.75   0.75   0.75   0.75   0.75   0.75   0.75   0.75   0.75   0.75   0.75   0.75   0.75   0.75   0.75   0.75   0.75   0.75   0.75   0.75   0.75   0.75   0.75   0.75   0.75   0.75   0.75   0.75   0.75   0.75   0.75   0.75   0.75   0.75   0.75   0.75   0.75   0.75   0.75   0.75   0.75   0.75   0.75   0.75   0.75   0.75   0.75   0.75   0.75   0.75   0.75   0.75   0.75   0.75   0.75   0.75   0.75   0.75   0.75   0.75   0.75   0.75   0.75   0.75   0.75   0.75   0.75   <	790301	2.09	0.75	1.33	1.60	4.11	0.86	0.81	0.74	0.64	0.67	0.57	0.41	0.16
'90324   2.03   0.70   1.43   1.75   4.09   0.87   0.60   0.78   0.78   0.75   0.75   0.643   0.643   0.643   0.643   0.75   0.75   0.75   0.643   0.75   0.75   0.75   0.75   0.75   0.643   0.75   0.643   0.75   0.643   0.75   0.643   0.75   0.643   0.75   0.643   0.75   0.613   0.642   0.76   0.53   0.623   0.76   0.53   0.623   0.623   0.623   0.623   0.623   0.623   0.623   0.623   0.623   0.623   0.623   0.623   0.623   0.623   0.623   0.623   0.623   0.623   0.623   0.623   0.623   0.623   0.623   0.623   0.623   0.623   0.623   0.623   0.623   0.623   0.623   0.623   0.623   0.623   0.623   0.623   0.623   0.623   0.623   0.623   0.623   0.623   0.623   0.623   0.623   0.63	790309	2.12	0,70	1.43	1.75	4.11	1.01	0.85	0.90	0.79	0.85	0.72	0.54	0.13
TSGE18 2.31 0.687 1.483 4.14 0.933 0.84 0.765 0.644 0.165 0.644 0.165 0.541 0.838 0.14   TSGE78 2.3177 0.72 1.23 1.53 4.10 0.931 0.440 1.136 1.241 1.262 1.73 3.477 0.225   TSGE78 2.347 0.73 1.23 1.53 4.108 0.949 0.422 0.480 0.432 0.480 0.432 0.480 0.432 0.440 0.432 0.440 0.432 0.440 0.422 0.440 0.432 0.421 0.425 0.430 0.422 0.411 0.433 0.441 0.430 0.432 0.421 0.430 0.432 0.421 0.430 0.432 0.421 0.431 0.432 0.431 0.432 0.431 0.432 0.431 0.432 0.432 0.431 0.432 0.432 0.431 0.432 0.431 0.432 0.432 0.431 0.432 0.441 0.433 0.431 0.432 0.441 0.433 0.431 0.432 0.431	790324	2.03	0.70	1.43	1.75	4.09	0.87	0.80	0.79	0.78	0.75	0.75	0.69	0.08
Type   J. H   L. H <thl< th="">   L. H   L. H   L.</thl<>	790618	2.31	0.68	1.48	1.83	4.14	0.93	0.84	0.76	0.64	0.66	0.54	0.39	0.14
190763   22.01   0.997   12.49   1.433   3.10   1.034   1.033   1.035   0.145   1.042   1.448   0.125   0.142   0.142   0.142   0.142   0.142   0.142   0.142   0.142   0.142   0.142   0.142   0.142   0.142   0.142   0.142   0.142   0.142   0.142   0.142   0.142   0.142   0.142   0.142   0.142   0.142   0.142   0.142   0.142   0.142   0.142   0.142   0.142   0.142   0.142   0.142   0.142   0.142   0.142   0.142   0.143   0.143   0.143   0.142   0.143   0.142   0.143   0.142   0.143   0.123   0.143   0.123   0.143   0.114   0.020   0.114   0.123   0.114   0.114   0.114   0.114   0.114   0.114   0.114   0.114   0.114   0.114   0.114   0.114   0.114   0.114   0.114   0.114   0.114   0.114   0.114 <th< td=""><td>790629</td><td>3.18</td><td>0.77</td><td>1.29</td><td>1.53</td><td>4.37</td><td>1.38</td><td>1.40</td><td>1.30</td><td>1.24</td><td>1.26</td><td>1.21</td><td>1.00</td><td>0.13</td></th<>	790629	3.18	0.77	1.29	1.53	4.37	1.38	1.40	1.30	1.24	1.26	1.21	1.00	0.13
1791125 1.23 1.43 1.43 1.43 1.43 0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.44	790725	23.11	0.82	1.21	1.40	5-18	11.60	11.80	10.83	8.14	10.42	181	3.85	0.12
add2223   1.102   0.77   1.23   1.433   3.860   0.39   0.34   0.32   0.22   0.22   0.23   0.23   0.23   0.24   0.35   0.23   0.23   0.23   0.23   0.35   0.32   0.31   0.23   0.33   0.51   0.23   0.35   0.32   0.31   0.23   0.33   0.52   0.31   0.23   0.32   0.31   0.23   0.33   0.51   0.32   0.31   0.23   0.35   0.32   0.31   0.23   0.35   0.32   0.31   0.23   0.35   0.35   0.35   0.32   0.31   0.72   0.48   0.41   0.42   0.35   0.41   0.42   0.42   0.42   0.43   0.43   0.43   0.42   0.42   0.42   0.33   0.41   0.42   0.43   0.42   0.43   0.42   0.42   0.42   0.42   0.42   0.42   0.43   0.43   0.43   0.43   0.43   0.43   0.43   0.43   0.43	791122	2.04	0.72	1 29	1.00	3 00	0.34	0.53	0.92	0.13	0.30	0.13	0.20	0.22
ab0333 0.62 0.62 0.63 1.65 0.55 0.55 0.52 0.51 0.29 0.50 0.15   b00323 8.53 0.73 1.38 1.68 4.72 4.16 4.065 3.76 3.24 3.55 2.96 2.15 0.11   b00401 5.81 0.73 1.38 1.68 4.55 2.63 2.28 2.23 1.91 1.93 1.68 1.14 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00	800223	1.02	0.77	1.29	1.53	3.80	0.39	0.34	0.32	0.28	0.27	0.35	0.20	0.14
800323 8.53 0.73 1.38 1.68 4.72 4.16 4.06 3.76 3.24 3.55 2.36 2.15 0.11   800401 5.81 0.73 1.38 1.68 4.55 2.63 2.28 2.23 1.91 1.99 1.68 1.40 0.00   800615 3.90 0.68 1.44 1.83 4.37 1.82 1.88 0.69 0.73 0.93 0.72 0.46 0.39   800761 1.47 0.65 1.54 1.91 4.02 0.78 0.88 0.489 0.73 0.93 0.72 0.45 0.39   800705 1.47 0.65 1.54 1.91 4.63 3.93 3.78 3.53 3.10 4.32 2.47 0.22 0.21 0.16   810227 1.83 0.60 1.63 0.64 0.63 0.52 0.36 0.33 0.29 0.31 0.27 0.22 0.16 1.11   810221 1.83 0.62 0.53 0.43 0.39 0.31 0.21 0.63 </td <td>800223</td> <td>0.82</td> <td>0.63</td> <td>1.60</td> <td>2.00</td> <td>3.69</td> <td>0.41</td> <td>0.35</td> <td>0.35</td> <td>0.32</td> <td>0.31</td> <td>0.29</td> <td>0.30</td> <td>0.15</td>	800223	0.82	0.63	1.60	2.00	3.69	0.41	0.35	0.35	0.32	0.31	0.29	0.30	0.15
800401 5.61 0.73 1.28 1.68 4.55 2.63 2.28 2.23 1.91 1.99 1.68 1.14 0.00   800404 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00	800323	8.53	0.73	1.38	1.68	4.72	4.16	4.08	3.76	3.24	3.55	2.96	2,15	0.11
B00404 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00	800401	5.81	0.73	1.38	1.68	4.55	2.63	2.28	2.23	1.91	1.99	1.68	1.14	0.09
800616 3.90 0.68 1.48 1.63 4.37 1.82 1.68 1.68 1.46 1.61 1.38 1.04 0.13   800521 1.77 0.65 1.54 1.91 4.02 0.78 0.68 0.73 0.53 0.71 0.53 0.748 0.32 0.22 0.48 0.32 0.22 0.48 0.32 0.22 0.48 0.32 0.22 0.48 0.32 0.23 0.77 3.11 0.17 0.13 0.48 0.32 0.23 0.27 0.44 0.32 0.23 0.23 0.23 0.23 0.23 0.23 0.23 0.23 0.23 0.23 0.23 0.23 0.23 0.23 0.23 0.23 0.23 0.23 0.23 0.23 0.23 0.23 0.23 0.23 0.23 0.23 0.23 0.23 0.23 0.23 0.23 0.23 0.23 0.23 0.23 0.23 0.23 0.31 0.32 0.33 0.11 0.11 0.107 0.33 0.33 0.61 0.55 0.55 0.57	800404	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
800621 1.77 0.65 1.54 1.91 4.02 0.78 0.88 0.73 0.93 0.72 0.46 0.88   800706 1.41 0.80 1.65 1.54 1.33 3.95 0.60 0.61 0.53 0.51 0.53 0.72 0.46 0.32 0.72 0.46 0.32 0.20   800718 1.04 0.80 1.25 1.47 3.95 0.60 0.45 0.43 0.27 0.21 0.22 0.22 0.22 0.22 0.21 0.21 0.21 0.21 0.21 0.21 0.21 0.22 0.22 0.21 0.21 0.21 0.21 0.21 0.21 0.21 0.21 0.21 0.21 0.21 0.21 0.21 0.21 0.21 0.21 0.21 0.21 0.21 0.21 0.21 0.21 0.21 0.21 0.21 0.21 0.21 0.21 0.23 0.21 0.21 0.21 0.21 0.21 0.21 0.21 0.21 0.21 0.21 0.21 0.21 0.21 0.21	800616	3.90	0.68	1.48	1.83	4.37	1.82	1.88	1.68	1.48	1.61	1.38	1.04	0.13
B00/106 1.41 0.40 1.25 1.44 3.95 0.61 0.51 0.59 0.449 0.32 0.70   B00/113 10.76 0.68 1.49 1.81 4.88 5.33 4.89 4.13 4.32 3.77 3.11 0.17 3.32 0.75 3.11 0.17 0.32 0.75 3.11 0.17 0.32 0.77 3.11 0.17 0.32 0.77 3.11 0.17 0.12 0.11 0.17 0.12 0.11 0.17 0.12 0.11 0.17 0.12 0.11 0.17 0.12 0.11 0.17 0.12 0.11 0.17 0.12 0.11 0.17 0.12 0.11 0.17 0.12 0.13 0.28 0.25 0.24 0.24 0.15 1.01 1.04 1.07 0.93 0.81 0.16 0.55 0.51 0.54 0.15 0.15 0.15 0.15 0.15 0.15 0.16 0.15 0.15 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 <td>800621</td> <td>1.77</td> <td>0.65</td> <td>1.54</td> <td>1.91</td> <td>4.02</td> <td>0.78</td> <td>0.88</td> <td>0.88</td> <td>0.73</td> <td>0.93</td> <td>0.72</td> <td>0.46</td> <td>0.38</td>	800621	1.77	0.65	1.54	1.91	4.02	0.78	0.88	0.88	0.73	0.93	0.72	0.46	0.38
abounds 1.0.10 1.0.10 1.0.10 1.0.10 1.0.11 0.11 0.11 0.11 0.11 0.11 0.11 0.11 0.11 0.11 0.11 0.11 0.11 0.11 0.11 0.11 0.11 0.11 0.11 0.11 0.11 0.11 0.11 0.11 0.11 0.11 0.11 0.11 0.11 0.11 0.11 0.11 0.11 0.11 0.11 0.11 0.11 0.11 0.11 0.11 0.11 0.11 0.11 0.11 0.11 0.11 0.11 0.11 0.11 0.11 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.	800706	1.41	0.80	1.25	1.47	3-95	0.60	0.61	0.59	0.51	0.59	0.48	0.32	0.20
B016327 6.63 0.80 1.25 1.47 3.92 0.33 0.47 3.43 3.34 3.34 2.23 2.21 0.16   B10306 0.75 0.80 1.25 1.47 3.67 0.33 0.29 0.31 0.27 0.22 0.31   B10306 0.73 1.25 1.47 3.67 0.36 0.35 0.33 0.29 0.31 0.27 0.22 0.31 0.27 0.22 0.31 0.27 0.22 0.31 0.27 0.22 0.31 0.21 0.22 0.31 0.27 0.22 0.31 0.21 0.27 0.22 0.31 0.22 0.31 0.22 0.31 0.22 0.33 0.31 0.28 0.25 0.24 0.24 0.15 5 5 0.41 0.53 0.55 0.41 0.50 0.53 0.55 0.41 0.50 0.53 0.55 0.41 0.51 0.44 0.51 0.44 0.51 0.44 0.51 0.44 0.51 0.44 0.51 0.44 0.51 0.44 0.51	800719	10.10	0.68	1.48	1.03	4+81	3.34	4.33	4.63	4.13	4.32	3.11	3.11	0.11
816366 1.75 0.80 1.25 1.47 3.67 0.36 0.33 0.23 0.23 0.43 0.627 0.622 0.63 0.637 0.627 0.627 0.627 0.627 0.627 0.627 0.627 0.627 0.637 0.637 0.637 0.637 0.637 0.637 0.637 0.637 0.637 0.637 0.637 0.637 0.637 0.637 0.637 0.637 0.637 0.637 0.637 0.637 0.637 0.637 0.637 0.637 0.637 0.637 0.637 0.637 0.637 0.637 0.637 0.637 0.637 0.637 0.637 0.637 0.637 0.637 0.637 0.637 0.637 0.637 0.637 0.637 0.637 0.637 0.637 0.637 0.637 0.637 0.637 0.637 0.637 0.637 0.637 0.637 0.637 0.637 0.637 0.637 0.637 0.637 0.637 0.637 0.637 0.637 0.637 0.637 0.637 0.637 0.637 0.637 0.637 0.637 <td>801203</td> <td>0.23</td> <td>0.60</td> <td>1.04</td> <td>1.47</td> <td>4.03</td> <td>3.33</td> <td>0.47</td> <td>3.33</td> <td>0.27</td> <td>3.32</td> <td>2.83</td> <td>2+41</td> <td>0.11</td>	801203	0.23	0.60	1.04	1.47	4.03	3.33	0.47	3.33	0.27	3.32	2.83	2+41	0.11
810328 2.03 0.73 1.38 1.68 4.03 0.73 0.74 0.69 0.58 0.63 0.52 0.43 0.39 0.61 0.56 0.58 0.63 0.52 0.43 0.39 0.61 0.56 0.50 0.45 0.43 0.39 0.61 0.56 0.45 0.43 0.39 0.61 0.57 0.43 0.42 0.42 0.42 0.42 0.42 0.42 0.42 0.42 0.43 0.42 0.43 0.42 0.43 0.43 0.43 0.42 0.43 0.42 0.43 0.42 0.43 0.44 0.43 0.42 0.43 0.44 0.43 0.44 0.43 0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.45 0.47 0.43 0.44 0.45 0.47 0.43 0.44 0.45 0.47 0.43 0.44 0.45 0.47 0.43 0.47 0.43 0.44 0.43 0.43 0.43 0.43 0.43 0.43 0.44 0.44	810306	0.75	0.80	1.25	1.47	3.67	0.36	0.35	0.33	0.29	0.31	0.27	0.22	0.16
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	810328	2.03	0,73	1.38	1.68	4.09	0.79	0.74	0.69	0.58	0.63	0.52	0.36	0.13
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	810410	1.42	0.63	1.60	2.00	3.93	0.61	0.56	0.50	D-45	0.43	0.39	0.31	0.12
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	810708	3.07	0.65	1.54	1.91	4.26	1.40	1.38	1.19	1.04	1.07	0.93	0.89	0.16
810803 3.00 0.68 1.48 1.83 4.26 1.20 1.17 1.10 1.01 1.05 0.96 0.75 0.15   811111 1.54 0.73 1.38 1.68 4.00 0.69 0.64 0.62 0.52 0.58 0.41 0.50 0.53 0.10   811205 1.65 0.73 1.38 1.68 4.00 0.69 0.64 0.62 0.52 0.58 0.41 0.50 0.53 0.10 0.10 0.10 0.10   820224 0.48 1.08 0.59 0.55 0.57 0.54 0.45 0.10   820227 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00	810718	0.97	0.68	1.48	1.83	3.77	0.39	0.34	0.31	0.28	0.25	0.24	0.24	0.15
811111 1.54 0.73 1.38 1.68 3.97 0.71 0.59 0.53 0.53 0.53 0.53 0.53 0.53 0.53 0.53 0.53 0.53 0.53 0.53 0.53 0.53 0.53 0.53 0.53 0.53 0.53 0.53 0.53 0.53 0.53 0.53 0.53 0.53 0.53 0.53 0.53 0.53 0.53 0.53 0.53 0.53 0.53 0.53 0.53 0.53 0.53 0.53 0.53 0.53 0.53 0.53 0.53 0.53 0.53 0.53 0.53 0.53 0.53 0.53 0.53 0.53 0.53 0.53 0.53 0.53 0.53 0.53 0.53 0.53 0.53 0.53 0.53 0.53 0.53 0.53 0.53 0.53 0.53 0.53 0.53 0.53 0.53 0.53 0.53 0.53 0.53 0.51 0.53 0.51 0.53 0.51 0.53 0.51 0.53 0.51 0.53 0.51 0.53 0.51 0.53	810803	3.00	0.68	1.48	1.83	4.26	1.20	1.17	1.10	1.01	1.05	0,96	0.75	0.15
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	811111	1.54	0.73	1.38	1.68	3+31	0.71	0.59	0.53	0.55	U-41	0.50	0.53	0.10
81020 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00	811203	1.60	0.13	1 54	1.00	4.00	2 16	1 07	1 70	1 59	1 55	1 29	1 10	0.14
B20224 0.48 1.08 0.93 0.86 3.59 0.22 0.23 0.22 0.13 0.16 0.10   B20220 1.22 1.30 0.77 0.54 4.11 0.62 0.58 0.55 0.57 0.54 0.45 0.20   B20270 1.22 1.30 0.77 0.54 4.11 0.62 0.58 0.55 0.57 0.54 0.45 0.20   B20627 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00	820220	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.10
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	820224	0.48	1.08	0.93	0.86	3.59	0.22	0.00	0.23	0.19	0.23	0.19	0.16	0.10
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	820320	1.22	1.30	0.77	0.54	4.11	0.62	0.58	0.59	0.55	0.57	0,54	0.45	0.27
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	820627	0.00	0.00	0.00	0.00	0.00	0,00	0.00	0.00	0.00	0.00	0.00	õ. 00	0.00
830419 13.72 0.70 1.43 1.75 4.92 5.89 4.91 4.46 4.43 3.53 3.98 3.99 0.15   830425 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.042 0.35	820701	2.44	0.75	1.33	1.60	4.18	0,93	1.03	0.93	0.83	0.93	0.81	0.63	0.11
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	830419	13.72	0.70	1.43	1.75	4.92	5.89	4.91	4.46	4.43	3.53	3,98	3.99	0.15
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	830425	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	830525	11.48	0.80	1.25	1.47	4.86	5.18	5.63	5.35	5-14	5.43	5.12	4.28	0.10
830628 5.01 0.15 1.33 1.60 4.49 2.22 1.39 2.06 1.11 1.11 1.56 0.63 0.24   830720 0.93 0.77 1.29 1.53 3.76 0.51 0.42 0.36 0.32 0.24 0.25 0.23 0.24   830720 0.93 0.77 1.29 1.53 3.76 0.51 0.42 0.36 0.32 0.24 0.25 0.23 0.24   830720 0.93 0.77 1.29 1.53 3.82 0.49 0.45 0.40 0.36 0.35 0.31 0.27 0.16   831207 1.38 0.90 1.11 1.22 3.97 0.73 0.63 0.60 0.67 0.55 0.63 0.23 0.13   840512 6.42 0.77 1.29 1.53 4.60 3.09 2.92 2.66 2.48 2.42 2.30 2.03 0.13   840612 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 <td>830618</td> <td>0.00</td> <td>0.00</td> <td>0.00</td> <td>1 60</td> <td>0.00</td> <td>0,00</td> <td>0.00</td> <td>0.00</td> <td>0.00</td> <td>0.00</td> <td>0.00</td> <td>0.00</td> <td>0.00</td>	830618	0.00	0.00	0.00	1 60	0.00	0,00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	830628	5.01	0.77	1.33	1.53	4.49	2.22	1.33	2.06	1.11	1.97	1.36	0.89	0.28
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	830804	2,21	0.88	1.14	1.27	4.17	1.13	1.11	0.36	0.95	0.24	0.23	0.23	0.24
831207 1.38 0.90 1.11 1.22 3.97 0.73 0.63 0.60 0.67 0.52 0.65 0.63 0.23   840512 6.42 0.77 1.29 1.53 4.60 3.09 2.92 2.66 2.48 2.42 2.30 2.03 0.10   840612 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00	831203	1,10	0.65	1.54	1.91	3.82	0.49	0.45	0.40	0.36	0.35	0.31	0.27	0.16
\$\$40512 6.42 0.77 1.29 1.53 4.60 3.09 2.92 2.66 2.48 2.42 2.30 2.03 0.13   \$\$40612 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.01 0.11 841201 0.42 0.31 0.51 0.44 0.40 0.36 0.34 0.31 0.28 0.11   \$\$41201 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 </td <td>831207</td> <td>1.38</td> <td>0,90</td> <td>1.11</td> <td>1.22</td> <td>3.97</td> <td>0.73</td> <td>0.63</td> <td>0.60</td> <td>0.67</td> <td>0.52</td> <td>0.65</td> <td>0.63</td> <td>0.23</td>	831207	1.38	0,90	1.11	1.22	3.97	0.73	0.63	0.60	0.67	0.52	0.65	0.63	0.23
840612 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00	840512	6.42	0.77	1.29	1.53	4.60	3.09	2.92	2.66	2.48	2.42	2.30	2.03	0.13
840616 3.16 0.88 1.14 1.27 4.32 1.37 1.32 1.20 1.22 1.12 1.18 1.22 0.19   841027 0.96 0.63 1.60 2.00 3.76 0.51 0.44 0.40 0.36 0.34 0.31 0.28 0.11   841021 0.025 0.65 1.54 1.91 4.79 4.84 4.90 4.45 3.76 4.25 3.43 2.52 0.13   841201 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00	840612	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
841027 0.96 0.63 1.60 2.00 3.76 0.51 0.44 0.40 0.36 0.34 0.31 0.28 0.11   841102 10.25 0.65 1.54 1.91 4.79 4.84 4.90 4.45 3.76 4.25 3.43 2.52 0.13   841201 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00	840616	3.16	0.88	1.14	1.27	4.32	1.37	1.32	1.20	1.22	1.12	1.18	1.22	0.19
841102 10.25 0.65 1.54 1.91 4.79 4.84 4.90 4.45 3.76 4.25 3.43 2.52 0.13   841201 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00	841027	0.96	0.63	1.60	2.00	3.76	0.51	0.44	0.40	0.36	0.34	0.31	0.28	0.11
941201   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   <	841102	10.25	0.65	1.54	1.91	4.79	4.84	4.90	4.45	3.76	4.25	3.43	2.52	0.13
841205 6.83 0.63 1.60 2.00 4.61 3.17 3.13 3.23 3.01 3.26 2.97 2.28 0.12   850430 1.03 0.70 1.43 1.75 3.80 0.39 0.42 0.37 0.34 0.36 0.33 0.26 0.14   850508 16.08 0.75 1.33 1.60 5.00 6.49 7.33 6.33 5.22 6.25 4.86 2.42 0.11   850603 1.79 0.63 1.60 2.00 4.03 0.82 0.76 0.70 0.65 0.63 0.61 0.52 0.16   850607 0.94 0.63 1.60 2.00 3.75 0.43 0.37 0.45 0.41 0.32 0.26	841201	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
850503   1.03   0.10   1.43   1.13   3.80   0.35   0.42   0.31   0.34   0.36   0.33   0.26   0.14     850508   16.08   0.75   1.33   1.60   5.00   6.49   7.33   6.33   5.22   6.25   4.86   2.42   0.11     850603   1.79   0.63   1.60   2.00   4.03   0.82   0.76   0.70   0.65   0.63   0.61   0.52   0.16     850607   0.94   0.63   1.60   2.00   3.75   0.43   0.37   0.45   0.41   0.46   0.41   0.32   0.26	841206	6.83	0.63	1.42	2.00	4.61	3.11	3.13	3.23	3.01	3.26	2.91	2.28	0.12
850603 1.79 0.63 1.60 2.00 4.03 0.82 0.76 0.70 0.65 0.63 0.61 0.52 0.16 850607 0.94 0.63 1.60 2.00 3.75 0.43 0.37 0.45 0.41 0.46 0.41 0.32 0.26	850430	16.09	0.75	1.43	1.60	5.00	0.33	0+42	0.37	0+34	6.25	0.33	2.42	0.14
850607 0.94 0.63 1.60 2.00 3.75 0.43 0.37 0.45 0.41 0.46 0.41 0.32 0.26	850603	1.79	0.13	1.55	2,00	4.03	0.92	0.76	0.33	J-22 D-65	0.23	0.61	0-52	0.10
	850607	0.94	0.63	1.60	2,00	3.75	0.43	0.37	0.45	0.41	0.46	0.41	0.32	0.26

A 12

		noise	(mc)	0.00	0.14	0.14	0.13	0.14	0.13	0.13	0.15	0.18	0.14	0.14	0.20	0.12	0.14	0.13	0.13	0.11	0.22	0.20	0.24	0.14	0.15	0.30	0.15	0.12	0.14	0.13	0.14	0.18
	7.B.S.	9-18s	( EC)	0.0	1.30	0.30	2.53	0.27	0.25	0.42	1.78	0.81	0.35	0.88	0.42	1.90	0.35	0.96	2.15	1.45	2.16	0.41	1.47	1.56	0.22	1.03	0.74	1.00	1.05	1.56	1.11	1.04
	7.9.N.	3-15s	( EL)	0.0	1.34	0.44	3.11	0.32	0.27	0.42	2.87	1.31	0.36	0.99	0.41	2.29	0.35	0.99	2.25	1.85	3.85	0.46	1.65	2.94	0.22	1.30	1.15	1.73	1.20	1.90	1.26	1.31
	7. B. S.	3-9s	(mc)	0.00	1.22	0.54	3.34	0.37	0.29	0.35	3.66	1.67	0.38	0.96	0.35	2.37	0.32	0.84	2.01	2.01	4.91	0.49	1.72	3.78	0.22	1.40	1.45	2.19	1.24	2.20	1.25	1.37
	.S.E.C	0-15s	(ac)	0.00	1.34	0.50	3.32	0.36	0.34	0.42	3.14	1.50	0.47	1.02	0.43	2.43	0.36	1.00	2.28	2.04	4.16	0.47	1.72	3.12	0.25	1.41	1.38	1.87	1.31	1.99	1.47	1.34
		0-9s	(mc)	0.00	1.26	0.59	3.59	0.42	0.38	0.37	3.79	1.82	0.54	1.02	0.41	2.57	0.35	0.91	2.15	2.24	5.01	0.50	1.81	3.77	0.27	1.53	1.68	2.24	1.40	2.24	1.59	1.4U
band		0-6s	(mc)	0.00	1.31	0.65	3.89	0.45	0.44	0.37	3.89	1.93	0.63	1.07	0.45	2.87	0.40	0.98	2.22	2.47	5.38	0.49	1.94	4.21	0.28	1.63	1.87	2.46	1.53	2.51	1.66	1.32
1.0-4.0Hz		0-3s	(EC)	0.00	1.35	0.69	4.05	0.50	0.53	0.42	4.05	2.09	0.77	1.11	0.51	2.93	0.42	1.05	2.40	2.65	5.21	0.52	1.97	3.76	0.35	1.77	2.06	2.35	1.68	2.33	2-12	1.44
ns in the	É	1		0.00	4.33	3.99	4.78	3.87	3.83	3.74	4.73	4.46	3.91	4.10	3.87	4.54	3.75	4.17	4.56	4.57	4.85	3.83	4.41	4.66	3.68	4.38	4.41	4.44	4.35	4.50	4.49	cZ.4
Observation	Gain			0.00	1.53	1.16	1.27	1.47	1.75	2.19	2.19	2.00	1.91	1.34	2.00	2.09	1.60	1.10	1.16	1.47	2.00	2.09	2.09	1.53	1.68	2.00	2.19	1.75	2.09	2.09	1.68	2.00
array - (	Frequency	(Hz)		0.00	1.29	1.08	1.14	1.25	1.43	1.74	1.74	1.60	1.54	1.18	1.60	1.67	1.33	1.05	1.08	1.25	1.60	1.67	1.67	1.29	1.38	1.60	1.74	1.43	1.67	1.67	1.38	1.60
Warramung	Period	(s)		0.00	0.77	0.93	0.88	0.80	0.70	0.57	0.57	0.63	0.65	0.85	0.63	0.60	0.75	0.95	0.93	0.80	0.63	0.60	0.60	0.77	0.73	0.63	0.57	00	0.60	0.60	0.73	0.63
(cont 'd)	1/2 PK-PK	(ac)		0.00	3.41	1.40	9.15	1.17	1.11	0.92	9.07	4.85	1.36	1.94	1.25	5.84	0.91	2.10	5.22	5.82	12.05	1.13	4.39	7.32	0.79	4.09	4.39	4.59	3.75	5.32	5.12	3.01
Table GA	Date			851024	851026	851124	851126	860426	860506	860527	860530	861112	861206	861210	870505	870520	870606	870621	871023	871105	871119	871129	880511	880525	880616	880623	881105	881123	830603	891024	891031	891120

Date	1∕⊕ (m ³ )	Moment (N m)	Duration (s)	Rise time	Fall time	pP-P time	1/2 Pk-Pk (nm)	Period (s)	Frequency (Hz)	Gain	₩D	
				(5)	(5)	(5)						
760711	0.00	0.0000E+00	0.00	0.00	0.00	0.00	3.62	0.73	1.38	1.69	4.18	26
770319	0.00	0+0000E+00	0.00	0.00	0.00	0.00	26.08	0.80	1.25	1.47	5.06	26
770706	0.00	0.00005+00	0.00	0.00	0.00	0.00	5.09	0.85	1.18	1.34	4.43	20
771124	0.00	0.0000E+00	0.00	0.00	0.00	0.00	26.40	0.80	1.25	1.47	5.06	26
771217	0.00	0.0000E+00	0.00	ň. nň	0.00	0.00	4.37	0.85	1.18	1.34	4.29	26
780227	ñ. ññ	0.0000E+00	0.00	0.00	ŏ. ŏŏ	0,00	0.00	0.00	0.00	0.00	0.00	žš
780322	0.00	0.0000E+00	0.00	0.00	0.00	Ō-OO	2.48	0.90	1.11	1.22	4.07	26
780719	0.00	0.0000E+00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	26
780726	0.00	0.0000E+00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	26
781102	0.00	0.0000E+00	0.00	0.00	0.00	0.00	3.90	0.88	1.14	1.28	4.25	26
781130	0.00	0.0000E+00	0.00	0.00	0.00	0.00	24.13	0.80	1.42	1.76	5+03	20
701219	0.00	0.0000000000000000000000000000000000000	0.00	0.00	0.00	0.00	4.04	0.80	1.25	1.47	4.25	26
790301	ñ. ññ	0.0000E+00	0.00	0.00	ŏ, ŏŏ	0,00	3.80	0.90	1.11	i 22	4.25	26
790309	0.00	0.0000E+00	0.00	Õ.ÕÕ	0.00	0.00	2.26	0.93	1.08	i.16	4.03	34
790324	0.00	0.0000E+00	0.00	0.00	0.00	0.00	2.74	0.73	1.38	1.66	4.07	34
790404	0.00	0-0000E+00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	26
790618	0.00	0.0000E+00	0.00	0.00	0.00	0.00	4.43	0.88	1.14	1.28	4.31	26
790629	0.00	0.0000E+00	0.00	0.00	0.00	0.00	3+23	0.11	1.29	1.34	4.30	20
790729	0.00	0.0000E+00	0.00	0.00	0.00	0.00	3.19	0.88	1.14	1.27	4.17	34
791122	0.00	0.0000E+00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	26
800223	ŏ.ŏŏ	0.0000E+00	0.00	0,00	0.00	0.00	1.22	0.75	1.33	1.59	3.72	34
800303	0.00	0.0000E+00	0.00	0.00	0.00	0.00	0.92	0.75	1.33	1.59	3.60	34
800323	0.00	0.0000E+00	0.00	0.00	0.00	0.00	11.55	0.85	1.18	1.33	4.72	34
800401	0.00	0.0000E+00	0.00	0.00	0.00	0.00	6+95	0.85	1.18	1.33	4.50	34
800404	0.00	0+0000E+00	0.00	0.00	0.00	0.00	1.26	0.82	1.21	1.39	3. (5	34
800521	0.00	0.0000000000	0.00	0.00	0.00	0.00	0.00	0.11	0.00	0.00	9.20	26
800719	0.00	0.0000E+00	0.00	0.00	0.00	0.00	15.73	0.82	1.21	1.39	4.85	34
801203	0.00	0.0000E+00	ŏ, ŏŏ	0.00	0.00	0.00	9.64	0.73	1.38	1.66	4.61	34
810227	0.00	0.0000E+00	0.00	0.00	0.00	0.00	1.05	0.68	1.48	1.81	3.65	34
810306	0.00	0.0000E+00	0.00	0.00	0.00	0.00	1.11	0.85	1.18	1.33	3.70	34
810328	0.00	0.0000E+00	0.00	0.00	0.00	0.00	3.19	0.82	1.21	1.33	4.15	34
810410	0.00	0.0000000000	0.00	0.00	0.00	0.00	1.60	0.62	1.29	1.96	3.84	34
010711	0.00	0.0000E+00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	34
810718	0.00	0.0000E+00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	34
810803	0.00	0.0000E+00	0.00	0.00	0.00	ŏ, ŏŏ	0.00	0.00	0.00	Ŏ.ŎŎ	0.00	34
811111	0.00	0.0000E+00	0.00	0.00	0.00	0.00	2.16	0.68	1.48	1.81	3,96	34
811205	0.00	0.0000E+00	0.00	0.00	0.00	0.00	2.62	0.93	1.08	1.16	4.10	34
811208	0.00	0.0000E+00	0.00	0.00	0.00	0.00	7.97	0.73	1.38	1.66	4.53	34
820220	0.00	0.000000	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	34
820224	0.00	0.00002.00	0.00	0.00	0.00	0.00	2.42	0.68	1.48	1.81	4.01	34
820627	0.00	0.00000000000	0.00	ñ. 00	0.00	0.00	ົ້ຄ. ກົດ	0.00	0.00	0.00	0.00	34
820701	0.00	0.0000E+00	ŏ, ŏŏ	0.00	0.00	Ŏ,ŎŎ	Ŏ.ŎŎ	0.00	0.00	0.00	0.00	34
820725	0.00	0.0000E+00	0.00	0.00	Ŏ. ÖÖ	0.00	9.88	0.77	1.29	1.52	4.63	34
830419	0.00	0+0000E+00	0.00	0.00	0.00	0.00	22+25	0.77	1.29	1.52	4.99	34
830425	0.00	0.0000E+00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	34
830525	0.00	0.0000000000	0.00	0.00	0.00	0.00	19-12	0.82	1.21	1.39	4.93	34
830618	0.00	0.000000000	0.00	0.00	0.00	0.00	7 99	0.00	0.00	1 22	4 56	34
830628	0.00	0.0000000000	0.00	0.00	0.00	0.00	0.00	0.00	0.00	1.33	0.00	34
830804	0.00	0.0000E+00	0.00	0.00	0.00	0.00	3,18	0.60	1.67	2.05	4.12	34
831203	0.00	0.0000E+00	ŏ, ŏŏ	ŏ.ŏŏ	ŏ.ŏŏ	0.00	ŏ. ôŏ	ŏ.ŏŏ	0.00	0.00	0.00	34
831207	0.00	0.0000E+00	0.00	0.00	0.00	0.00	2.23	0.90	1.11	1.21	4.02	34
840508	0.00	0.0000E+00	0.00	0.00	Ö• ÖÖ	0.00	1.54	0.65	1.54	1.88	3.81	34
840512	0.00	0.0000E+00	0.00	0.00	0.00	0.00	12.23	0.77	1.29	1.52	4.73	34

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Table 7A Gauribidanur array - Broad band and short period observations

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	Table 7A Date	(cont`d) ∲ <u></u> (m ³ )	Gauribidanur Moment (N m)	array - Bro Duration (s)	ad band Rise Cime	and short Fall time	period pP-P time	observation 1/2 Pk-Pk (nm)	Period (s)	Frequency (Hz)	Gain	Mb	
840612 0.00 0.000 0.00 0.00 1.61 0.65 1.54 1.88 3.83 34   840612 0.00 0.000 0.00 0.00 5.37 0.88 1.14 1.27 4.33 34   841027 0.00 0.0000 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00					(5)	(5)	(5)						
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	840612	0.00	0.0000E+00	0.00	0.00	0.00	0.00	1.61	0.65	1.54	1.88	3.83	34
841027   0.00   0.000000000000   0.00   0.00   0.000   0.000   0.000   0.000   0.000   0.000   0.000   0.000   0.000   0.000   0.000   0.000   0.000   0.000   0.000   0.000   0.000   0.000   0.000   0.000   0.000   0.000   0.000   0.000   0.000   0.000   0.000   0.000   0.000   0.000   0.000   0.000   0.000   0.000   0.000   0.000   0.000   0.000   0.000   0.000   0.000   0.000   0.000   0.000   0.000   0.000   0.000   0.000   0.000   0.000   0.000   0.000   0.000   0.000   0.000   0.000   0.000   0.000   0.000   0.000   0.000   0.000   0.000   0.000   0.000   0.000   0.000   0.000   0.000   0.000   0.000   0.000   0.000   0.000   0.000   0.000   0.000   0.000   0.000   0.000   0.000   0.000   0.000	840616	0.00	0.0000E+00	0.00	0.00	0.00	0.00	5-37	0.88	1.14	1.27	4.39	34
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	841027	0.00	0.00006+00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	34
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	841102	0.00	0+0000E+00	0.00	0.00	0.00	0.00	9.86	0.77	1.29	1.52	4.63	34
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	841201	0.00	0.00005+00	0.00	0.00	0.00	0.00	00.00	0.00	0.00	0.00	0.00	34
$\begin{array}{c} 83050430 \\ 850503 \\ 850503 \\ 0.00 \\ 0.0000000000000000 \\ 0.00 \\ 0.00000000$	841206	0.00	0+0000E+00	0.00	0.00	0.00	0.00	11+90	0.85	1.18	1.33	4.73	34
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	850430	0.00	0.00000000000	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	34
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	850508	0.00	0+0000E+00	0.00	0.00	0.00	0.00	14.25	0.93	1.08	1.16	4.83	34
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	850603	0.00	0.000000000	0.00	0.00	0.00	0.00	2.11	0.68	1.48	1.81	3.32	34
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	051024	0.00	0.0000E+00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	34
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	051024	0.00	0.00002.00	0.00	0.00	0.00	0.00	5 40	0.00	0.00	0.00	0.00	34
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	951124	0.00	0.00002.00	0.00	0.00	0.00	0.00	1 96	0.00	1 25	1.40	9.40	34
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	951124	0.00	0.00002.000	0.00	0.00	0.00	0.00	16 27	0.80	1.25	1.40	3.33	34
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	860527	0.00	0.0000000000000000000000000000000000000	0.00	0.00	0.00	0.00	10.00	0.00	6.00	0.00	4.00	24
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	860530	0.00	0.0000000000000000000000000000000000000	0.00	0.00	0.00	0.00	9.36	0.85	1.18	1.33	4.63	24
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	861112	0.00	0.0000E+00	ň, ňň	0.00	ň. nň	ň. ňň	4.09	0.73	1.38	1.66	4.24	34
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	861206	ŏ, ŏŏ	0.0000E+00	0.00	0.00	0,00	0.00	0.75	0.55	1.82	2.23	3.50	34
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	861210	0.00	0,0000F+00	0.00	ð. Öð	0.00	0.00	4.10	0.85	1.18	1.33	4.27	34
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	870505	0.00	0.0000E+00	0.00	ō, ōō	0,00	ŏ, ŏŏ	2.13	0.82	1.21	1.39	3.98	34
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	870520	0.00	0.0000E+00	0.00	0.00	0.00	0,00	7.30	0.82	i.2i	1.39	4.ŠĬ	34
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	870606	0.00	0.0000E+00	0.00	0.00	0,00	Ŏ. ÖÖ	1.78	0.63	1.60	1.96	3.87	34
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	870621	0.00	0.0000E+00	0.00	0.00	0.00	0.00	7.07	0+98	1.03	1.05	4.55	34
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	871023	0.00	0.0000E+00	0.00	0.00	0.00	0.00	9-03	0.85	1.18	1.33	4.61	34
871119 0.00 0.0000E+00 0.00 0.00 0.00 12.75 0.85 1.18 1.33 4.76 34   871129 0.00 0.0000E+00 0.00 0.00 0.00 2.64 0.73 1.38 1.65 4.05 34   880511 0.00 0.0000E+00 0.00 0.00 0.00 5.74 0.75 1.33 1.59 4.39 34   880525 0.00 0.0000E+00 0.00 0.00 0.00 10.40 0.82 1.21 1.39 4.67 34   880525 0.00 0.0000E+00 0.00 0.00 0.00 10.40 0.82 1.21 1.39 4.67 34   880523 0.00 0.0000E+00 0.00 0.00 0.00 5.48 0.88 1.14 1.27 4.40 34   881105 0.00 0.000 0.00 0.00 0.00 7.83 0.82 1.21 1.39 4.54 34   890511 0.00 0.000 0.00 0.00 0.00 0.00 0.00 <td< td=""><td>871105</td><td>0.00</td><td>0.0000E+00</td><td>0.00</td><td>0.00</td><td>0.00</td><td>0.00</td><td>10.77</td><td>0.75</td><td>1.33</td><td>1.59</td><td>4.67</td><td>34</td></td<>	871105	0.00	0.0000E+00	0.00	0.00	0.00	0.00	10.77	0.75	1.33	1.59	4.67	34
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	871119	0.00	0.0000E+00	0.00	0.00	0.00	0.00	12.75	0+85	1.18	1.33	4.76	34
880511   0.00   0.0000E+00   0.00   0.00   0.00   5.74   0.75   1.33   1.59   4.39   34     880525   0.00   0.0000E+00   0.00   0.00   0.00   1.40   0.82   1.21   1.39   4.67   34     880516   0.00   0.0000E+00   0.00   0.00   0.00   2.06   0.93   1.08   1.16   3.99   34     880616   0.00   0.0000E+00   0.00   0.00   0.00   2.06   0.93   1.08   1.16   3.99   34     880623   0.00   0.0000E+00   0.00   0.00   0.00   5.48   0.88   1.14   1.27   4.40   34     891511   0.00   0.000   0.00   0.00   0.00   5.42   0.80   1.25   1.46   4.38   34     890520   0.00   0.000   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   34     890603 <td>871129</td> <td>0.00</td> <td>0+0000E+00</td> <td>0.00</td> <td>0.00</td> <td>0.00</td> <td>0.00</td> <td>2.64</td> <td>0.73</td> <td>1.38</td> <td>1.66</td> <td>4.05</td> <td>34</td>	871129	0.00	0+0000E+00	0.00	0.00	0.00	0.00	2.64	0.73	1.38	1.66	4.05	34
880525 0.00 0.0000E+00 0.00 0.00 0.00 10.40 0.82 1.21 1.39 4.67 34   880616 0.00 0.0000E+00 0.00 0.00 0.00 2.06 0.93 1.08 1.16 3.99 34   880623 0.00 0.0000E+00 0.00 0.00 0.00 5.48 0.88 1.14 1.27 4.40 34   881105 0.00 0.0000E+00 0.00 0.00 0.00 7.83 0.82 1.21 1.33 4.54 34   890511 0.00 0.0000E+00 0.00 0.00 0.00 5.42 0.80 1.25 1.46 4.38 34   890520 0.00 0.000 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 </td <td>880511</td> <td>0.00</td> <td>0.0000E+00</td> <td>0.00</td> <td>0.00</td> <td>0.00</td> <td>0.00</td> <td>5.74</td> <td>0.75</td> <td>1.33</td> <td>1.59</td> <td>4.39</td> <td>34</td>	880511	0.00	0.0000E+00	0.00	0.00	0.00	0.00	5.74	0.75	1.33	1.59	4.39	34
880616   0.00   0.00006+00   0.00   0.00   0.00   2.06   0.93   1.08   1.16   3.99   34     880623   0.00   0.00006+00   0.00   0.00   0.00   5.48   0.88   1.14   1.27   4.40   34     88105   0.00   0.00006+00   0.00   0.00   0.00   5.48   0.88   1.11   1.27   4.40   34     890511   0.00   0.00006+00   0.00   0.00   0.00   5.42   0.80   1.25   1.46   4.38   34     890520   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00 <td>880525</td> <td>0.00</td> <td>0.0000E+00</td> <td>0.00</td> <td>0.00</td> <td>0.00</td> <td>0.00</td> <td>10-40</td> <td>0.82</td> <td>1.21</td> <td>1.39</td> <td>4.67</td> <td>34</td>	880525	0.00	0.0000E+00	0.00	0.00	0.00	0.00	10-40	0.82	1.21	1.39	4.67	34
880623 0.00 0.000000000000 0.00 0.00 0.00 5.48 0.88 1.14 1.27 4.40 34   881105 0.00 0.00000000 0.00 0.00 0.00 7.83 0.82 1.21 1.39 4.54 34   890511 0.00 0.000000000000 0.00 0.00 0.00 5.42 0.80 1.25 1.46 4.38 34   890520 0.00 0.00000000000 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 34   890503 0.00 0.000000000000000 0.00 0.00 0.00 0.00 3.46 0.80 1.25 1.46 4.18 34   891024 0.00 0.000000000 0.00 0.00 0.00 6.08 0.73 1.38 1.66 4.41 34   891031 0.00 0.00 0.00 0.00 9.19 0.75 1.33 1.55 4.60 34	880616	0.00	0.0000E+00	0.00	0.00	0.00	0.00	2.06	0.93	1.08	1.16	3+99	34
881105 0.00 0.0000E+00 0.00 0.00 0.00 1.33 0.82 1.21 1.33 4.54 34   890511 0.00 0.000E+00 0.00 0.00 0.00 5.42 0.80 1.25 1.46 4.38 34   890520 0.00 0.000E+00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 3.46 4.54 34   890503 0.00 0.000E+00 0.00 0.00 0.00 3.46 0.80 1.25 1.46 4.18 34   891024 0.00 0.000E+00 0.00 0.00 0.00 6.08 0.73 1.38 1.66 4.41 34   891031 0.00 0.00 0.00 0.00 9.19 0.75 1.33 1.59 4.60 34	880623	0.00	0.0000E+00	0.00	0.00	0.00	0.00	5.48	0.88	1.14	1.27	4-40	34
890511   0.00   0.00   0.00   0.00   0.00   5.42   0.80   1.25   1.46   4.38   34     890520   0.00   0.000   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00 <td< td=""><td>881105</td><td>0.00</td><td>0.00005+00</td><td>0.00</td><td>0.00</td><td>0.00</td><td>0.00</td><td>[·83</td><td>0.82</td><td>1.21</td><td>1.39</td><td>4.54</td><td>34</td></td<>	881105	0.00	0.00005+00	0.00	0.00	0.00	0.00	[·83	0.82	1.21	1.39	4.54	34
850220   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   0.00   <	890511	0.00	0.0000000000	0.00	0.00	0.00	0.00	5.42	0.80	1.25	1.46	4.38	34
891024 0.00 0.0000E+00 0.00 0.00 0.00 0.00 3.46 0.80 1.25 1.46 4.18 34 891024 0.00 0.0000E+00 0.00 0.00 0.00 0.00 6.08 0.73 1.38 1.66 4.41 34 891031 0.00 0.0000E+00 0.00 0.00 0.00 0.00 9.19 0.75 1.33 1.55 4.60 34	830320	0.00	0.0000E+00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	34
891031 0.00 0.0000E+00 0.00 0.00 0.00 0.00 0.0	830603	0.00	0.00000000000	0.00	0.00	0.00	0.00	3+40	0.80	1.20	1.46	4.18	- 54
	001024	0.00	0.0000000000	0.00	0.00	0.00	0.00	0.08	0.75	1.38	1.60	4.41	34
891120 0.00 0.0000 0.00 0.00 0.00 0.00 4.21 0.70 1.43 1.73 4.25 24	891120	0.00	0.0000E+00	0.00	0.00	0.00	0.00	4.21	0.70	1.43	1.73	4.00	34

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 $\begin{array}{l} & & \\ \mathsf{B}(\Delta) = 3.71 \ \mathsf{G}(\Delta) = 0.0000 \mathsf{E}^{+}00 \mathsf{s} \ \mathsf{m}^{-2} \ \rho_0 = 2700.0 \mathsf{kg} \ \mathsf{m}^{-3} \ v_0 = 5670.0 \mathsf{km} \ \mathsf{s}^{-1} \\ \rho_1 = 2400.0 \mathsf{kg} \ \mathsf{m}^{-3} \ v_1 = 3600.0 \mathsf{km} \ \mathsf{s}^{-1} \ \mathsf{K} = 0.00 \end{array}$ 

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T.m.s. Noise	(m) 1.04 0.94 0.73	1-07 0-71		888	0.80	0-23 0-80	0.93 0.48	0.00	- 46 - 46	62.00	0.31	0.23	0.25	0.00	0.71	0.23 80.23	0.02	88	0.39	0.43	0000	0.00	0.00	800 800		0.00	0.69
7.m.s. 9-18s	5.34 1.28	1.00 3.72		888	0.84 6.97	0.74 1.02	0.95	92-0	1.76			2-2-1- 	0.38	-0-8 -0-8	2•14 0•27		1.37	88	0.40 0.62	0.00		000	0.00	.0. .0		0.01	0.45 2.14
7.m.\$. 3-15s	1.26 1.86 1.86	1.17	886	88	0.87 8.97	1.14	1.02 0.66	0.02	1.84	1.16	989 900	9.74 4.74	0.39	0-0 3-80	2•71 0•33	-0-0 -0-0 -0-0 -0-0-0 -0-0-0 -0-0-0 -0-0-0 -0-0-0 -0-0-0 -0-0-0 -0-0-0 -0-0-0-0 -0-0-0-0 -0-0-0-0-0-0-0-0-0-0-0-0-0-0-0-0-0-0-0-0	1.47	888	0.60	0.02	323	888	0.00	888 900	800 70		0.59 3.04
Г. Ш. S. 3-95	9-519 9-519 0.00	9-83 9-83	100	88	0.99	1.41	0.82	80.0	1.95		0.37	4.7.4	0.40	0.00	3.11 0.48	0.77	1.56	88	0.72 0.82	0.00	386	000	0.025	80.0 0.00		-00 888	0-68 3-63
7.m.s. 0-15s	2.04 8.41 2.04	- 252 - 252 - 255	0.00	88	800 0.30	1.35	1.12	-0-04 -07	- 6.g	1.25	0.40		0.44	0.00	2•96 0•42	- 4-0 - 79-0 - 79-0		88	0.67 0.78	62-20 -00 -00			6.74	.00 20 20 20 20 20 20 20 20 20 20 20 20 2		1000	0.67 3.42
7.8.7 0-9s	9.85 9.85 2.42	1.76 10.04	0.00	88	1.12	1.50	0.88	200.0	2.02	1.34	0.40	4.77	0.47	2.01	3.35 0.49	- 00 - 00	0.00	88	0.78	008 0-08 0-0			0.00	0.00	2000	0000	0.4 9.00
r.m.s. 0-65		- 8- - 95 - 95 - 95	00.00	888	1.19 8.89	1.56	1•36 0•97	0.00	2-03	1.48	0.43	4.14	0.49	0.00	0.52 0.52 0.52	0.03	1.68	88	0.79	0.00 0.00 0.00			7.46 0.00		- 00 - 0		0.79 4.28
band r.m.s. 0-3s	1.51 10.40 2.65	2.46 10.44 - 73	0.00	88.0	1.35	1.94 1.83	1.47	0.00		1.57	0.51	4.82 102 102	0.59	0.00	3-79 0-52 0-52	0.58 1.32	1.75	88	0.88 1.04	0.00	888	80-7 80-7	10.00	0.00	10.0	00-0	4.65
0.5-4.0Hz mb	4.11 5.00 4.37	4.39 7.00 8.00	0.00	88	5.23 5.23	4.26 4.26	4.14 3.95	4.0 0.00 800	1 4 v	4.27	205 605 605 605 605 605 605 605 605 605 6	4.68	3.79	0.00	4.60 9.63	4.12 122 202	0.00	88	ភូសិ សូសិ សូសិ	4·51	0.4 C	008	4.98 80.0	4.0 800 800	-0-4 -0-4	-040 -040	3.88 4.66
ons in the J Gain	2.02 1.85 1.34	1.16 1.69	-0- -0-	88	1.76	1.54	1.61	0.00	92.1	0.82	81. 2. 2. 2.	225	0.95	0.00	1.59	4		800	1.73	0.00			0.00	-00 0.00		0000	1.81
Observatio Frequency (Hz)	1.60 1.48 1.18	1.38	0.00	800	1.43 0.74	1.29	1.33 1.38	0.00	1.43	16.0	1.74	1.29	0.98	0.00	1.33	1.25		88	1.43	0.00		0.00	0.00	0.00	-00	0000	1.48 1.38
r array - Period (s)	0.63 0.68 0.85	0.43 133 133	0.00	888	0.70	0.73	0.75	0.00	0.10	01-10	0.57	0.77	0.75	0.00	0.73		0.63	88	0.70	0.00		000	0.00	0.00			0.73
Gauribidanu 1/2 Pk-Pk (nm)	3.17 24.56 5.19	5.10 23.61	0.0	88	3.13 22.46	4.19 4.38	3•23 5•03	.00 0.00 0.00	4 4 5 2 4 4 2 6 0 5	3.29 9.79	00-1	11.09	1.18	0.00	9.41 1.00	3.03	3.31 0.00	889	2.09 2.26	0.00	886 5 % 6	0.08	22.41 0.00	16-51 0-00	285	888	1.81
Table 8A Date	760711 770319 770706	7711124	780227	780726	781102	781217 781219	102062	790324 790404 700010	790629	790728	800223 800223	800323 800323	800404 800621	800706 800719	801203 810227	810328 810328	810708	810718 810803	811111 811205	811208 820220	820224 820320 020527	820701 820701	830419 830425	830525 830618	830720 830720	831203 831203	840508 840512

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840612	( በጠ )	(5)			-								
840612			(H2)			0-3s	0-6s	0-9s	0~15s	3 <b>-9s</b>	3-15s	<b>9-1</b> 8s	noise
840612						(חת)	(nm)	( רוח )	(nm)	(nn)	(nm)	(nm)	(nm)
040616	2.20	1.15	0.87	0.74	4.12	1.27	1.05	1.14	1.01	1.07	0.93	0.70	0.97
040010	4.95	1.35	0.74	0.49	4.58	2.63	2.47	2.29	1.85	2.09	1.60	0.92	0.92
841027	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
841102	9.40	0.73	1.38	1.66	4.60	4.14	3.81	3.71	3.19	3.47	2.91	2.01	0+39
841201	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
841206	10.77	0.77	1.29	1.52	4.67	4.60	4.13	4.58	3.83	4.57	3-61	2.11	0.41
850430	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
850508	12.70	0.88	1.14	1.27	4.77	6.08	6.20	6.14	5.26	6+16	5-04	3+31	0.27
850603	2.48	2.03	0.49	0.15	4.62	1.16	1.06	1.04	0.94	0.98	0.88	0.84	0.91
850607	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0+00	0.00
851024	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
851026	4.33	0.82	1.21	1.39	4.29	2.32	1.93	1.85	1.57	1.56	1.31	0+94	0.44
851124	1.91	0.80	1.25	1.46	3.92	0.90	0.85	0.81	0.65	0.75	0.57	0.46	0.39
851126	14.29	0.82	1.21	1.39	4.80	6.59	6.12	6+42	5.35	6.33	4.99	2.73	0.40
860527	0.00	0.00	0.00	0.00	8.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
860530	8.90	0.13	1.38	1.66	4.58	4.12	3.39	3.39	3.00	2.95	2.65	2.12	0.43
861112	4.32	0.13	1.38	1.66	4-21	1.84	1.65	1.58	1.31	1.44	1.14	0.75	0.28
861206	1.21	0.65	1.54	1.88	3.71	0.52	0.65	0.60	0.59	0.64	0.60	0.62	0.44
861210	3.69	1.42	0.10	0.42	4.50	1.80	1.44	1.33	1.13	1.01	0.88	0.66	0.37
810505	2.10	0.68	1 • 48	1.81	3.92	0.90	0.86	0.85	0.73	0.82	0.68	0.58	0.49
870520	5.12	1.43	0.80	0.50	4.62	2.9(	2.86	3.21	2.66	3.40	2.58	1.32	0.68
870606	2.48	0.((	1.29	1.52	4.03	0.95	1.03	1.15	1.10	1.24	1.14	1.05	0.75
810621	3.11	1.02	0.98	0.95	4.48	2.82	2.28	2.10	1.81	1.62	1.45	1.22	0.80
8/1023	1.14	0.35	1.05	1.10	4.58	3. (1	2.25	3.12	3.13	3.13	3.05	1.91	0.37
871103	10.03	0.13	1.33	1.33	4.04	4.13	3.63	4.31	3.50	4.39	3.33	1.63	0.20
871113	11.60	0.82	1.21	1.33	4.12	3.38	2.13	5.59	4.52	2.63	4.21	1.88	0.63
000511	2.00	0.10	1.43	1.13	4.09	1.08	1.02	1.04	0.88	1.02	0.82	0.55	0.31
000515	J. 45	0.15	1.30	1.50	4.31	2.30	2.21	2.51	1.86	2.23	1.12	0.98	0.21
000020	3. 30	0.13	1.33	1.55	2 00	4.43	3.14	3.03	3.22	2.98	2.84	2.45	0.12
000010	5.09	0.13	1.33	1.29	4 26	2 10	1 72	2 00	0.83	0.33	0.81	0.64	0.11
000023	7 20	0.02	1.00	1 10	4.50	2.10	2 92	2.00	1.11	2.01	1.60	0.81	0.69
001103	6 15	0.33	1.25	1 46	4 42	2.22	2.32	2.10	2.34	2.43	2.02	1.36	0.50
000500	0.13	0.00	1.23	1.40	0 00	2.00	2.30	2.40	2.12	2.22	1.83	1.29	0.19
890603	4.25	0.85	1.18	1.33	4.28	2.49	1.90	2.22	2.12	2 24	2 01	0.00	0.00
891024	5.47	0.69	1.48	1.81	4.20	2.39	2.25	2.33	2.12	2.24	2.01	1.01	1.40
891021	9.29	0.70	1.43	1.73	4.59	2.50	3.27	2.33	2.11	2.50	2 97	1.23	0.43
891120	4.17	0.80	1.25	1.46	4.26	1.97	1.74	2.00	1 70	2.00	2.31	2.00	0.62

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r.⊯.s. ⊓oise	0.00 6.481 6.481	0.33	0.00	383	0.52	0.54	0.23	0.00	0.77	0.0 0.0	0.17 0.14	0.12	0.14	0.00	0.78	901-0 0	90	800	0.17	0.18	0.0	88	0.18	8.0	0.00	0.00	0.00	0.47
7.m.s. 9-185	(m) 9.80 180 180 180 180 180 180	0-24 0-24	0.50 0.50	388		52.0 22.0	0.35	0.00	1.16	0.53 0.00	0.22 0.18	1.54	0.24	-20	0.20	0.45	0.66	888	0.29	1.13		88	3.27	0.0	0.00	0.0 0.42 0.5	0.00	1.52
r.m.s. 3-15s	0.95 2.62 2.62	0.40 0.74	0.00		6.26	88.0	0.68	0.00	1.27	69 <b>-</b> 0	0.26	2.61 1.45	0.26	2.12 2.12	0.29	0.4.0	22.00	886	0.42	1.66	0.0	88	1.91	0.00	5-00 5-00	0.0 8 1 8 1 8	0.00 0.490 0.490	2.91 2.06
r.m.s. 3-9s	(cm) 1.04 1.04 1.04 1.04 1.04 1.04	6.40 0.84 0.84	0.00	888	2.63 7.63	0.94	0.62	0.00	8.94 8.94	0.08 0.08	0.31	3.38 1.67	0.23	2•50 540	0.34 24 40	200 200	8000	888	0-51	60-1-0	0.00	000	2.47 4.99	0.00	0.00 2.67	0.0 1-08	8 <u>8</u>	0.45 2.44
<b>r.m.s.</b> 0-15s	(mc) 1.03 1.04 1.02 1.02 1.02	5.11 0.82	0.00	888	6.17 6.17	86.0 86.0	0.53	0.00	1.28	0.73 0.00	0.29	2.73 1.59	0.90	2•51 5•51	0.32		200 200	888	0.49	1.78	0.00		2.03 2.03	0.00	0.00 5.00	0.0 0.9	0.520	2.22 2.22
r.m.s. 0-9s	(na) 1.14 1.79 1.79 1.79	0.90 0.90 0.90	0.00	388	7.08	1.08	0.64	0.00	1.37 8.44	0.75	0.33	3.31 1.81	0.34 1.00	0.00 2.97	2-13 0-37			888	82.0	5-00 0-00	0.0	88	2.55 5.71	0.00	0.00	0.00 1.14	0.00	2.56 2.56
r.m.s. 0-6s	(nm) 1.18 6.07 1.42	666 0	0.00	388	2.59	1.15	0.83	0.00	1.34	0.78 0.00	0.33	2.92 1.82	0.36	0.00 2.91	N8:	*89.*	1.26	888	0.58	505	0.0	88	2.33 2.33	0.00	0.00	0.00 1.12	0.00	0.64 2.32
and r.m.s. 0-3s	(nm) 1.32 6.542 1.494	6.03 1.08 1.08	0.00	882	2.83	1.32	0.67	0.00	1.33	0.87 0.00	0-38 0-38	3.18 2.06	0.43 1.05	0.00 3.67	2.00 C 14 (2		1.46	888	0.10	2.21	0.0	88	2.70 6.92	0.00	0.00 2.61	0.00	0.00	2.77
.0-4.0Hz b Mb	4.07 4.81 17	4.80 50 50 50 50	0000	386	4.76	4 C	3.92	0.00 4.03	4.07	3-95 0-00	ຕີ ເມື່ອ ເມື່ອ	4.53 4.32	3.61 4.00	0.00 4.59	3.56 .6	ກ ເດິດ ກໍ່ຕໍ່ຕໍ່	90.4 90.6	888	3-85 3-86	4.39	0.00		4.40 4.86	0.00	0.00	0.00 4.06	0-00 3-75	4.48 0 80
s in the l Gain	2.32 2.21 2.21 2.21	2.02 1.69	0.00 0.430 0.430	887	1.69 1.76	1.26	1.81	0.00	2.02 1.59	1.66 0.00	1.73 2.13	1.73 1.66	1.96 2.02	0.00	1-23	65-1 - 200		888	1.73 1.66	5.02	0.00	800	1.73	0.00	0.00	0.00 2.23	0.00	
bservation Frequency (Hz)	1.82 1.74 1.29	1.38 1.38	0.00	00.0	861		1.54	0.00	1.33	1.38 0.00	1.43 1.74	1.43 1.38	1.60 1.60	0.00	1.29	861 	09.1	800	1.43	1.67	8.0	88	1.54	0.00	8.	0.00 1.82	0.0	1.54
array - O Period (s)	0.55 0.57 0.77	0.63	0.22	385	0.73	0.680	0.65	0.00	0.63	0.73 0.00	0.10	0.73	0-63 0-63	0.00	0.11	500 522	0.63	888	0.70	0.00	0.00	80.0	0.65	0.00	000	0.00	0000	0.65
Gauribidanur 1/2 Pk-Pk (nm)	2.91 16.11 3.41	2.66	0.00 5.20 0.20	300	13.82		1.59 2.23 2.23	0.00 2.45	2.91	2.11 0.00	0.91 0.84	7.97 4.87	0.97 2.48	0.00 9.26	0.84	205 205	2.74	800 800	1.69	600	0.00	000	5.97 17.25	0.00	0.00	0.00 2.75	0.81 1.58	5.1 7.27
Table 9A I Da <u>t</u> e	112037 112037 112077 112077	771124	780227 780322	780726	781130	781219	790309	790404	790629	790728 791122	800223 800303	800323 800401	800404 800621	800706	801203 810227	810328 810328	810708	81018	811111	811208	820224 820320	820627	820725 830419	830425 830525	830618 830628	830720 830804	831203 831207	840512 840512

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I GOT 6 20	(cont'd) G	auribidanu	ur array - U	Dservation	ns in the	1.U~4.UH2	band						
Date	1/2 Pk-Pk	Period	Frequency	Gain	m _b	r.m.s.	r•m•s•	r.m.s.	r.m.s.	r.a.s.	r.m.s.	r•m•s•	r•m•s•
	(nm)	(s)	(Hz)			0-3 <del>s</del>	0-6s	0-9s	0-15s	3-9s	3-15s	9-18s	noise
						(nm)	(nm)	(שת)	(nm)	(nm)	(nm)	(nm)	(nm)
840612	1.58	0.70	1.43	1.73	3,83	0.81	0.68	0.63	0.54	0.53	0.45	0+36	0.36
840616	2.69	0.70	1.43	1.73	4.06	1.21	1.14	1.14	0.94	1.11	0.86	0.50	0.31
841027	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
841102	7.04	0.68	1.48	1.81	4.47	2.94	2.44	2.56	2.18	2.35	1.95	1.37	0.18
841201	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
841206	7.32	0.75	1.33	1.59	4.50	3.07	2.89	3.42	2.85	3.59	2.80	1.56	0-19
850430	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
850508	8.35	0.77	1.29	1.52	4.56	3.84	4.39	4.52	3.77	4.83	3.76	2.11	0.16
850603	1.57	0.60	1.67	2.05	3.82	0.80	0.69	0.71	0.60	0.67	0.53	0.36	0.42
850607	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
851024	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
851026	2.49	0.68	1.48	1.81	4.02	1.11	0.92	1.01	0.89	0.96	0.83	0.61	0.22
851124	1.29	0.63	1.60	1.96	3.73	0.58	0.50	0.50	0-41	0+45	0.35	0.26	0.21
851126	9.02	0.80	1.25	1.46	4.60	3.81	3.15	4.38	3.62	4.63	3.57	1.75	0.21
860527	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
860530	7.00	0.55	1.54	1.88	4.47	3.13	2.48	2.56	2.20	2.23	1.90	1.52	0.22
861112	3.08	0.10	1.43	1.(3	4.12	1.3(	1.21	1.18	0.98	1.08	0.85	0.57	0.17
861206	1.05	0.93	1.08	1.16	3.10	0.43	0.42	0.44	0.39	0.45	0.37	0.30	0.25
861210	2.02	0.50	1.61	2.05	3.95	0.32	0.75	0.14	0.54	0.61	0.54	0.40	0.21
870505	1.58	0.35	1.82	2.23	3.80	0.50	0.58	0.58	0.51	0.54	0.46	0.34	0.23
870520	3.11	0.13	1.38	1.00	4.20	1.12	1.64	2.13	1.12	2.31	1.(2	0.80	0.26
870606	1.56	0.60	1.02	2+05	3.81	0.39	0.10	0.51	0.65	0.10	0.66	0.31	0.27
071022	2.50	0.30	1.00	1.16	4.11	2 05	1.12	1.20	1.12	1.19	1.03	0.11	0.23
9711023	7.66	0.33	1.29	1.66	4.50	2.00	2 61	2.42	2.10	2.33	2.11	1.20	0.22
971119	7.39	0.75	1.33	1.59	4.50	3.30	2.01	2.20	2.00	3.31	2.01	1.20	0.30
971129	2.24	0.63	1.60	1.96	3.97	0.82	0.74	0 77	0 65	0.74	3.03	1.11	0.20
880511	2.73	0.65	1.54	1.98	4.19	1.59	1.42	1.62	1.22	1 62	1 25	0.40	0.20
880525	6.69	0.65	1.54	1.88	4.45	2.90	2.41	2.44	2.08	2.19	1.92	1 21	0.30
a1a088	1.40	0.70	1.43	1.73	3.77	0.56	0.46	ñ. 56	0.51	0.56	0.50	0 42	0.31
880623	3.46	0.73	1.38	1.66	4.17	1.50	1.24	1.60	1.29	1.64	1.23	0.52	0.31
881105	4.45	0.82	1.21	1.39	4.30	1.95	1.77	1.80	1.51	1.73	1.39	0.92	0.21
890511	4.99	0.75	1.33	1.59	4.33	1.97	1.70	1.88	1.59	1.84	1.48	0.86	0.38
890520	0.00	0.00	0.00	0.00	0.00	0.00	0.00	n nă	0.00	ň, ňá	0.00	0.00	0.00
890603	3.13	0.75	1.33	1.59	4.13	Ĩ. 70	1.31	1.60	1.44	1.54	1.37	1.09	0.79
891024	3.85	0.60	1.67	2.05	4.21	1.66	1.55	1.63	1.40	1.61	1.33	0.86	0.27
891031	7.50	0.65	1.54	1.88	4.50	2,94	2.51	2.71	2.43	2.58	2.29	1.67	0.38
891120	3.15	0.82	1.21	1.39	4.15	1.35	1.18	1.48	Ĩ•20	1.54	Ī•Ī6	0.54	0.21

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Table 9A (cont'd) Gauribidanur array - Observations in the 1.0-4.0Hz band

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### <u>APPENDIX D</u>

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# TABLES OF FANGATAUFA OBSERVATIONS

The title page to Appendix C gives a description of how  $\psi_{\infty}$  and moment is calculated and describes how magnitude is calculated from the observations listed.

#### Table 1A Yellowknife array - Broad band and short period observations

(5) (5) (5) 750605 454.50 0.1776E+15 0.46 0.18 0.13 0.36 5.00 0.75 1.33 1.61 4. 751126 1327.93 0.5190E+15 0.55 0.17 0.16 0.86 8.37 0.65 1.54 1.91 4. 881130 18383.31 0.7185E+16 0.77 0.20 0.27 0.79 59.11 0.90 1.11 1.22 5.6 890610 15709.78 0.6140E+16 0.71 0.19 0.27 0.80 52.23 0.90 1.11 1.22 5.6 890127 14373.01 0.5618E+16 0.77 0.21 0.24 0.81 50.96 0.73 1.38 1.82 5.5	Date	p i	Fall time	Fall time	all Ne	t	pP- time	1	,	t	ti	pi tim	oP−F me	P	1/2 Pk [.] (nm)	-Pk	F	Period	F	requency (Hz)	C	Bain	ш ^р		
	750605 751126 881130 890610 891127		(5) 0.13 0.27 0.27 0.24	(5) 0.13 0.16 0.27 0.27 0.24	5) •13 •16 •27 •27 •24		(5) 0.3 0.8 0.7 0.8 0.8					000000000000000000000000000000000000000	(s) 0.3( 0.8( 0.7( 0.8( 0.8( 0.8(	16 19 10	5.0 8.3 59.1 52.2 50.9	0 7 1 3 6		0.75 0.65 0.90 0.90 0.73		1.33 1.54 1.11 1.11 1.38	1	1.61 1.91 1.22 1.22 1.82	4.55 4.76 5.66 5.61 5.52		23 23 23 23 23 23 23 23 23 23

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* B( $\Delta$ )=3.93 G( $\Delta$ )= 0.5975E-11s m⁻²  $\rho_0$ =2670.0kg m⁻³  $v_0$ =5640.0km s⁻¹  $\rho_1$ =2400.0kg m⁻³  $v_1$ =3600.0km s⁻¹ K=0.76

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Date	1/2 Pk-Pk	Period	Frequency	Gain	m _b	r•m•s•	r•m•s•	r.m.s.	r.m.s.	r • m • 5 •	r.m.s.	C+M+S+	r.m.s.
	(กล)	(5)	(Hz)			0-3s	0-6s	0-9s	0-15s	3-9s	3-15s	9-18s	noise
						(nm)	(nm)	(nn)	(nm)	(mm)	(nm)	(nm)	(mm)
750605	5.22	0.75	1.33	1.61	4.57	2.35	1.71	1.42	1.11	0.51	0.41	0.31	0.37
751126	8.21	0.60	1.67	2.09	4.75	3.38	2.68	2.22	1.77	1.29	1.02	0.65	0.36
991120	ຣ <u>ຈັ</u> ້ດີ5	1.42	0.70	0.42	5.95	33.86	27.42	23.32	18.18	15.57	11.24	4.06	0.40
000610	60.14	1.10	0.91	0.82	5.76	33.00	25.73	21.54	16.87	12.30	9.14	4.51	0.41
091127	51 74	1.59	0.63	0.29	5,98	28.55	23.63	20.09	15.81	14.07	10.43	4.91	0.21

Table 3A	Yellowknif	e array -	Observation	s in the	1.0-4.0Hz	band							
Date	1/2 Pk-Pk (nm)	Period (s)	Frequency (Hz)	Gain	тъ	r.m.s. 0-3s (nm)	r+m-s+ 0-6s (nm)	r•m•s• 0-9s (∩m)	ເ⊳ະໜາະຊາ 0∽15s (ເດຫຼ)	r•m•s• 3-9s (nm)	ຕ•m•s• 3−15s (ກm)	r•m•s• 9-18s (nm)	romoso noise (nm)
750605	4.21	0.73	1.38	1.68	4.47	2.02	1.47	1.21	0.95	0.40	0.32	0.20	0.31
751126	6.72	0.60	1.67	2.09	4.66	2.77	2.15	1.77	1.40	0.93	0.73	0-44	0.17
881130	39.49	0.65	1.54	1.91	5.43	17.06	12.96	11.12	8.71	6.32	4.70	2.82	0.16
890610	39.98	0.65	1.54	1.91	5.44	17.74	13.49	11.16	8.79	5.43	4.24	3.01	0.32
891127	39+56	0.63	1.60	2.25	5.38	16.98	12.94	10.77	8.53	5.46	4.34	3.24	0.09

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Table 4A	Warramu	nga arrau - Brc	ne pred bed	d short	period ob	servatio	su				
Date	*	Moment	Duration	Rise	Fall	9-9q	1/2 Pk-Pk	Period	Frequency	Gain	ŧ
	(a³)	(W W)	( S )	time	time	time	(mu)	(s)	(H2)		•
				(S)	(S)	(S)					
751126	304.67	0.1191E+15	0.56	0.13	0.12	0.84	2.11	0.65	1.54	1.93	4.10
881130	6490.26	0.2537E+16	0.75	0.17	0.20	0.88	26.93	0.73	1.38	1.68	5.22
830610	7399.58	0.2892E+16	0.77	0.18	0.23	0.86	29.04	0.82	1.21	1.40	5.27
# Β(Δ)=3.ξ ρ ₁ =2400	37 G(∆)= ( •0kg m ⁻³ v ₁	0.6802E-11s m ⁻² =3600.0km s ⁻¹ K	թ ₀ =2600-0kg :=0.77	ј m ⁻³ ∪ ₀ =	5600.0km	Ť.					

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erio erio (s)	0.65 0.65 0.70
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amun 2k-Pk	02 50 50
Har 1/2 F 1/2 F	56.2 24.2
E a	ဖိုစ္တဝ
Date	7511 8811 8906

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Table 6A	Warramunga	- fielie i	Observations	in the 1	1.0-4.0H=	pand							
Date	1/2 PK-PK	Period	Frequency	Gain	é	7.B.S.				.S.E.	F.B.S.	1.B.S.	2.E.1
	( <b>u</b> u)	(s)	(HZ)		•	0-3s	0-6s	0-9s	0-15s	3-9s	3-15s	9-18s	noise
						(mc)	(EC)	(mc)	( <b>u</b> C)	(mc)	( <b>E</b> C)	( <b>W</b> C)	(ec)
751126	1.88	0.55	1.82	2.32	4.04	0.94	0. 70	0.58	0.47	0.26	0.23	0.17	0.11
881130	22.43	0.65	1.54	16.1	5.13	10.32	8.79	7.34	5.75	5.25	3.83	1.41	0.11
890610	21.47	0.73	1.38	1.68	5.12	8.65	6.42	5.34	4.23	2•32	1.92	1.31	0.23

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Table 7A Gauribidanum array - Broad band and short period observations

Date	₩ <u></u> (m ³ )	Momént (Nm)	Duration (s)	Rise time	Fall time	pP-P time	1/2 Pk-Pk (nm)	Period (s)	Frequency (Hz)	Gain	m _b	
750605 751126 881130 890610 891127 *	0.00 0.00 0.00 0.00 0.00	0+0000E+00 0+0000E+00 0+0000E+00 0+0000E+00 0+0000E+00	0.00 0.00 0.00 0.00 0.00	(s) 0.00 0.00 0.00 0.00 0.00	(5) 0.00 0.00 0.00 0.00 0.00	(s) 0.00 0.00 0.00 0.00 0.00	0.00 3.88 12.94 12.74 17.80	0.00 0.63 0.73 0.70 0.73	0.00 1.60 1.38 1.43 1.38	0.00 2.02 1.66 1.73 1.66	0.00 4.20 4.74 4.73 4.88	26 26 34 34 34

**ب** 

B(Δ)=3.71 G(Δ)= 0.0000E+00s m⁻²  $\rho_0$ =2700.0kg m⁻³  $v_0$ =5670.0km s⁻¹  $\rho_1$ =2400.0kg m⁻³  $v_1$ =3600.0km s⁻¹ K=0.00

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7.m.5. (0156 0.00) 1.29 0.32 0.32 0.32
9-10 - 185 - 185 - 10 - 10 - 10 - 10 - 10 - 10 - 10 - 10
3-155 (na) (na) (na) (na) (na) (na) (na) (na)
r.m.s. (nm) 2.000 2.000 2.058 2.058 11.65 12.76
7.m.s 0-15s (nm) 0.00 2.25 8.81 8.81 9.47
7.m.s. (nm) 2.75 2.75 10.93 110.23 110.23
7.m.s. 0-6s (nm) 3.20 112.79 112.44 11.40 113.44
Pand 7. 0-35 0.00 0.00 9.51 10.19 10.19 10.19
0.5-4.0Hz -4.0Hz -4.45 5.31 5.31 5.32 5.32
s in the 6 6ain 0.00 1.76 0.57 0.57 0.57
Dbservatior Frequency (Hz) 0.00 1.43 0.78 0.78 0.78 0.78
array - 1 (s) 0.00 0.70 1.27 1.27
Gaur ib i danur 1/2 Pk-Pk (nm) 0.00 6.82 29.23 29.23 29.23 29.23
Table 8A Date 750605 751126 891120 890130 891127

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7.8.S. 70158	(m) 0.00 0.19 0.33 0.25
F.m.s. 9-18s	(nm) 0.00 1.78 1.89 2.28
Г. М. S. 3-15s	(nm) 0.00 5.155 5.125 5.125 5.125
5-8-€ 3-9s	(mc) 0.00 1.99 7.07 1.07 1.07
r.m.s. 0-15s	0.00 5.21 5.88 5.88 5.88 5.88 5.88 5.88 5.88 5.8
<b>r.m.</b> s. 0-95	(mm) 0.00 5.32 6.18 6.18 7.14
<b>Γ.m.\$.</b> 0-65	(nm) 0.00 2.73 7.12 7.99 7.99
and r.m.s. 0-35	(0.00) 0.00 7.2.86 5.27 5.27
1.0-4.0Hz t mb	0.00 4.33 4.78 88 4.78 88 88 81 81
s in the Gain	0.00 1.93 1.52 1.52
Observations Frequency (Hz)	0.00 1.554 1.29 1.29
array - Period (s)	0.00 0.65 0.77 0.77
Gauribidanur 1/2 Pk-Pk (nm)	0.00 5.82 17.92 13.76
Table 9A Date	750605 751126 881130 890610 891127

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