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**A Computer Program for the Determination of the Phase Velocity
of Seismic Surface Waves between Pairs of Stations**

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SUMMARY

The program described determines the phase velocity of a dispersed seismic surface wave as a function of period between a pair of stations from their digitized seismograms. The cross-multiplication technique of Bloch and Hales [1] is used to compute the phase velocity curve.

1. INTRODUCTION

Seismic surface waves generated by a distant earthquake or explosion are dispersed; that is the velocity at which their energy (the group velocity) and their individual harmonic components (the phase velocity) propagate is a function of frequency. This is because the longer period surface waves usually travel faster than the shorter periods, as they sample deeper down in the Earth's interior where the shear and compressional wave velocities are greater.

From the dispersion of surface waves deductions can be made about the P and S wave velocity and density structure of the crust and upper mantle through which they have passed; this is usually carried out by comparing theoretical dispersion curves computed for layered Earth models with the observational data to obtain a reasonably fitting model.

The relationship between group and phase velocity is $U = C - \lambda(dC/d\lambda)$, where U is the group velocity, C is the phase velocity and λ is the wavelength.

As group velocity depends on the derivative of phase velocity, it has an inherent non-uniqueness [2], hence models are best tested against phase velocity data.

The Fourier transform of a surface wave signal $x(t)$, ($x(t) = 0$, for $t < 0$) recorded by a seismological station at a distance r, and azimuth θ from the source is

$$X(\omega) = \int_0^\infty x(t) \cdot e^{-i\omega t} dt,$$

where t is time and ω is angular frequency.

The complex spectrum of the signal, $X(\omega)$, can be represented by its amplitude, A, and phase, ϕ , functions

$$X(\omega) = A(r, \theta, \omega) \cdot e^{i\phi(r, \theta, \omega)}.$$

The phase spectrum can be represented as

$$\phi(r, \theta, \omega) = k(\omega) \cdot r + \phi_o(\theta, \omega) + \phi_i(\omega) + 2n\pi, \dots (1)$$

where $k(\omega)$ is the wavenumber ($2\pi/\text{wavelength}$), $\phi_o(\theta, \omega)$ is the source phase shift and $\phi_i(\omega)$ is the instrumental phase shift. The term $2n\pi$ arises ($n = 1, 2, \dots$) since the Fourier transform contains phase information only for an angle interval $(0, 2\pi)$.

Now, $C(\omega) = \frac{\omega}{k(\omega)}$.

To evaluate $k(\omega)$ it is necessary to determine ϕ_o , ϕ_i , and the integer n (see equation (1)).

Due to the difficulty in measuring the source phase shift ϕ_o , which can only be calculated with a knowledge of the earthquake mechanism, single station measurements of phase velocity are not frequently used. This problem may be overcome by using two stations and an earthquake or explosion on a great circle path (the interstation phase velocity method) and measuring the phase difference between the two seismograms.

From equation (1)

$$k(\omega) \cdot r_1 = \phi_i(r_1, \theta, \omega) - \phi_o(\theta, \omega) - \phi_{i1}(\omega) + 2n_1\pi \dots (2)$$

for the nearest station, and

$$k(\omega) \cdot r_2 = \phi_i(r_2, \theta, \omega) - \phi_o(\theta, \omega) - \phi_{i2}(\omega) + 2n_2\pi \dots (3)$$

for the furthest station.

Thus, assuming that ϕ_o is constant for a given azimuth and that both stations are at the same azimuth from the epicentre, then, by subtracting equation (1) from equation (2) and rearranging, we get

$$C(\omega) = \frac{\omega}{k(\omega)} = \frac{\omega(r_2 - r_1)}{\phi_2 - \phi_1 - \phi_{i2} + \phi_{i1} + 2m\pi}.$$

The source phase shift is thus eliminated and ϕ_{i1} and ϕ_{i2} can be calculated if the instrumental constants are known. The integer m reflects the ambiguity in the identification of peaks between the two stations, and it may be determined by a knowledge of possible phase velocity values.

2. OUTLINE OF METHOD

Interstation phase velocity may be determined using several techniques [3]. The cross-multiplication method of Bloch and Hales [1] is used in this program.

The method is based on the principle that, when two signals are in phase for a given frequency, the average of their cross-multiplication function is a maximum.

The computation procedure is as follows:-

(a) Suitable earthquakes with epicentres within 4 - 5 degrees of the interstation great circle have to be chosen in order to eliminate the influence of the source radiation pattern. Their surface wave traces are then digitized at a constant sampling rate.

(b) If the instruments at the two recording stations are not identical, their instrumental phase delays have to be taken into account before further processing.

(c) The seismograms are windowed around the group arrival time of the period of interest to eliminate any disturbance in the phase velocity determination due to microseismic noise, non-least time path arrivals and other modes. The group arrival times are calculated from group velocity values which are computed outside the program [4].

(d) The signals are then narrow band-pass filtered so that both are effectively single frequency seismograms and can be represented as $A_1 \cdot \cos \omega t$ and $A_2 \cdot \cos (\omega t + \phi)$ where A_1 and A_2 are constants, and ϕ is the phase difference between the seismograms.

(e) The two records are cross-multiplied to produce:-

$$A_1 \cdot \cos \omega t \cdot A_2 \cdot \cos (\omega t + \phi) = (A_1 \cdot A_2 / 2) \cdot (\cos (2\omega t + \phi) + \cos \phi) \dots (4)$$

which represents a wave with twice the original frequency superimposed on a dc level proportional to $\cos \phi$. When the two records are in phase, $\phi = 0$, $\cos \phi = 1$ and the dc level is thus at a maximum.

(f) In practice the two filtered signals are cross-multiplied for various relative time shifts, corresponding to constant phase velocity steps, the maximum value of the dc level being recorded in each case.

(g) Steps (c) to (f) are repeated for the various periods of interest, building up to 2-D matrix of values of the maximum dc level as a function of phase velocity and period. The maxima in the contoured matrix define positive ridges which represent velocity values at which the various periods in the two seismograms are in phase. The phase velocity curve is represented by the ridge with the most reasonable velocity values.

3. PROGRAM PROCEDURE

3.1 Input data - program MAIN

Variables have the suffix 1 when referring to the station nearer to the source, and the suffix 2 for the station further away.

Each surface wave train is represented in the program as a series of digits (SEIS1(I), I = 1, NEIS1) sampled at equal time intervals, DELA, beginning from a known point in time (GMT1).

The group velocities (GV1(I), I = 1, NGV) at the periods of interest PEROD1(I) are read in to construct the group arrival time windows, enabling one to reduce the extraneous noise in the analysis.

The variables for the second station are similarly represented.

Title cards and parameter cards, which specify the operations to be carried out, are read in, together with the data (see INPUT DATA CARDS).

3.2 Preparation of the time series for analysis - program MAIN

There are options in the program to remove the mean or linear trend from the time series and to cosine taper both ends (see INPUT DATA CARDS). This eliminates the effects on the analysis of a time series superimposed on a non-zero or sloping base line and it reduces Gibb's phenomenon.

If required, either of the seismograms may be inverted by the specification of IVSEIS.

For the efficient application of the Cooley-Tukey algorithm used in the Fast Fourier Transform routine COOL, the number of points in the digital series has to be a power of two. In accordance with this, the number of points in each seismogram is increased to N points by adding zeros, where $N = 2^{**}(I + 1)$ and I is the first integer which makes N both greater than NSEIS1 and NSEIS2.

Examples of observed and synthetic seismograms are shown in figures 1 and 3.

3.3 Windowing around the group arrival time - subroutine PACKET

Both seismograms are windowed around the group arrival time of each period of interest with a time window 4.5 times the period. A symmetrical cosine taper centred on the group arrival time is then applied to these windowed seismograms.

At longer periods where the group arrival time is near the start of the time series and the time window is large, the window may extend beyond the data block. In these circumstances the program will use an asymmetrical cosine taper. In order to avoid this happening a specified number of zeros, NOZERO, can be added to the front of both seismograms (see INPUT DATA CARDS).

Examples of the windowed synthetic seismograms are shown in figure 4(a).

3.4 Band-pass filtering of the seismograms - subroutine CRUNCH

To band-pass filter both windowed seismograms, SA(I) and SB(I) simultaneously, one is put as the real, the other as the complex part of a complex array Z. The filtering is carried out in the frequency domain by the multiplication of the spectrum of Z by that of the filter function (see section 3.4.1) for both positive and negative frequency components. When the resultant spectrum is transformed back into the time domain it has as its real and imaginary parts the band-pass filtered seismograms SA'(I) and SB'(I).

3.4.1 The filter

A Gaussian function is used as the band-pass filter because of its good resolution in both the time and frequency domains. The harmonic (OMEGAC) of the Fourier analysed time series nearest to the period of interest is chosen as the centre frequency of the filter and it is at this period ($2\pi/\text{OMEGAC}$) that the phase velocity determinations are calculated.

The band-pass Gaussian filter function, with a centre frequency ω_c , is given by

$$\exp \left\{ -\alpha \left(\frac{\omega - \omega_c}{\omega_c} \right)^2 \right\},$$

where α determines the filter resolution and is specified by BAND and DWF ($\alpha = \ln \text{DWF}/\text{BAND}^2$). BAND and DWF have typical values of 0.2 and 10.0 respectively.

Examples of the band-pass filtered seismograms are given in figure 4(b).

3.5 Parameters for time shifting in cross-multiplication - MAIN

The highest phase velocity VELHI and the lowest phase velocity of interest VELLOW are read in as input parameters. The relative time shifts of the two seismograms needed to correspond with VELHI and VELLOW are specified by NMIN and NMAX, respectively. If the first point of SEIS1(I) travels at a velocity VELHI, it would arrive at the second station at a time $NMIN \times \text{DELA}$ seconds before the first point in the second seismogram (GMT2). If SEIS1(1) travels at velocity VELLOW, it would arrive at the second station $NMAX \times \text{DELA}$ seconds after GMT2.

An array TT(I) is created which corresponds to all possible time shifts required for the phase velocity range VELHI to VELLOW. The array TSTEP(I) corresponds to the time shifts required through specification of the velocity interval DV between VELHI and VELLOW.

3.6 Cross-multiplication process - subroutine OUTPUT

The cross-multiplication function, SAMSBS(I), of the windowed band-pass filtered seismograms (cf, equation (4)) for various time shifts TT(I), is computed within this subroutine, see figure 4(c).

If the first windowed filtered seismogram is represented as SA(1), SA(2), ... SA(N), and the second SB(1), SB(2), ... SB(N), then when the point SA(NMIN) travels at a velocity VELHI, it will arrive at the second station at a time corresponding to SB(1). Hence, the cross-multiplication function SAMSBS(I) for a time shift corresponding to a phase velocity of VELHI is formed by the product of SA(NMIN).SB(1), SA(NMIN+1).SB(2), ... SA(NMIN+n).SB(n+1), ... SA(N).SB(N-NMIN+1).

The value of the dc shift is determined by finding the value X_{\max} of the maximum amplitude of the product seismogram and the following minimum X_{\min} . The dc level for this particular time shift is then $(X_{\max} + X_{\min})/2$. This value is then stored in E(l) of an array of dc levels E(k), $k = 1, NP$. NP is the number of points between NMIN and NMAX.

This operation is repeated for the next time shift, which corresponds to a lower phase velocity, and an array of dc levels E(k) is built up.

	<u>TIME SHIFT</u>	<u>TT(I), I=1, NP</u>
<u>CROSS</u>	SA(NMIN).SB(1), SA(NMAX).SB(1)
<u>MULTI-</u>	SA(NMIN+1).SB(2), SA(NMAX+1).SB(2)
<u>PLICATION</u>	"	"
<u>FUNCTION</u>	SA(NMIN+n).SB(n+1), SA(NMAX+n).SB(n+1)
<u>SAMSBS(I)</u>	"	"
	↓ SA(N).SB(N-NMIN+1), SA(N).SB(N-NP)

The operation continues until a dc level has been found for all the time shift values TT(I).

Commonly, the point SA(NMIN-n), where $n < NP$, is equal to SA(1) before the whole range of time shifts has been computed. When this occurs, the role of each seismogram is reversed. SB(I) is now time shifted relative to SA(I) until the appropriate amount of time shifts are completed.

The dc levels stored in E(k) correspond to time shift values TT(I), ie. $D21/VELHI, (D21/VELHI)+DELA, \dots, D21/VELLOW$, where D21 is the distance between the two stations. These values have to be interpolated in subroutine INTPOL to produce a function X(KPER,I) (KPER is a period index) of dc levels for time shifts TSTEP(I) corresponding to the velocities of interest VSTEP(I).

3.7 The phase velocity values

The sequence of operations starting at the windowing of the seismogram (see section 3.3) is repeated for each period of interest and the dc levels are stored in subsequent columns of X(I,J) (where I is a period index and J is the dc level) which has a maximum size of 120×120 . The maximum value of X is determined and set to 99, all other values of X are then scaled accordingly. X is a 2-D matrix of dc levels as a function of period and phase velocity (see figure 2 and 5). The phase velocity curve is determined from the most reasonable maxima of the contoured matrix.

3.8 Output

The output from the program is in the form of paper print-out and graphical display.

The print-out consists of:-

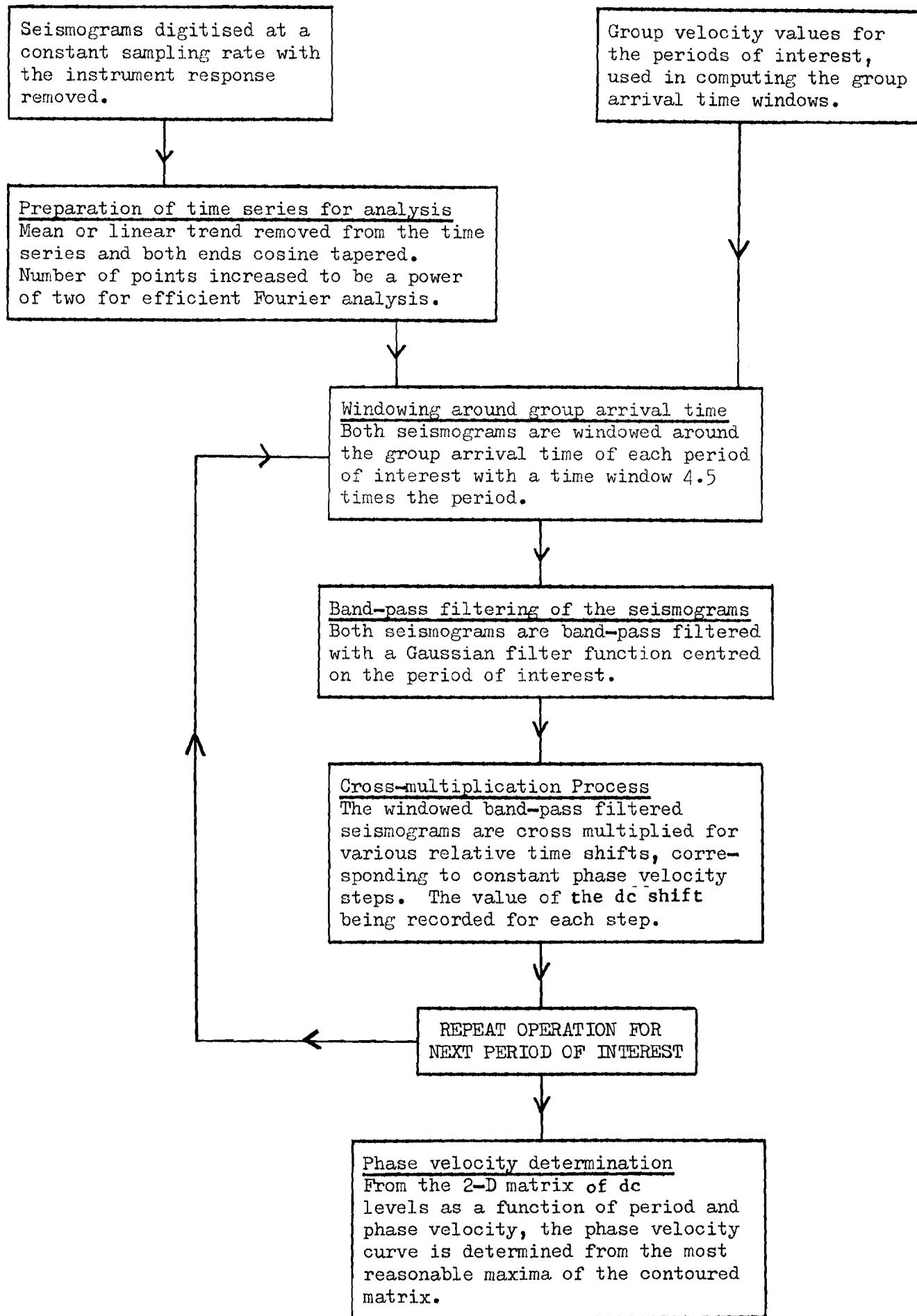
- (a) The input parameters, seismograms and group velocity data.
- (b) The 2-D matrix of the dc level of the cross-multiplied trace as a function of period and phase velocity.
- (c) An extended print-out if required (set IMTRX=1) of many of the variables calculated during the computations.

The graphical output consists of:-

- (a) The group velocity curves used in the formation of the group arrival time window.
- (b) The two seismograms prior to analysis, SEIS1 and SEIS2.
- (c) For the largest, the centre and the smallest periods of interest, the windowed seismograms (WIND1,2), the band-pass filtered seismograms (FILT1,2) and the cross-multiplication function (XMULT) for a particular time shift (when $SA(NMIN-n) = SA(1)$, $n < NP$) are graphed out.
- (d) A contour plot (positive values only) of the dc levels for the phase velocity/period array.

4. PROGRAM SPECIFICATION

The program is written in FORTRAN IV. A storage of 384K is required. The output is in the form of paper print-out and SC 4060 graphics. The maximum number of digits in the time series is 1024. The maximum size of the phase velocity/period matrix that may be requested is 120×120 .

FLOW DIAGRAM OF PROCEDURE

REFERENCES

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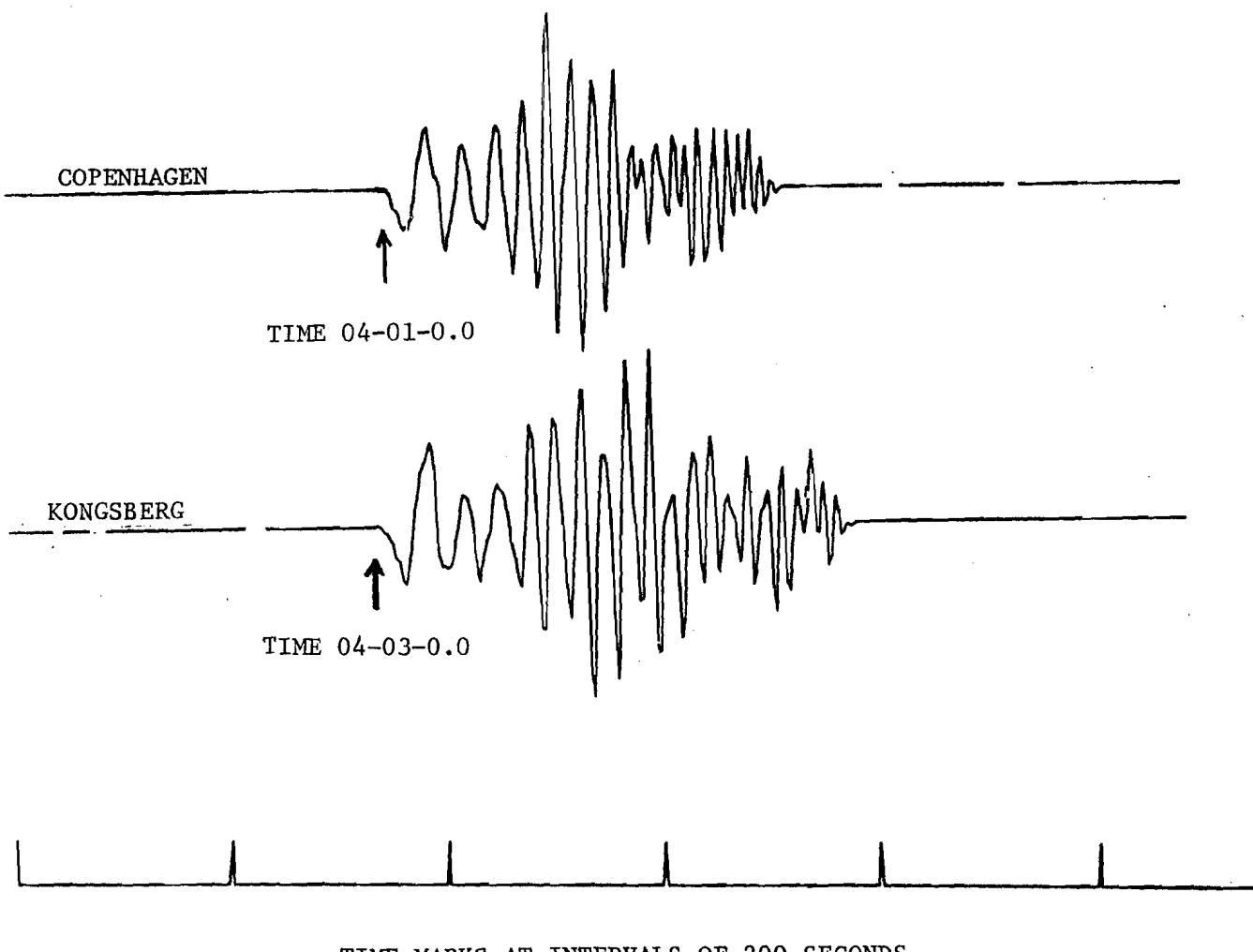


FIGURE 1. OBSERVED SEISMOGRAMS ON THE LONG PERIOD WSSN INSTRUMENTS AT COPENHAGEN (DISTANCE = 16.10 DEGREES, AZIMUTH 345.2) AND KONGSBERG (DISTANCE = 20.36 DEGREES, AZIMUTH 345.0) OF THE FUNDAMENTAL MODE RAYLEIGH WAVES FROM AN EARTHQUAKE IN ALBANIA ON THE 16TH SEPTEMBER 1972. ORIGIN TIME 03-53-26.5, EPICENTRE 40.32N, 19.69E, $M_s = 4.7$, $m_b = 5.1$

MATRIX OF X(I)																	
PERIOD, s																	
95.15	71.36	57.09	47.57	40.78	35.68	31.72	28.54	25.95	23.79	21.96	20.39	19.03					
4.25	0.2	0.5	1.0	1.7	2.1	3.0	3.7	4.4	4.8	4.7	3.8	2.9	2.0	-1.2	-4.5-13.9-20.4	-5.5-45.7-40.9-43.4	-7.3 26.5 38.0 29.6
4.23	0.2	0.5	1.1	1.7	2.2	3.1	4.0	4.9	5.4	5.5	4.8	4.0	3.1	0.1	-3.0-12.2-20.3-13.9-43.9-50.5-53.6-17.8	17.6 33.8 30.4	
4.21	0.2	0.6	1.1	1.8	2.3	3.3	4.4	5.3	6.0	6.2	5.8	5.1	4.2	1.4	-1.5 -9.8-20.5-24.7-41.6-59.6-59.9-26.9	7.8 28.4 30.5	
4.19	0.2	0.6	1.1	1.8	2.4	3.4	4.7	5.6	6.5	6.9	6.8	6.2	5.2	2.8	0.0 -6.9-20.3-35.4-39.3-66.8-61.0-33.8	-2.4 22.1 29.5	
4.17	0.2	0.6	1.1	1.8	2.5	3.6	4.9	6.0	7.0	7.5	7.7	7.2	6.2	4.2	1.8 -3.8-18.9-41.6-38.3-69.9-54.0-37.0-13.2	15.3 27.0	
4.15	0.2	0.6	1.1	1.9	2.6	3.7	5.0	6.4	7.5	8.2	8.4	8.1	7.3	5.5	3.8 -0.8-15.5-39.9-39.1-67.5-37.9-35.9-24.1	8.4 22.8	
4.13	0.2	0.6	1.1	1.9	2.6	3.8	5.2	6.7	8.0	8.8	9.1	8.9	8.3	6.9	5.9 2.2-11.2-34.6-40.0-62.6-20.6-33.8-32.6	1.3 17.5	
4.11	0.2	0.6	1.1	1.9	2.7	3.9	5.3	7.0	8.4	9.4	9.8	9.7	9.3	8.1	7.9 5.1 -6.2-26.7-40.4-56.3 -6.2-32.4-37.2 -6.1 11.6		
4.09	0.2	0.6	1.1	2.0	2.7	4.0	5.4	7.2	8.7	9.9	10.3	10.3	10.2	9.1	9.7 8.0 -1.0-18.4-38.9-50.6 -1.7-34.7-35.0-13.7 5.5		
4.07	0.2	0.5	1.1	2.0	2.8	4.0	5.5	7.4	9.0	10.2	10.9	10.9	11.0	10.0	11.1 10.6 3.9-11.6-34.7-47.3-3-12.2-43.0-24.3-21.5 -0.3		
4.05	0.2	0.5	1.1	2.0	2.8	4.1	5.7	7.5	9.2	10.4	11.3	11.4	11.6	10.8	12.2 13.2 8.6 -4.8-28.7-43.8-27.4-51.7-12.5-28.7 -5.9		
4.03	0.2	0.5	1.1	2.0	2.8	4.1	5.8	7.6	9.3	10.6	11.6	11.8	12.2	11.4	13.2 15.6 13.2 1.8-20.9-39.3-42.9-58.6 -3.0-34.7-11.3		
4.01	0.2	0.5	1.1	2.0	2.8	4.1	5.8	7.6	9.4	10.7	11.8	12.0	12.5	12.0	14.3 17.8 17.5 8.4-11.8-32.1-51.1-59.1 -3.1-39.0-16.4		
3.99	0.2	0.5	1.1	2.0	2.8	4.1	5.7	7.7	9.4	10.7	11.8	12.0	12.7	12.6	15.4 19.9 21.4 14.9 -1.7-21.7-48.4-51.8-14.3-41.1-21.1		
3.97	0.2	0.5	1.1	2.0	2.8	4.1	5.6	7.6	9.3	10.7	11.7	11.9	12.6	13.0	16.4 21.7 25.0 21.4 8.8 -9.6-39.2-40.5-28.5-41.7-24.9		
3.95	0.2	0.5	1.1	1.9	2.8	4.0	5.5	7.5	9.2	10.6	11.5	11.7	12.4	13.2	17.1 23.0 28.3 27.7 19.5 3.4-24.8-27.0-41.7-40.8-27.5		
3.93	0.2	0.5	1.0	1.9	2.7	3.9	5.4	7.4	9.0	10.2	11.2	11.4	12.1	13.1	17.4 23.8 31.3 34.1 29.4 16.1 -7.9-14.8-45.3-39.0-28.2		
3.91	0.2	0.5	1.0	1.9	2.7	3.8	5.3	7.1	8.6	9.7	10.8	10.9	11.6	12.6	17.2 24.0 33.8 40.1 38.6 28.2 10.1 -3.7-40.6-36.3-37.4		
3.89	0.2	0.5	1.0	1.8	2.6	3.7	5.2	6.9	8.2	9.2	10.3	10.3	11.0	11.9	16.6 23.7 35.6 45.1 46.8 39.8 27.8 6.8-30.5-32.3-25.7		
3.87	0.2	0.5	1.0	1.8	2.6	3.6	5.0	6.5	7.8	8.6	9.6	9.6	10.2	11.0	15.8 23.0 36.4 48.8 54.1 50.7 43.4 17.0-16.8-27.1-23.6		
3.85	0.2	0.4	0.9	1.7	2.5	3.5	4.7	6.2	7.3	8.0	8.7	8.6	9.4	10.2	14.8 22.0 36.0 50.3 60.3 60.9 53.9 27.1 -2.7-20.4-22.2		
3.83	0.2	0.4	0.9	1.7	2.3	3.3	4.4	5.8	6.7	7.4	7.8	7.4	8.4	9.2	13.5 20.6 34.6 50.4 65.0 69.6 61.9 37.4 12.1-12.4-20.2		
3.81	0.2	0.4	0.8	1.6	2.2	3.1	4.0	5.3	6.0	6.6	6.7	6.2	7.2	8.1	11.9 18.6 32.4 49.1 67.8 76.3 68.5 47.9 26.7 -3.3-16.9		
3.79	0.2	0.4	0.8	1.5	2.1	2.9	3.7	4.8	5.3	5.6	5.6	5.0	5.7	6.7	10.1 16.1 29.6 47.1 68.3 80.0 76.6 60.0 39.7 7.0-11.3		
3.77	0.2	0.4	0.8	1.5	2.0	2.7	3.4	4.2	4.5	4.4	4.4	3.7	4.0	5.1	8.0 13.0 26.3 44.4 66.4 80.9 84.8 72.0 50.9 18.0 -3.6		
3.75	0.2	0.3	0.7	1.4	1.9	2.4	3.0	3.6	3.6	3.2	3.2	2.4	2.2	3.3	5.7 9.6 22.4 40.5 62.6 79.1 90.2 81.5 60.1 29.1 5.1		
3.73	0.1	0.3	0.7	1.3	1.8	2.2	2.6	3.0	2.7	2.0	1.9	1.0	0.6	1.4	3.4 5.9 17.9 35.5 57.4 75.1 90.1 85.8 67.6 39.8 13.7		
3.71	0.1	0.3	0.6	1.2	1.6	1.9	2.1	2.3	1.7	1.1	0.5	-0.7	-0.7	-0.4	0.9 2.1 12.8 29.2 51.1 69.2 82.3 83.1 73.4 49.4 21.3		
3.69	0.1	0.3	0.6	1.1	1.4	1.6	1.6	1.6	0.8	0.3	-0.9	-2.3	-2.0	-2.3	-1.6 -1.6 7.2 21.6 42.9 60.8 71.0 76.4 76.5 57.0 28.6		
3.67	0.1	0.3	0.5	1.0	1.2	1.3	1.1	0.9	-0.0	-0.8	-2.3	-3.9	-3.5	-4.0	-4.1 -5.1 0.9 12.8 32.7 49.7 58.2 67.8 76.3 61.8 35.3		
3.65	0.1	0.2	0.4	0.8	1.1	1.0	0.6	0.2	-0.7	-2.2	-3.7	-5.1	-5.3	-5.5	-6.6 -7.9 -6.1 3.2 19.6 35.0 48.8 60.9 72.1 62.5 42.3		
3.63	0.1	0.2	0.4	0.7	0.9	0.7	0.2	-0.6	-1.3	-3.7	-5.0	-6.3	-7.2	-7.0	-9.0 -10.7 -12.8 -6.9 5.6 19.2 38.0 52.4 64.6 60.2 47.5		
3.61	0.1	0.2	0.4	0.6	0.7	0.3	-0.2	-1.3	-2.1	-5.0	-6.1	-7.4	-9.0	-8.5	-11.2 -13.8 -18.3 -16.9 -8.1 3.9 24.1 40.8 54.5 55.3 49.8		
3.59	0.1	0.1	0.3	0.5	0.5	0.0	-0.8	-2.1	-3.2	-5.9	-6.7	-8.9	-10.2	-10.7	-13.4 -18.4 -22.3 -27.4 -19.7 -7.2 2.8 23.8 43.0 49.2 47.3		
3.57	0.1	0.1	0.2	0.3	0.3	-0.3	-1.4	-2.8	-4.5	-6.5	-7.2	-10.2	-10.8	-12.2	-14.7 -22.2 -23.5 -34.7 -29.0 -17.5 -21.1 3.5 29.3 41.0 41.4		
3.55	0.1	0.1	0.1	0.2	0.0	-0.7	-2.0	-3.4	-5.6	-7.0	-7.7	-10.9	-10.6	-12.5	-14.6 -23.7 -21.4 -36.4 -35.5 -29.0 -44.2 -17.9 13.1 30.4 33.3		
3.53	0.0	0.1	0.0	0.1	-0.2	-1.0	-2.4	-4.1	-6.2	-7.7	-8.9	-10.3	-9.0	-9.7	-11.6 -19.5 -13.7 -26.1 -38.3 -46.5 -63.9 -40.8 -7.0 17.2 25.0		
3.51	0.0	0.0	0.0	-0.1	-0.4	-1.3	-2.8	-4.7	-6.5	-8.5	-10.1	-9.3	-7.3	-6.3	-8.0 -13.7 -5.8 -13.9 -39.6 -63.5 -74.2 -56.9 -27.5 1.8 15.7		
3.49	0.0	-0.0	-0.0	-0.2	-0.6	-1.7	-3.1	-5.3	-6.3	-9.1	-11.0	-8.7	-6.1	-4.0	-5.6 -9.3 -1.8 -6.7 -41.0 -75.8 -71.4 -60.6 -45.4 -15.0 5.2		
3.47	0.0	-0.0	-0.0	-0.1	-0.4	-0.8	-1.9	-3.6	-6.1	-5.8	-9.4	-10.7	-9.5	-7.0	-5.9 -7.5 -11.9 -9.4 -18.1 -45.7 -75.0 -44.4 -38.2 -56.0 -34.6 -8.0		
3.45	-0.0	-0.0	-0.1	-0.2	-0.5	-1.0	-2.2	-4.0	-6.5	-5.4	-9.6	-10.0	-9.5	-7.0	-5.9 -9.0 -10.6 -16.1 -20.0 -34.2 -50.6 -68.8 -15.5 -13.1 -63.1 -48.7 -20.2		
3.43	-0.0	-0.1	-0.3	-0.6	-1.2	-2.6	-4.5	-6.4	-5.4	-9.6	-9.4	-11.1	-9.8	-11.3	-12.8 -8 -18.6 -27.7 -46.1 -53.9 -62.0 -1.5 -2.4 -68.9 -50.3 -28.6		

FIGURE 2. 2-D MATRIX OF NORMALISED DC LEVELS AS A FUNCTION OF PERIOD AND PHASE VELOCITY FOR THE INTERSTATION PHASE VELOCITY DETERMINATION BETWEEN THE WWSSN STATIONS OF COPENHAGEN AND KONGSBERG. THE DOTS REPRESENT THE COMPUTED PHASE VELOCITY CURVE

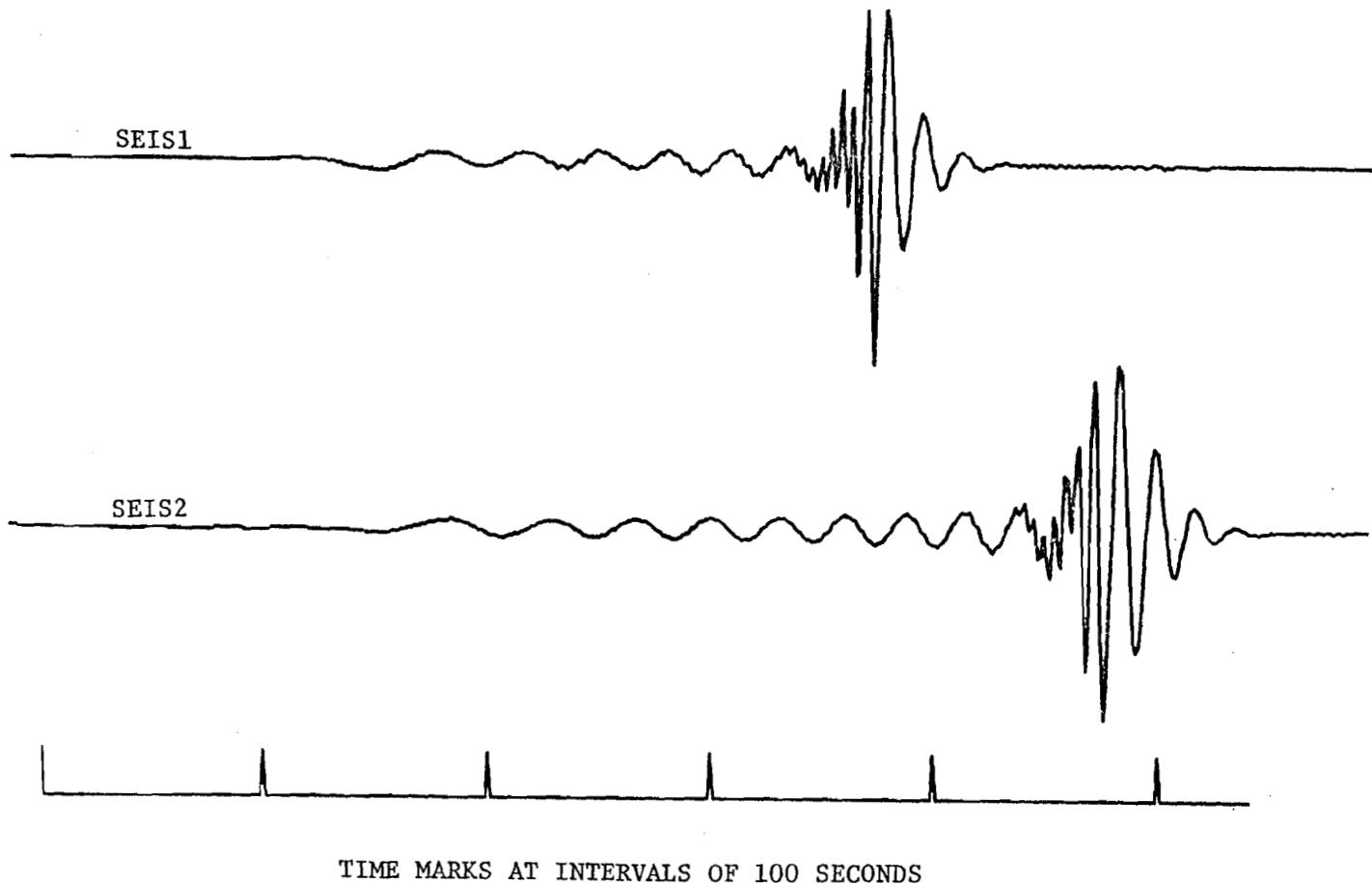


FIGURE 3. SYNTHETIC, FUNDAMENTAL MODE, RAYLEIGH WAVE SEISMOGRAMS COMPUTED (SEE DOUGLAS, HUDSON AND BLAMEY [5]) FOR A 25000 KTON EXPLOSION IN AIR AT EPICENTRAL DISTANCES OF 30.0 (SEIS1) AND 40.0 (SEIS2) DEGREES, RECORDED BY STANDARD WWSSN LONG PERIOD INSTRUMENTS. THE DETAILS OF THE STANDARD CONTINENTAL STRUCTURE USED IN THE COMPUTATION IS SHOWN BELOW

STANDARD CONTINENTAL CRUST (KANAMORI [6])

	P WAVE VELOCITY (km s ⁻¹)	S WAVE VELOCITY (km s ⁻¹)	DENSITY (g cm ⁻³)	THICKNESS (km)
1st LAYER	6.10	3.50	2.70	11.0
2nd LAYER	6.40	3.68	2.90	9.0
3rd LAYER	6.70	3.94	2.90	18.0
HALF SPACE	8.15	4.75	3.30	∞

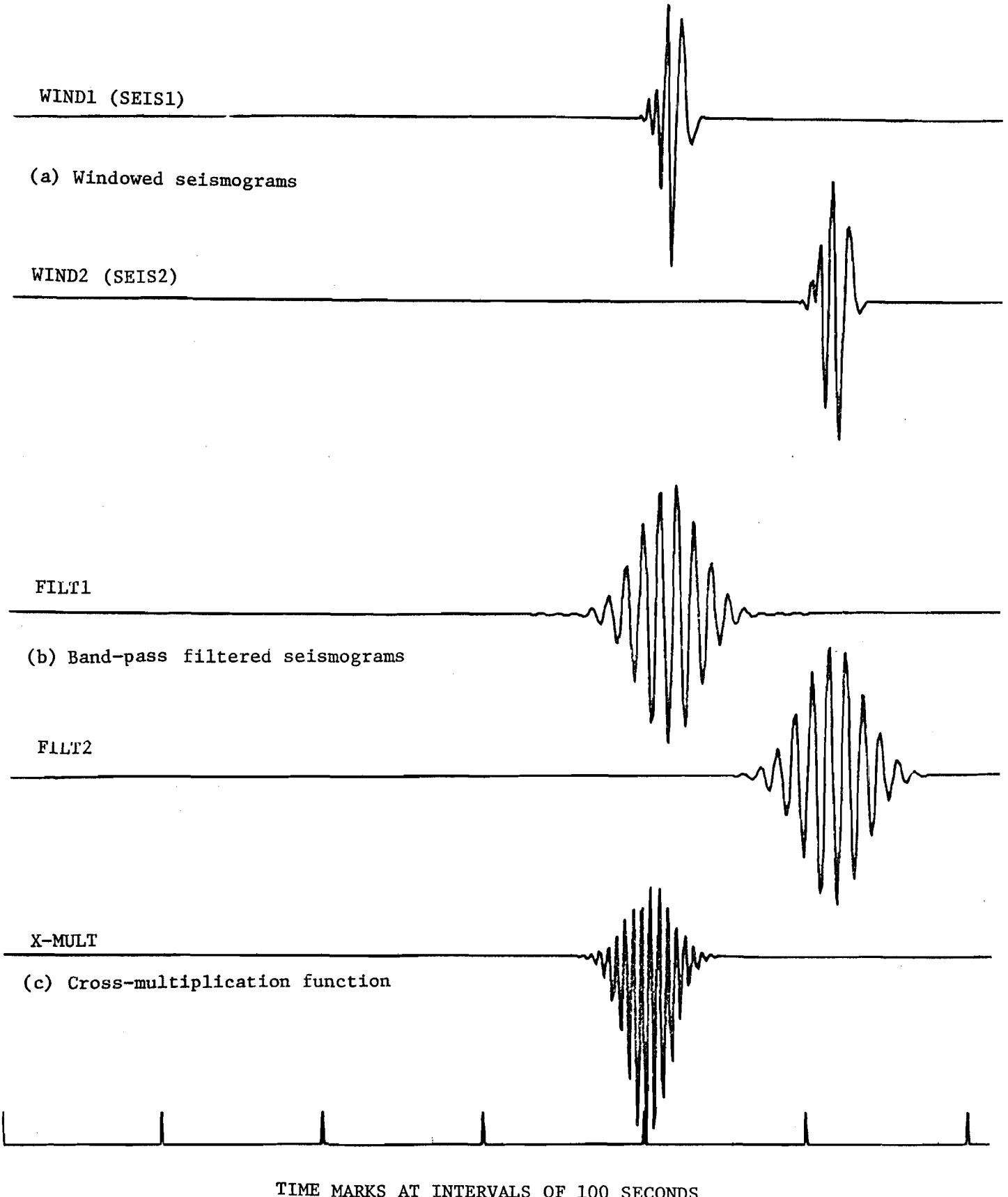


FIGURE 4. (a) SEISMOGRAMS WINDOWED AROUND THE GROUP ARRIVAL TIME OF 10.5 SECOND PERIOD WITH A WINDOW 4.5×10.5 s IN LENGTH AND THEN SYMMETRICALLY COSINE TAPERED
 (b) BAND-PASS FILTERED SEISMOGRAMS, FILTERED IN THE FREQUENCY DOMAIN BY A GAUSSIAN FILTER CENTRED ON 10.5 s PERIOD
 (c) CROSS-MULTIPLICATION FUNCTION OF THE TWO FILTERED SEISMOGRAMS FOR A PARTICULAR TIME SHIFT

MATRIX OF X(I)

PERIOD, s

56.89	39.38	31.12	24.38	20.48	17.66	15.52	13.84	12.49	11.38	10.45														
4.50	0.1	-0.1	-0.3	-0.1	0.4	0.0	-0.6	1.1	-0.4	1.2	-0.8	0.2	0.3	-0.3	0.3	-0.1	0.1	-0.0	0.0	0.0	0.0			
4.48	0.1	-0.0	-0.3	-0.2	0.4	0.2	-0.5	1.2	-0.9	1.0	-0.3	-0.2	0.6	-0.3	0.4	-0.1	0.1	-0.0	-0.0	0.0	0.0	0.0		
4.46	0.1	-0.0	-0.3	-0.3	0.3	0.3	-0.8	1.2	-1.0	0.6	0.1	-0.7	0.9	-0.1	0.3	-0.1	0.1	0.0	-0.0	0.0	0.0	0.0		
4.44	0.1	0.0	-0.2	-0.3	0.2	0.5	-0.6	1.1	-0.6	0.1	0.7	-1.1	1.0	-0.5	0.2	-0.0	-0.0	0.1	0.0	0.0	0.0	0.0		
4.42	0.1	0.1	-0.2	-0.3	0.1	0.6	-0.8	0.8	-0.3	-0.4	1.2	-0.8	0.9	-0.2	0.0	0.2	-0.1	0.2	0.0	0.0	0.0	0.0		
4.40	0.1	0.1	-0.2	-0.3	0.0	0.7	-0.7	0.5	0.2	-1.0	1.6	-0.8	0.6	-0.0	-0.2	0.3	-0.1	0.2	-0.0	-0.0	0.0	0.0		
4.38	0.1	0.1	-0.1	-0.3	-0.1	0.7	-0.5	0.2	0.8	-1.6	1.8	-1.0	0.1	0.4	-0.4	0.4	-0.1	0.1	0.0	-0.1	0.1	0.0		
4.36	0.1	0.2	-0.1	-0.4	-0.2	0.7	-0.3	-0.2	1.3	-0.2	1.6	-0.5	-0.5	0.8	-0.0	0.4	-0.1	-0.0	0.1	-0.0	0.0	0.0		
4.34	0.1	0.2	0.0	-0.3	-0.3	0.6	0.1	-0.7	1.6	-1.7	1.2	0.3	-1.1	1.1	-0.4	0.3	0.1	-0.2	0.2	-0.1	0.0	0.0		
4.32	0.1	0.2	0.1	-0.3	-0.4	0.5	0.4	-1.0	1.8	-1.6	0.4	1.0	-0.9	1.1	-0.3	0.0	0.3	-0.2	0.2	-0.0	-0.0	0.0		
4.30	0.1	0.2	0.1	-0.2	-0.5	0.3	0.7	-1.0	1.8	-1.0	-0.5	1.8	-0.2	0.8	0.1	-0.3	0.4	-0.1	0.1	0.1	0.0	0.0		
4.28	0.1	0.2	0.2	-0.2	0.1	1.0	-1.3	1.5	-0.2	-1.4	2.2	-1.2	0.2	0.5	-0.4	0.5	-0.1	-0.1	0.2	-0.0	0.0	0.0		
4.26	0.1	0.2	0.2	-0.1	-0.5	-0.1	1.1	-1.5	1.0	0.7	-2.3	2.2	-0.7	-0.5	1.0	-0.3	0.4	0.1	-0.2	0.2	-0.0	0.0		
4.24	0.1	0.2	0.3	0.0	-0.5	-0.3	1.2	-1.2	0.3	1.6	-0.1	1.7	0.3	-1.2	1.2	-0.3	0.1	0.4	-0.0	0.1	0.1	0.1		
4.22	0.1	0.2	0.3	0.1	-0.4	-0.5	1.2	-0.8	-0.5	2.4	-2.5	0.7	1.4	-1.3	1.1	-0.1	-0.4	0.6	-0.2	-0.0	0.2	0.0		
4.20	0.1	0.2	0.3	0.2	-0.3	-0.6	1.0	-0.1	-1.3	2.8	-2.0	-0.5	2.3	-0.8	0.6	0.5	-0.4	0.6	-0.0	-0.3	0.0	0.2		
4.18	0.1	0.2	0.3	0.3	-0.2	-0.6	0.7	0.5	-1.6	2.7	-0.8	-1.9	2.8	-1.1	-0.3	1.1	-0.6	0.3	0.3	-0.0	0.1	0.1		
4.16	0.1	0.2	0.3	0.3	-0.1	-0.7	0.4	1.2	-0.8	2.3	0.6	-2.4	2.6	-0.3	1.2	1.5	-0.5	-0.1	0.6	-0.2	-0.1	0.1		
4.14	0.0	0.2	0.3	0.4	0.1	-0.8	-0.0	1.8	-2.3	1.2	2.2	-1.9	1.6	-0.9	1.3	0.2	-0.7	0.7	-0.0	-0.1	0.0	0.0		
4.12	0.0	0.1	0.3	0.4	0.2	-0.7	-0.5	2.2	-2.0	-0.2	3.5	-3.1	-0.1	2.5	-1.0	0.7	0.8	-0.2	0.4	0.3	-0.1	0.1		
4.10	0.0	0.1	0.2	0.4	0.4	-0.6	-0.8	2.3	-1.4	-1.6	4.0	-1.4	-2.0	3.2	-1.0	-0.6	1.5	-0.5	-0.2	0.7	-0.3	0.1		
4.08	-0.0	0.0	0.2	0.4	0.5	-0.3	-1.3	2.1	-0.2	-3.3	3.9	0.0	-3.4	3.0	0.3	-1.5	1.6	-0.0	-0.7	0.7	0.1	0.1		
4.06	-0.0	-0.0	0.1	0.4	0.6	-0.1	-0.7	1.5	1.1	-1.0	2.8	2.4	-4.3	1.7	1.7	-1.4	1.0	0.9	-0.7	0.3	0.6	0.1		
4.04	-0.0	-0.0	0.1	0.3	0.6	0.2	-1.3	0.8	2.3	-3.6	0.7	4.3	-2.0	-0.4	3.2	-1.6	-0.3	1.8	-0.7	-0.6	0.9	0.1		
4.02	-0.1	-0.1	-0.0	0.2	0.6	0.5	-1.4	0.0	3.2	-3.2	-1.6	5.4	-2.3	-2.8	3.6	-0.3	-1.9	1.9	0.2	-0.6	0.5	0.1		
4.00	-0.1	-0.1	0.1	0.1	0.7	1.0	-0.9	3.6	-1.7	-3.8	5.2	0.9	-4.6	2.5	1.4	-0.5	1.0	1.4	-0.8	-0.3	0.3	0.1		
3.98	-0.1	-0.2	0.0	0.5	0.9	-0.5	-1.6	3.4	0.5	-3.2	3.2	3.9	-2.5	0.4	3.5	-2.1	-0.8	2.2	-0.3	-0.7	0.0	0.1		
3.96	-0.1	-0.2	0.0	-0.1	0.3	1.0	0.0	-2.2	2.5	2.8	-3.7	0.2	6.2	-3.5	-2.7	4.2	-0.1	-2.3	1.8	1.2	-0.7	0.1		
3.94	-0.1	-0.2	0.3	-0.2	0.2	1.0	0.7	-2.4	1.2	4.6	-4.5	-3.3	6.8	0.3	-2.5	3.2	2.0	-0.2	0.2	2.2	-0.7	0.1		
3.92	-0.1	-0.2	0.3	-0.3	-0.0	0.8	1.2	-2.6	-0.5	5.7	-1.9	-7.0	5.1	3.9	-2.8	0.4	4.1	-1.9	-2.2	2.2	1.1	0.1		
3.90	-0.1	-0.3	0.4	-0.2	0.6	1.6	-1.9	-2.8	5.6	1.5	-1.5	1.3	7.0	-2.6	-2.5	4.4	1.1	-0.7	0.4	2.6	0.6	0.1		
3.88	-0.1	-0.2	0.3	-0.4	0.3	1.8	-0.7	-4.1	4.0	5.2	-6.9	-3.6	8.0	0.3	-2.7	2.3	4.0	-2.1	-2.2	2.3	0.1	0.1		
3.86	-0.1	-0.2	0.3	-0.0	-0.5	0.0	1.8	0.5	-2.7	1.3	8.0	-3.3	-7.8	5.8	4.8	-2.9	-1.3	5.3	0.7	-1.3	0.1	0.1		
3.84	-0.1	-0.2	0.3	-0.5	-0.7	1.0	1.9	-4.6	-1.9	8.4	1.6	-8.0	0.9	8.4	-2.0	-5.9	3.6	4.1	-2.6	-3.1	0.1			
3.82	-0.1	-0.2	0.3	-0.6	-0.3	0.9	3.1	-3.2	-4.9	6.5	6.7	-6.4	-5.5	8.5	3.5	-2.0	-1.1	6.1	1.2	-0.7	0.1			
3.80	-0.1	-0.1	-0.2	-0.3	-0.7	-0.9	0.2	0.6	-1.0	-3.4	2.7	10.5	-3.2	-7.0	3.8	8.3	-3.2	-5.6	3.9	5.1	-2.3			
3.78	-0.1	-0.1	-0.2	-0.5	-1.1	-1.6	3.5	1.6	-7.5	-2.3	11.1	4.4	-10.1	-3.8	9.4	2.3	-0.9	-1.5	6.4	2.5	0.1			
3.76	-0.1	-0.1	0.0	-0.1	-0.4	-1.0	1.2	2.8	4.1	-5.6	-7.7	7.6	10.9	-6.2	7.1	6.4	8.5	-4.2	-7.3	2.8	6.9			
3.74	-0.1	-0.0	0.0	0.0	0.2	-0.8	-1.6	1.6	5.8	-2.0	-9.1	0.9	14.0	1.5	-5.8	-1.8	10.7	3.8	-3.3	-4.6	6.1			
3.72	-0.0	0.0	0.1	0.2	0.0	-0.7	-0.6	0.1	6.2	2.6	-10.4	-6.8	11.9	11.0	-7.2	-9.0	6.2	10.6	-2.7	-2.8	-0.6			
3.70	-0.0	0.1	0.2	0.3	0.3	-0.3	-2.2	-1.7	5.1	6.8	-6.7	12.2	4.2	16.5	0.3	-10.6	-3.3	11.8	7.5	-6.1	-7.9			
3.68	0.0	0.1	0.3	0.4	0.5	0.1	-1.6	-3.1	2.8	9.5	0.1	-14.6	-6.2	14.7	10.9	-6.4	-11.4	4.2	13.3	3.8	-4.4			
3.66	0.0	0.2	0.3	0.4	0.6	0.6	-0.9	-2.4	-0.5	9.8	7.5	-9.7	-16.6	5.9	17.7	2.1	-6.2	-8.7	10.0	12.6	-1.2			
3.64	0.1	0.2	0.3	0.5	0.7	0.9	0.1	-4.0	-4.1	7.1	13.0	-1.9	-8.4	-7.4	15.4	15.4	-6.7	-9.4	-2.3	14.2	12.6			
3.62	0.1	0.2	0.4	0.5	0.7	1.2	1.0	-3.1	-6.9	2.0	14	5	8.8	-13.9	18.9	3.6	20.8	9.1	-11.6	16.2	2.0	16.8		
3.60	0.1	0.2	0.3	0.4	0.6	1.2	1.8	-1.3	-6.7	-4.4	11	0	-9.0	-9.1	13.9	12.9	20.2	3.4	-12.2	14.5	5.0			
3.58	0.1	0.2	0.3	0.3	0.5	1.1	2.3	1.0	-6.2	-10.8	3.2	19	6	14.2	-10.7	-13.5	-4.4	18.9	19.5	-1.0	-7.6	-12.5		
3.56	0.1	0.2	0.2	0.2	0.3	0.8	2.4	3.2	-3.4	-1.4	6.6	13	7	23	9	6.8	-14.1	-21.1	3.1	23.7	18.5	-1.7	-11.5	
3.54	0.1	0.2	0.1	0.0	0.1	0.4	2.0	4.7	1.1	-10.6	-14.8	0.6	23	1	-5.1	-20.5	-18.8	8.3	26.4	17.9	-6.0			
3.52	0.1	0.2	0.0	-0.1	-0.3	-0.2	1.2	5.2	5.5	-4.8	-14.8	-14.1	10.4	27	17.7	-8.3	-14.6	-18.2	10.9	28.6	21.5			
3.50	0.1	0.1	-0.0	-0.3	-0.5	-0.7	0.1	4.3	8.6	3	11	-13.6	-11.9	-9.3	19.1	31	6	13.6	-17.6	-17.8	-17.3	11.9	31.6	
3.48	0.1	0.1	-0.1	-0.4	-0.7	-1.0	-1.1	2.2	9.1	10.7	-2.8	-20.3	-26.3	-2.2	25.9	22	12.5	-17.8	-17.7	-23.9	7	31.6		
3.46	0.1	0.0	-0.2	-0.5	-0.7	-0.9	-1.6	-0.4	6.7	14.9	10.0	-10.3	-11.0	-27.1	1	9	30.8	36	3	13.4	-17.7	-8.3	-29.6	
3.44	0.1	-0.0	-0.3	-0.4	-0.7	-1.2	-2.3	-2.7	2.0	13.9	19.6	8	2	-17.9	-16.4	-24.7	3	6	31.3	3	21.6	-9.5	-27.5	
3.42	0.1	-0.1	-0.3	-0.6	-1.0	-2.5	-4.7	-3.7	7.6	21	3	24	2	6.4	-22.4	-32.6	-29.5	-0.1	31.8	46	35	6	5.7	
3.40	0.1	-0.1	-0.2	-0.3	-0.6	-1.9	-5.2	-8.5	-2.1	13	4	29	2	29.5	8	2	-21.8	-42.3	-37.4	-9.3	26	2	49	
3.38	0.0	-0.2	-0.3	-0.2	-0.0	-0.0	-0.7	-4.4	-9.9	-11.2	-2	-1.4	19	2	37.0	36	9	13.4	-17.9	-33.3	-37.8	25.6	9	40.8
3.36	0.0	-0.2	-0.2	-0.1	0.2	0.6	0.6	-2.1	-8.8	-2.6	-16	6	-1.9	23	0	43.7	44.4	22.6	-9.7	-34.3	25.1	-43.8	-18.2	
3.34	-0.0	-0.2	-0.2	0.1	0.5	1.1	1.8	1.2	-4.0	-15.3	-7.9	-19.4	-6.7	21.5	45.5	51.8	36.8	8	7	-24.8	-33.8	-49.5		
3.32	-0.0	-0.1	-0.1	0.3	0.7	1.3	2.6	4.3	2.7	-5.7	-22.6	-30	9	-32.1	-16.3	11.8	39.5	54.5	55.3	40.0	14.7	-22.3		
3.30	-0.0	-0.2	-0.0	0.4	0.7	1.3	2.7	6.1	8.8	6.1	-6.5	-25	1	-39.3	-45.5	7	37.2	-8.1	21.2	48.4	66.2	69.4	55.0	
3.28	-0.1	-0.2	0.1	0.4	0.7	1.0	2.1	6.0	11.6	16.1	12.5	-0.7	-22.4	-42.6	-45.2	52.6	-35.9	-12.6	18.5	49.3	69.1			
3.26	-0.1	-0.1	0.2	0.5	0.5	0.5	1.0	3.9	10.0	19.4	26.0	25.3	14.0	-5.7	-28.0	-48.6	-60.4	-36.1	-55.0	-32.6	-7.7			

FIGURE 5. 2-D MATRIX OF NORMALISED DC LEVELS AS A FUNCTION OF PERIOD AND PHASE VELOCITY FOR THE SYNTHETIC SEISMograms. BLACK DOTS REPRESENT THE COMPUTED PHASE VELOCITY, THE DASHED LINE REPRESENTS THE ACTUAL PHASE VELOCITY CURVE. PROCESSING ERROR FOR ALL PERIODS IS BETTER THAN ± 0.015 km/s

APPENDIX A

PROGRAM LISTING

INTERSTATION PHASE VELOCITY PROGRAM (IPV)

THE PROGRAM COMPUTES THE PHASE VELOCITY OF A DISPERSED SEISMIC SIGNAL BETWEEN TWO STATIONS FROM A SOURCE WHICH IS ON OR NEAR THE INTERSTATION GREAT CIRCLE. THE SEISMOGRAMS, WHICH ARE REPRESENTED IN THE PROGRAM AS DIGITS SAMPLED AT EQUAL INTERVALS, ARE INITIALLY WINDOWED AROUND THE GROUP ARRIVAL TIME OF THE VARIOUS PERIODS OF INTEREST IN ORDER TO ELIMINATE EXTRANEOUS NOISE. BOTH SEISMOGRAMS ARE THEN PASSED THROUGH A NARROW BAND PASS DIGITAL FILTER CENTRED AT VARIOUS PERIODS AND THEIR CROSS PRODUCT FORMED FOR A NUMBER OF TIME SHIFTS CORRESPONDING TO CONSTANT PHASE VELOCITY STEPS. THE AVERAGE OF THE RESULTANT TIME SERIES IS A MAXIMUM WHEN THE TWO SIGNALS ARE IN PHASE. THE PHASE VELOCITY DISPERSION IS DETERMINED FROM A CONTINUED MATRIX CONSISTING OF AVERAGES AS A FUNCTION OF PHASE VELOCITY AND PERIOD.

GENERAL REFERENCE --- "NEW TECHNIQUES FOR THE DETERMINATION OF SURFACE WAVE PHASE VELOCITIES" S.BLOCH AND A.L.HALES, BULL.SEISM.SOC.AM. 58, 1021-1034.

* * * * *

NOTES FOR USERS.

- 1) ENSURE THAT GROUP VELOCITY VALUES ARE AT THE SAME PERIODS AND OVER THE SAME RANGE IN EACH RECORD.
- 2) SELECT THE RANGE OF PERIODS OVER WHICH THE GROUP VELOCITY VALUES LOOK SENSIBLE.
- 3) FIRST SEISMOGRAM, STATION ETC. IS NEARER THE SOURCE, THE SECOND SEISMOGRAM, STATION ETC. IS FURTHER FROM THE SOURCE.

INPUT DATA CARDS

CARD 1
----- FORMAT (10A8)

TITLEA----TITLE FOR THE DATA SET (10A8)

CARD 2
----- FORMAT (8A1,F12.5,I2,I2,F3.1,3X,8A1,F12.5,I2,I2,F3.1,16X,
I2,I2,F3.1)

STNAM1----NAME OF THE RECORDING STATION NEARER THE SOURCE
(8A1)

DELTA1----DISTANCE IN DEGREES BETWEEN STNAM1 AND THE SOURCE
1 DEGREE = 111.1 KM (F12.5)

MGMT1----HOURS (I2) GMT TIME OF FIRST SAMPLE IN THE
MNGMT1----MINUTES (I2) FIRST SEISMOGRAM

SCGMT1----SECONDS (F3.1)

STNAM2----NAME OF RECORDING STATION FURTHER FROM
THE SOURCE (8A1)

DELTA2----DISTANCE IN DEGREES BETWEEN STNAM2 AND SOURCE
(F12.5)

MGMT2----HOURS (I2) GMT TIME OF FIRST SAMPLE IN THE
MNGMT2----MINUTES (I2) SECOND SEISMOGRAM
SCGMT2----SECONDS (F3.1)

M HOUR ----HOURS (I2) GMT ORIGIN
MIN ----MINUTES (I2) TIME
SEC ----SECONDS (F3.1)

CARD 3
----- FORMAT (4I10,3F10.5)

NSEIS1----NUMBER OF SAMPLES IN THE FIRST SEISMOGRAM, NOT
MORE THAN 1024 (I10)

NSEIS2----NUMBER OF SAMPLES IN THE SECOND SEISMOGRAM, NOT

C MORE THAN 1024 (I10)
 C
 C NCV ---- NUMBER OF GROUP VELOCITY / PERIOD VALUES FOR THE
 C TWO SEISMGRAMS, NOT MORE THAN 120 (I10)
 C
 C NCOSTP----NUMBER OF POINTS IN COSINE TAPER OF BOTH ENDS OF
 C SIGNAL, IF NCOSTP=0 NO COSINE TAPER APPLIED
 C
 C DELA ---- INTERVAL BETWEEN SAMPLES IN SECONDS (F10.5)
 C
 C VELHI ---- HIGHEST PHASE VELOCITY OF INTEREST (F10.5)
 C
 C VELLOW----LOWEST PHASE VELOCITY OF INTEREST (F10.5)
 C
 C
 C CARD 4
 C ----- FORMAT (1X,A8,1X,3I10,3I5)
 C
 C TYPE ---- IF "TYPE"=MEAN, MEAN BASELINE REMOVED FROM SIGNALS
 C IF "TYPE"=LEAST, LEAST SQUARES BASELINE IS REMOVED
 C (A8)
 C
 C NZERO---- "NZERO" NUMBER OF ZEROS ADDED TO THE FRONT OF
 C BOTH SEISMGRAMS (I10)
 C
 C INTRX ---- IF "INTRX"=1, AN EXTENDED PRINT OUT IS OBTAINED.
 C (I10)
 C
 C IVSEIS---- INVERT THE FIRST SIGNAL IF "IVSEIS"=1, THE SECOND
 C IF "IVSEIS"=2 (I10)
 C
 C N1 ---- IF N1=1, GROUP VELOCITY CURVES AND ORIGINAL
 C SEISMGRAMS GRAPHED. (I5)
 C
 C N2 ---- IF N2=1, WINDOWED, BAND-PASS FILTERED AND CROSS-
 C MULTIPLIED TRACES GRAPHED FOR THE LONGEST, CENTRE
 C AND SHORTEST PERIODS.
 C
 C N3 ---- IF N3=1, COUNTS PLCT OF POSITIVE VALUES OF 2-D
 C MATRIX ARE GRAPHED.
 C
 C
 C CARD 5
 C ----- FORMAT (3F10.5)

C
 C BAND ---- RELATIVE BANDWIDTH OF GAUSSIAN FILTER (F10.5)
 C
 C DAF ---- DECAY RATE OF GAUSSIAN FILTER FUNCTION (F10.5)
 C
 C DV ---- THE VELOCITY INTERVAL BETWEEN PHASE VELOCITY
 C VALUES, IF DV LEFT BLANK IT IS SET TO 0.02 KM/SEC
 C (NOT MORE THAN 120 INTERVALS BETWEEN VELHI AND
 C VELLOW)
 C
 C
 C CARD 6
 C ----- FORMAT (2E15.7)
 C
 C PERIOD1 (I) PERIODS AT WHICH GROUP VELOCITIES ARE GIVEN
 C I=1,NGV FOR FIRST SEISMGRAM
 C
 C GV1 (I) GROUP VELOCITY VALUES FOR THE ABOVE PERIODS
 C I=1,NGV
 C
 C CARD 7
 C ----- FORMAT (2E15.7)
 C
 C PERIOD2 (I) PERIODS AT WHICH GROUP VELOCITIES ARE GIVEN
 C I=1,NGV FOR SECOND SEISMGRAM
 C
 C GV2 (I) GROUP VELOCITY VALUES FOR THE ABOVE PERIODS
 C I=1,NGV
 C
 C CARD 8
 C ----- FORMAT (10A8)
 C
 C TITLE1----TITLE FOR THE FIRST SEISMGRAM (10A8)
 C
 C CARD 9
 C ----- FORMAT (10A8)
 C
 C FMT1 ---- INPUT FORMAT FOR FIRST SEISMGRAM (10A8)
 C BRACKETS MUST BE PLACED AROUND ARGUMENT
 C
 C
 C CARD 10
 C ----- FORMAT FMT1
 C
 C SEIS1 (I) DIGITAL SEISMIC SIGNAL FROM FIRST STATION,
 C I=1,NSEIS1 NOT MORE THAN 1024 POINTS (FMT1)


```

6   FORMAT(4I10,3F10.5)
NGV1=NGV
NGV2=NGV
READ 7,TYPE,NOZERC,IMTRX,IVSEIS,NG1,NG2,NG3
7   FCRMAT(1X,A8,1X,3I10,3I5)
READ 8,BAND,DWF,DV
8   FCRMAT(3F10.5)
READ 9,(PER001(I),GV1(I),I=1,NGV1)
READ 9,(PER002(I),GV2(I),I=1,NGV2)
9   FCRMAT(2E15.7)

C   CONVERSION TO BASIC UNITS OF TIME(SECS) AND DISTANCE(KMS.)
GMT1=3600.0*FLOAT(MHGMT1)+60.0*FLCAT(MNGMT1)+SCGMT1-
1FLCAT(N0ZER0)*CELA
GMT2=3600.0*FLCAT(MHGMT2)+60.0*FLCAT(MNGMT2)+SCGMT2-
1FLCAT(N0ZER0)*CELA
ORIGTM=3600.0*FLCAT(MHCUR)+60.0*FLCAT(MIN)+SEC
DELTAL1=DELTAL1*111.1
DELTAL2=DELTAL2*111.1
D21=DELTAL2-DELTAL1
IF(DV.EQ.0.0)DV=0.02

C   FILTER CHARACTERISTICS
BETA=ALOG(DWF)
ALPHA=BETA/BAND**2

C   CALCULATE TIME SHIFT FACTORS FOR CROSS-MULTIPLICATION
NCZER1 = NOZERC
TMAX=D21/VELLOW+3.0*DELA
TMIN=D21/VELHI-3.0*DELA
NMIN=(GMT2-GMT1-TMIN)/DELA+1.0
IF (NMIN.GT.0) GO TO 33
NCZER1 = NCZER1-NMIN + 1
GMT1 = GMT1 + FLOAT (NMIN-1) * CELA
33  NSEIS1=NSEIS1+NOZER1
NSEIS2=NSEIS2+NOZERC
NCZERC=NCZER1+1
NCZER1=NCZER1+1
NMIN=(GMT2-GMT1-TMIN)/DELA+1.0
NMAX=(TMAX-GMT2+GMT1)/DELA+1.0
TMIN=GMT2-GMT1-FLAT(NMIN-1)*DELA
TMAX=GMT2-GMT1+FLAT(NMAX-1)*DELA
NF=NMAX-NMIN+1
TT(1)=TMIN

```

```

DC 34 I=2,NP
TT(I)=TT(I-1)+CELA
CCONTINUE

C   READ 4,(TITLE1(I),I=6,15)
READ 4,(FMT1(I),I=1,10)
REAL FMT1,(SEIS1(I),I=NOZER1,NSEIS1)
READ 4,(TITLE2(I),I=6,15)
READ 4,(FMT2(I),I=1,10)
READ FMT2,(SEIS2(I),I=NOZERC,NSEIS2)

C   PRINT OUT INPUT DATA AND PARAMETERS
PRINT 11,CATE
PRINT 12
PRINT 13,(TITLEA(I),I=6,15)
PRINT 14,MHOUR,MIN,SEC,ORIGTM
PRINT 15,STNAM1,DELTAL1,MHGMT1,MNGMT1,SCGMT1,GMT1
PRINT 15,STNAM2,DELTAL2,MHGMT2,MNGMT2,SCGMT2,GMT2
PRINT 16,NSEIS1,NSEIS2,NGV1,NGV2,NCUSTP,DELA,VELHI,VELLOW,DV
PRINT 17,BAND,DWF,NG1,NG2,NG3
PRINT 18,TYPE,NOZERC,IMTRX,IVSEIS
PRINT 19
PRINT 13,(TITLE1(I),I=6,15)
PRINT 4,(FMT1(I),I=1,10)
PRINT 20,(I,SEIS1(I),I=NOZER1,NSEIS1)
PRINT 21
PRINT 13,(TITLE2(I),I=6,15)
PRINT 4,(FMT2(I),I=1,10)
PRINT 20,(I,SEIS2(I),I=NOZERC,NSEIS2)
PRINT 22
PRINT 23,(I,PER001(I),GV1(I),I=1,NGV1)
PRINT 24
PRINT 23,(I,PER002(I),GV2(I),I=1,NGV2)
PRINT 25

C   INVERT SEISMGRAM
IVSEIS=IVSEIS+1
GC TO {26,27,28},IVSEIS
27  DC 29 I=1,NSEIS1
SEIS1(I)=-SEIS1(I)
29  CCONTINUE
GC TO 26
28  DC 30 I=1,NSEIS2
SEIS2(I)=-SEIS2(I)
30  CCONTINUE

```

```

26 IMTRX=IMTRX+1
C
C INCREASE NO. OF PCINTS TO A POWER OF 2 .CT. NSEIS1 OR NSEIS2
IF(NSEIS1.GT.1024.OR.NSEIS2.GT.1024)CALL EXIT
N=128
N2=7
31 IF(NSEIS1.LE.N.AND.NSEIS2.LE.N)GC TO 32
N=2*N
N2=N2+1
GC TO 31
C
32 DCDELA=DELA
NGBZ=NGV1/2
NBY=N/2
DCMEGA=PI/(DELA*FLOAT(NBY))
C
NVEL=(VELHI-VELLOW)/DV+1.0
VSTEP(1)=VELHI
TSTEP(1)=D21/VSTEP(1)
DC 35 I=2,NVEL
VSTEP(I)=VSTEP(I-1)-DV
TSTEP(I)=D21/VSTEP(I)
35 CCNTINUE
C
C REMOVE MEAN JR LINEAR TREND FROM SEISMOGRAMS
IP1=IMTRX-1
CALL BASE(SEIS1(NCZERO1),NSEIS1-NOZERO1+1,TYPE,IP1)
CALL BASE(SEIS2(NUZERO),NSEIS2-NCZERO+1,TYPE,IP1)
C
C COS TAPER BOTH ENDS OF SEISMOGRAM
IF(NCOSTP.EQ.0) GO TO 36
CALL CSTOP(SEIS1(NOZERO1),NSEIS1-NOZERO1+1,NCOSTP,1)
CALL CSTOP(SEIS2(NUZERO),NSEIS2-NCZERO+1,NCOSTP,1)
C
IF(NG1.EQ.0) GC TO 42
C
GRAPH OUT GROUP VELOCITY VALUES
36 CALL CRFGPV(NGV1,PERCD1,GV1)
CALL CRFGPV(NGV2,PERCD2,GV2)
C
C GRAPH CUT SEISMOGRAMS
DC 37 I=1,1024
Y(I,1)=SEIS1(I)
Y(I,2)=SEIS2(I)
Y(I,3)=0.0
Y(I,4)=0.0
Y(I,5)=0.0
37 CCNTINUE
CALL CHAN(N,2,3,1)
42 DC 201 I=1,5
201 TITLE(I)=TT2(I)
C
GC TO (100,38),IMTRX
38 PRINT 39,NP,NMIN,KMAX,TMIN,TMAX
PRINT 40,(TT(I),I=1,NP)
PRINT 41,(VSTEP(I),TSTEP(I),I=1,NVEL)
C
C
100 NC=0
KPER=1
101 CALL PACKET(N,DELA,NSEIS1,SEIS1,CRIGTM,DELTA1,GMT1,NGV1,PERCD1,
    IGV1,KPER,SA)
    CALL PACKET(N,DELA,NSEIS2,SEIS2,CRIGTM,DELTA2,GMT2,NGV2,PERCD2,
    IGV2,KPER,SB)
    DC 102 I=1,N
    Y(I,1)=SA(I)
    Y(I,2)=SB(I)
102 CCNTINUE
    CALL CRUNCH
    DC 103 I=1,N
    Y(I,3)=SA(I)
    Y(I,4)=SB(I)
103 CCNTINUE
    CALL COUTPUT
    IF (NG2.EQ.0) GO TO 104
    IF(KPER.EQ.1.OR.KPER.EQ.NGBZ.OR.KPER.EQ.NGV1)CALL CHAN(N,5,3,1)
104 KPER=KPER+1
    NC=NC+1
    IF(KPER.LE.NGV1)GO TO 101
    CALL EXHBIT
    CALL TIMER
    GC TO 1
C
C
11 FCRMAT(1H1//10X,62HSURFACE WAVE ANALYSIS(PHASE VELOCITY (KMS/SEC)
1/ PERIOD (SECS),49X,A8)
12 FCRMAT(10X,62H-----)
1-----,49X,BH-----)
13 FCRMAT(20X,10AB//)
14 FORMAT(//10X,20HORIGIN TIME OF EVENT,2X,I2,1X,5HHOURS,2X,I2,1X,
    14HMIN,2X,F4.1,1X,4HSECS,5X,2HOR,5X,F12.4,1X,4HSECS)

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15  FCRMAT(///10X,'STATION NAME OF SEISMOGRAM 1 IS',2X,8A1//
110X,45HDISTANCE OF RECORDING STATION FROM EPICENTRE ,F12.5,2X,
13HKMS//
110X,25HGMT TIME OF FIRST SAMPLE ,I2,2X,5HOURS,2X,I2,2X,4HMIN,2X,
1F4.1,2X,4HSECS,5X,2HGR,5X,F12.4,1X,4HSECS)
16  FCRMAT(///10X,'NSEIS1 =',I6,5X,'NSEIS2 =',I6,5X,'NGV1 =',I4,5X,'N
1GV2 =',I4,5X,'NCNSTP =',I5,5X,'DELA =',F6.2,///10X,'VELHI =',F6.2
2,5X,'VELLOW =',F6.2,5X,'DV =',F6.2)
17  FCRMAT(//10X,'BAND =',F6.2,5X,'DWF =',F6.2,5X,'NG1 =',I4,5X
1,'NG2 =',I4,5X,'NG3 =',I4)
18  FCRMAT(//10X,A8,11X,'NOZERO =',I6,5X,'IMTRX =',I4,5X,'IVSEIS =',I4
1)
19  FCRMAT(1H1//10X,12HSEISMCGRAM 1,3X,'ORIGINAL DATA')
20  FCRMAT(6(13,E15.7))
21  FCRMAT(1H1//10X,'SEISMOGRAM 2',3X,'ORIGINAL DATA')
22  FCRMAT(1H1//20X,53HPERIOD(SECS)/GRCUP VELOCITY(KMS/SEC) FOR SEISMO
1GRAM 1//)
23  FCRMAT(3(15,E15.7))
24  FCRMAT(1H1//20X,53HPERIOD(SECS)/GRCUP VELOCITY(KMS/SEC) FOR SEISMO
1GRAM 2//)
25  FCRMAT(1H1)
39  FCRMAT(1H1//2X,3HNP=,I5,1X,5HMIN=,I5,1X,5HMAX=,I5,1X,5HTMIN=,
1G12.5,1X,5HTMAX=,G12.5)
40  FCRMAT(//,1X,'TT(I),I=1,NP',/(1X,10G12.5))
41  FCRMAT(//,1X,'VSTEP(I),TSTEP(I),I=1,NVEL',/(1X,5(2G12.5)))
C
C
999 CALL FINISH
STOP
END
C
C
* * * * * * * * * * * * * * * * * * * * * * * * * * * * *
C
C
SUBROUTINE PACKET(N,DELA,NSEIS,SEIS,ORIGTM,DELTA,GMT,NGV,PERIOD,
1GV,KPEROD,WAVPKT)
C
C
DIMENSION SEIS(1),PERIOD(1),GV(1),WAVPKT(1)
C
GROUP ARRIVAL TIME FOR PERIOD OF INTEREST (TMARR)
TMARR=DELTA/GV(KPEROD)+ORIGTM
C
LENGTH (WINDOW) AND NO. OF SAMPLES (NWIN) OF CCSINE TAPER WINDOW
NWINDW=4.5*PERIOD(KPEROD)

```

```

NWIN=NWINDW/DELA
NWBY2=NWIN/2
NWIN=2*NWBY2
C
TIME (TARG) AND NO. OF POINTS (NSACW) FROM START OF SEISMOGRAM
TC 'TMARR'
TARG=TMARR-GMT
NSACW=TARG/DELA
C
NO. OF POINTS FROM START OF SEISMOGRAM TO START (INSTARW) AND END
(NFINW) OF WINDOW
NSTARW=NSACW-NWBY2
NFINW=NSACW+NWBY2
NFRONT=NWBY2
C
CHECK THAT WINDOW IS INSIDE DATA SET
IF(INSTARW.GT.1)GJ TC 2
NWIN=NWIN+NSTARW
NFRONT=NWIN-NWBY2
NSTARW=1
PRINT 1,NSACW,NWBY2,PERIOD(KPEROD)
1  FCRMAT(///10X,'FOR THIS PERIOD THE PROGRAM IS USING AN ASYMMETRICAL
1L CCSINE TAPERED WINDOW//10X,
1*BECAUSE A SYMMETRICAL WINDOW WOULD EXTEND BEYOND THE EDGE OF THE
1SEISMOGRAM//10X,
1*THE USER CAN OVERCOME THIS ASYMMETRY BY LENGTHENING THE SEISMOGRAM
1M//10X,
1*IF NO MORE ACTUAL DATA IS AVAILABLE THEN ZEROS CAN BE ADDED TO THE
1E FRONT. (SEE MAIN PROGRAM LISTING) //10X,
1*NSACW=,I7,10X,NWBY2=,I7,10X,'PERIOD=',F12.5)
C
LOAD AND CCSINE TAPER THE WINDOWED SEISMOCGRAM
2  DC 3 I=1,N
WAVPKT(I)=0.0
3  CCNTINUE
DC 4 I=NSTARW,NFINW
WAVPKT(I)=SEIS(I)
CCNTINUE
CALL CSTP(WAVPKT(INSTARW),NWIN+1,NFRONT,1)
C
RETURN
END
C
* * * * * * * * * * * * * * * * * * * * * * * * * * * * *
C

```

```

C      SUBROUTINE CRUNCH
C
C      CCMON/PHASE1/NSEIS1,SEIS1(2048),NSEIS2,SEIS2(2048),N,DELA,IMTRX,
C      IPI,N2,NBY,OMEGA,ALPHA,BETA
C      CCMON/PHASE2/NGV1,PEROD1(120),GV1(120),NGV2,PEROC2(120),GV2(120)
C      CCMON/PHASE3/Z(8192),SA(2048),SB(2048)
C      CCMON/PHASE4/X(120,120),VSTEP(120),NR,NX,KPER,NC,PERIOD(120)
C
C      COMPLEX Z
C
C      WINDOWED SEISMICGRAMS (SA(I),SB(I)) ARE PUT INTO A COMPLEX ARRAY Z
C      AND FOURIER ANALYSED
C      DC 1 I=1,N
C      Z(I)=CMPLX(SA(I),SB(I))
1     CCNTINUE
C      CALL CGOL(N2,Z,1.0)
C      Z(1)=CMPLX(0.0,0.0)
C      Z(NBY+1)=Z(1)
C
C      CHOOSE THE CENTRE FREQUENCY OF THE FILTER (CMEGAC) FROM THE
C      HARMONICS IN THE TIME SERIES (DCMEGA*L) SO THAT IT IS NEAREST TO
C      THE PERIOD OF INTEREST (PERCD1(I))
C      OMEGAC=2.0*PI/PEROD1(KPER)
C      L=CMEGAC/DCMEGA+0.5
C      L=L-1
C      CMEGAC=DCMEGA*FLOAT(L)
C      PERIOD(KPER)=2.0*PI/CMEGAC
C      CMEGA=0.0
C
C      BAND PASS FILTER THE WINDOWED SEISMICGRAMS
C      GAUSSIAN FILTER FUNCTION P IS MULTIPLIED BY BOTH +VE AND -VE
C      FREQUENCIES, J,K AND NJ,NK.
C      DC 2 I=1,NBY
C      J=L-I
C      K=L+I
C      IF(J.LT.2.AND.K.GT.NBY) GO TC 5
C      NJ=N-J+2
C      NK=N-K+2
C      OMEGA=DCMEGA-DCMEGA
C      P=0.0
C      PCNENT = (-ALPHA*(OMEGA/CMEGAC)**2)
C      IF (ABS(PCNENT).GT. 100.00) GO TC 3
C      P=EXP(PONENT)
C
C
C
3     IF(J.LT.2) GO TC 4
C      Z(J)=Z(J)*P
C      Z(NJ)=Z(NJ)*P
4     IF(K.GT.NBY) GO TO 2
C      Z(K)=Z(K)*P
C      Z(NK)=Z(NK)*P
2     CCNTINUE
C
C      TRANSFORM FILTERED SEISMICRAMS BACK INTO TIME DOMAIN
5     CALL CGOL(N2,Z,-1.0)
C      DC 6 I=1,N
C      SA(I)=REAL(Z(I))
C      SB(I)=AIMAG(Z(I))
6     CCNTINUE
C
C      PRINT 7, NC,L,CMEGAC,J,PERIOD(KPER)
7     FCRMAT(/,2X,3HNC=,I5,1X,2HL=,I5,1X,7HCMEGAC=,F10.5,1X,2HJ=,I5,5X,
1F16.5)
C
C      GO TO (8,9),IMTRX
9     IF(KPER.GT.5) GO TO 8
C      PRINT 10,NC,N,KPER,L,N2
10    FCRMAT(/,2X,"NC =",I5,2X,"N =",I5,2X,"KPER =",I5,2X,"L =",I5,2X,"N
12   =",I5)
C      PRINT 11,(SA(I),I=1,N)
11    FCRMAT(/,1X,"SA(I),I=1,N",/(1X,10G12.5))
C      PRINT 12,(SB(I),I=1,N)
12    FCRMAT(/,1X,"SB(I),I=1,N",/(1X,10G12.5))
C
8     RETURN
ENC
C
C      * * * * * * * * * * * * * * * * * * * * *
C
C      SUBROUTINE OUTPLT
C
C      CCMON/PHASE1/NSEIS1,SEIS1(2048),NSEIS2,SEIS2(2048),N,DELA,IMTRX,
C      IPI,N2,NBY,OMEGA,ALPHA,BETA
C      CCMON/PHASE3/Z(16384),SA(2048),SB(2048)
C      CCMON/PHASE4/X(120,120),VSTEP(120),NR,NX,KPER,NC,PERIOD(120)
C      CCMON/PHASE5/VELHI,VELLOW,NVEL,NP,NMAX,NMIN,TT(2048),TSTEP(120),N
1G3
C      CCMON /CLT/ Y(2048,5)

```

```

C
C      DIMENSION E(2048),SAMSBS(2048)
C
C      SET UP CONSTANTS
C      NEND=N
C      NSTA=NMIN
C      NSTB=0
C      ISW=1
C      IF(NSTA.LT.2) ISW=2
C      K=1
C
C
C      CROSS-MULTIPLY TRACES FOR VARIOUS TIME SHIFTS
1      XMAX=0.0
C      IC=NSTA
C      DC 2 I=NSTA,NEND
C      IN=I-NSTA+NSTB+1
C      SAMSBS(I)=SA(I)*SB(IN)
C      IF (XMAX-SAMSBS(I))3,2,2
3      IC=I
C      XMAX=SAMSBS(I)
2      CONTINUE
C
C      SAMSBS(I) GRAPHED IF NSTA = 1
C      IF(NSTA.NE.1)GO TO 4
C      DC 5 I=NSTA,NEND
C      Y(I,5)=SAMSBS(I)
5      CONTINUE
C
4      NEND1=NEND-1
C      E(K)=C.C
C      IF(NEND1.LT.IC)GO TO 6
C      FIND MIN VALUE OF X-MULT TRACE AFTER THE MAX AT 'IC' AND CALCULATE
C      THE D.C. LEVEL
C      DC 7 I=IC,NEND1
C      IF (SAMSBS(I+1).GT.SAMSBS(I))GO TO 8
7      CONTINUE
8      E(K)=(SAMSBS(IC)+SAMSBS(I))*0.5
6      K=K+1
C      CHECK RANGE OF PHASE VEL. VALUES COMPLETED
C      IF (K.GT.NP)GO TO 9
C
C      IF RANGE NOT COMPLETED REVERSE TRACES IN X-MULT PROCESS
C      GO TO (10,11),ISW
10     IF (NSTA.EQ.2)ISW=2

```

```

NSTA=NSTA-1
GC TO 1
11    NEND=NEND-1
NSTB=NSTB+1
IF (NEND.NSTB+1.GT.N.CR.NSTB+1.GT.NMAX)GO TO 9
GC TO 1
C
C      INTERPOLATE TO FIND D.C. LEVEL AT VEL. STEPS OF INTEREST
9      KLIM=K-1
DC 12 I=1,NVEL
X(KPER,I)=J.
INC=1
CALL INTPL (NP,3,TT,E,TSTEP(I),X(KPER,I),IND)
12    CONTINUE
C
GC TO (13,14),IMTRX
14    IF (KPER.GT.2) GO TO 13
PRINT 15,NEND,NSTA,NSTB,ISW,K,KLIM,KPER
15    FCRMAT(1H//2X,*NEND =",I5,2X,*NSTA =",I5,2X,*NSTB =",I5,2X,*ISW =
1*,I5,2X,*K =",I5,2X,*KLIM =",I5,2X,*KPER =",I5)
PRINT 16,(TT(I),E(I),I=1,KLIM)
16    FCRMAT(//,1X,TT(I),E(I),I=1,KLIM*,/(1X,10G12.5))
PRINT 17,(TSTEP(I),X(KPER,I),I=1,NVEL)
17    FCRMAT(//,1X,*TSTEP(I),X(KPER,I),I=1,NVEL*,/(1X,10G12.5))
C
13    RETURN
END
C
* * * * * * * * * * * * * * * * * * * * * * *
C
C      SUBROUTINE EXHIBIT
C
C
COMMON/PHASE4/X(120,120),VSTEP(120),NR,NX,KPER,NC,PERICD(120)
COMMON/PHASE5/VELHI,VELLOW,NVEL,NP,NMAX,NMIN,TT(2048),TSTEP(120),N
1G3
C
C      NR=NVEL
C      NC=KPER-1
C
C      FIND MAXIMUM OF MATRIX
C
XMAX=0.0

```

```

DC 1 J=1,NR
CALL AMAX(X(1,J),NC,HOLD)
IF(HOLD.GT.XMAX)XMAX=HOLD
1 CCNTINUE
C
DC 2 I=1,NR
DC 3 J=1,NC
X(J,I)=X(J,I)/XMAX*99.0
3 CCNTINUE
2 CCNTINUE
C
N25=(NC-1)/25+1
DC 4 IZ=1,N25
NLCW=(IZ-1)*25+1
NHY=NLCW+24
IF(NHY.GT.NC)NHY=NC
PRINT 5
5 FCRMAT(1H1//50X,14HMATRIX OF X(I)//)
PRINT 6,(PERIOC(I),I=NLOW,NHY,2)
6 FCRMAT(3X,13F10.2)
DC 7 I=1,NR
PRINT 8 ,VSTEP(I),(X(J,I),J=NLCW,NHY)
8 FORMAT(1X,F4.2,3X,25F5.2)
7 CCNTINUE
4 CCNTINUE
C
IF (NG3.EQ.0) GO TO 9
CALL CCNTUR(X,NC,NR,120,5.0,5.0,100.0,3)
C
9 RETURN
END
C
* * * * * * * * * * * * * * * * * * * * *
C
C
SUBROUTINE BASE(X,N,TYPE,IP1)
ENTRY CBASE(DX,N,TYPE,IP1)
ENTRY CBASE(X,N,TYPE,IP1)
ENTRY DCHASE(DX,N,TYPE,IP1)
C
C
REMOTES EITHER THE LEAST SQUARES OR MEAN BAELINE OR THE FIRST POINT
C
C
SUBROUTINE BASE(X,N,TYPE,IP1)
DIMENSION X(N),DX(N)

```

```

      DOUBLE PRECISION CX,SUMX,SUMIX,FX,PHI,XINT0,XBAR,AN,X1,X2,
      SUMX2,SUMX3,VARX,A3MNT,SKEW
      REAL*8 TYPE,MEAN,LEAST
      DATA MEAN/BHMEAN      /,LEAST/BHLEAST    /
C
      IPC=1
      IF(N.LE.0)GO TO 210
      N2=N
      N3=1
      FX=DBLE(X(1))
      GC TO 100
C
      ENTRY DBASE(DX,N,TYPE,IP1)
      IPC=2
      IF(N.LE.0)GO TO 210
      N2=N
      N3=1
      FX=DX(1)
      GC TO 100
C
      ENTRY CBASE(X,N,TYPE,IP1)
      IPC=1
      IF(N.LE.0)GO TO 210
      N2=N*2-1
      N3=2
      FX=CBLE(X(1))
      GC TO 100
C
      ENTRY DCEASE(DX,N,TYPE,IP1)
      IPC=2
      IF(N.LE.0)GO TO 210
      N2=N*2-1
      N3=2
      FX=DX(1)
C
C
100  INDE=1
      IF(TYPE.EQ.MEAN)INDE=2
      IF(TYPE.EQ.LEAST)INDE=3
C
      AN = DFLCAT(N)
      SUMX = 0.0D0
      SUMIX = 0.0D0
      DC 104 I=1,N2,N3
      GC TO (101,102),IPC

```

```

101 X1 = DBLE(X(I))
102 GC TO 103
103 X1 = DX(I)
104 SUMX = SUMX + X1
SUMIX = SUMIX + DFLCAT(I)*X1
CONTINUE
XEAR = SUMX/AN
XINT0 = (((4.00*AN)+2.00)*SUMX-6.00*SUMIX)/(AN*(AN-1.00))
PHI = ((12.00*SUMIX)-6.00*(AN+1.00)*SUMX)/(AN*(AN+1.00)*(AN-1.00))
C
GC TO (110,120,130),INDE
110 DC 113 I=1,N2,N3
GC TO (111,112),IPC
111 X(I) = DBLE(X(I)) - FX
GC TO 113
112 DX(I) = DX(I) - FX
113 CONTINUE
PRINT 1
1 FCRMAT(//4X,42F0 DATA HAS BEEN CORRECTED BY THE FIRST POINT)
GC TO 200
120 DC 123 I=1,N2,N3
GC TO (121,122),IPC
121 X(I) = DBLE(X(I)) - XBAR
GC TO 123
122 DX(I) = DX(I) - XBAR
123 CONTINUE
PRINT 2
2 FCRMAT(//4X,44F0 DATA HAS BEEN CORRECTED TO THE MEAN BASELINE)
GC TO 200
130 DC 132 I=1,N2,N3
GC TO (131,132),IPC
131 X(I) = DBLE(X(I)) - DFLDAT(I)*PHI - XINTC
GC TO 133
132 UX(I) = CX(I) - DFLCAT(I)*PHI - XINTO
133 CONTINUE
PRINT 3
3 FCRMAT(//4X,53F0 DATA HAS BEEN CORRECTED TO THE LEAST SQUARES BASELINE)
C
200 SUMX2 = 0.00
SUMX3 = 0.00
DC 204 I=1,N
GC TO (201,202),IPC
201 X1 = DBLE(X(I))
GC TO 203

```

```

202 X1 = CX(I)
203 X2 = X1*X1
SUMX2 = SUMX2 + X2
SUMX3 = SUMX3 + X2*X1
204 CONTINUE
VARX = SUMX2/AN
A3MNT = SUMX3/AN
SKEW = (A3MNT*A3MNT)/(VARX**3)
PRINT 4, XBAR, FX, PHI, VARX, SKEW
4 FCRMAT(4X,14HMEAN OF DATA =,G12.5,8X,22FVALUE OF FIRST POINT =,
1G12.5/4X,32FGRADIENT OF LEAST SQUARES LINE =,G12.5,8X,18HVARIANCE
2OF DATA =,G12.5,8X,10HSKEWNESS =,G12.5)
C
IF(IP1.EQ.1)PRINT 5, (I, X(I), I=1,N2,N3)
5 FCRMAT(//4X,24HTHE BASELINED DATA IS --//5(4X,6HSAMPLE,4X,4HX(I),
13X)/(15(4X,15,G12.5)))
C
210 RETURN
END
C
* * * * * * * * * * * * * * * * * * * * * * * * *
C
C

```

```

C SUBROUTINE CSTP(X,N,NC,INDE)
C ENTRY CCSTP(DX,N,NO,INDE)
C ENTRY CCSTP(X,N,NC,INDE)
C ENTRY DCCSTP(DX,N,NC,INDE)
C
-----
```

```

C INDE=1-----COSINE TAPER BOTH ENDS OF CURVE.
C INDE=2-----COSINE TAPER FRONT END OF CURVE.
C INDE=3-----COSINE TAPER BACK END OF CURVE.
C
-----
```

```

C -----IS THE ARRAY.
C

```

```

C -----IS THE NUMBER OF POINTS IN THE ARRAY.
C

```

```

C -----IS THE STARTING NUMBER.
C
-----
```

```

SUBROUTINE CSTP(X,N,NC,INDE)
DIMENSION X(N),DX(N)
DOUBLE PRECISION DX,PI,PHI,Cphi,SPHI,CTHET1,STHET1,CTHET2,STHET2
C
IPC=1
IC=1
GC TO 1
C
ENTRY CCSTP(DX,N,NC,INDE)
IPC=2
IC=1
GC TO 1
C
ENTRY CCCSTP(X,N,NC,INDE)
IPC=1
IC=2
GC TO 1
C
ENTRY CCCSTP(DX,N,NC,INDE)
IPC=2
IC=2
C
C
1   PI = 4.00*DATAN(1.00)
Phi = PI/DFLOAT(NO-1)
Cphi = DCOS(PHI)
SPhi = DSIN(PHI)
CTHET1 = 1.00
STHET1 = 0.00
CTHET2 = 1.00
STHET2 = 0.00
IF(NO.LE.0)RETURN
C
GC TO (10,20),IPC
C
10  DC 17 I = 1,NO
GC TO (11,12,13),INDE
11  IA = (N-I)*IC+1
12  IN = (I-1)*IC+1
GC TO 14
14  IN = (N-I)*IC+1
15  X(IN) = 5.0-1*CBL(E(X(IN)))*(1.00-CTHET2)
GC TO (15,16,16),INDE
16  X(IA) = 5.0-1*CBL(E(X(IA)))*(1.00-CTHET2)
CALL SINCOS(Cphi,SPhi,CTHET1,STHET1,CTHET2,STHET2)

C
C
17  CCNTINUE
GC TO 30
C
20  DC 27 I = 1,NO
GC TO (21,22,23),INDE
21  IA = (N-I)*IC+1
22  IN = (I-1)*IC+1
GC TO 24
24  IN = (N-I)*IC+1
25  DX(IN) = 5.0-1*DX(IN)*(1.00-CTHET2)
GC TO (25,26,26),INDE
26  DX(IA) = 5.0-1*DX(IA)*(1.00-CTHET2)
CALL SINCOS(Cphi,SPhi,CTHET1,STHET1,CTHET2,STHET2)
27  CCNTINUE
C
30  RETURN
ENC
C
* * * * * * * * * * * * * * * * * * * * * * * * *
C
C
SUBROUTINE SINCOS(Cphi,SPhi,CTHET1,STHET1,CTHET2,STHET2)
C
DOUBLE PRECISION Cphi,SPhi,CTHET1,STHET1,CTHET2,STHET2
C
CTHET2 = CTHET1*Cphi - STHET1*SPhi
STHET2 = STHET1*Cphi + CTHET1*SPhi
CTHET1 = CTHET2
STHET1 = STHET2
RETURN
ENC
C
* * * * * * * * * * * * * * * * * * * * * * * *
C
C
GIP SLBROUTINE INTPCL
--- -----
C
C
BESSELS INTERPLATION FORMULA TO THE FIFTH DIFFERENCE
REFERENCE - I.A.T. P.56
C
C
FROM THE CALL INTPCL(N,L,X,Y,XP,YP,IND)

```

```

C      N  NUMBER OF FCINTS
C      L  STARTING POSITION IN TABLE OF VALUES (NOT LESS THAN 3)
C      X  INDEPENDENT VARIABLE WHICH MUST BE EQUALLY SPACED
C      Y  VALUES OF THE FUNCTION
C      XP  INTERMEDIATE VALUE OF REQUIRED YP
C      YP  VALUE OF FUNCTION OF REQUIRED XP
C      INC = 1  NORMAL INTERPOLATION YP FROM XP
C      INC = 2  INVERSE INTERPOLATION XP FROM YP
C      INC = 3  NO INTERPOLATION VALUE OUTSIDE TABLE
C
C      FORMS THE FOLLOWING DIFFERENCE TABLE --
C
C      X      Y      D1      D2      D3      D4      D5
C      -      -      --      --      --      --      --
C
C      X(K-2)  Y(K-2)      D11
C      Y(K-1)  Y(K-1)      D12      D21      D31
C      X(K)    Y(K)        D22      D32      D41      D51
C      XP     YP          D13      D23      D32      D42
C      X(K+1)  Y(K+1)      D14      D24      D33
C      X(K+2)  Y(K+2)      D15
C      X(K+3)  Y(K+2)
C
C      SUBROUTINE INTPOL(N,L,X,Y,XP,YP,INC)
C      DIMENSION X(N),Y(N)
C
C      DOUBLE PRECISION P,B2,B3,B4,B5,C11,C12,C13,C14,C15,
C      1   C21,C22,C23,C24,C31,C32,C33,C41,C42,C51
C
C      NL=N-L
C      GO TO (10,20),INC
C
C      SET K FOR INTERPOLATION
10    K=L
      IF(X(L)-XP)11,11,14
11    DC 13 I=L,NL
      IF(X(I)-XP)12,15,100
12    K=I
C
C      CONTINUE
13    XP OUTSIDE TABLE
14    INC=3
      GO TO 300
C      XP IS A TABULAR VALUE
15    YP=Y(I)
      GO TO 300
C
C      SET K FOR INVERSE INTERPOLATION
20    DC 23 K=L,NL
      P=(YP-Y(K))/(Y(K+1)-Y(K))
      IF(P)23,25,22
22    IF(P-1.0)100,23,23
23    CONTINUE
C      YP OUTSIDE TABLE
24    INC=3
      GO TO 300
C      YP IS A FUNCTION VALUE
25    XP=X(K)
      GO TO 300
C
C      FORM DIFFERENCES
100   D11=Y(K-1)-Y(K-2)
      D12=Y(K)-Y(K-1)
      D13=Y(K+1)-Y(K)
      D14=Y(K+2)-Y(K+1)
      D15=Y(K+3)-Y(K+2)
      D21=D12-D11
      D22=C13-C12
      D23=C14-C13
      D24=C15-C14
      D31=D22-C21
      D32=C23-C22
      D33=C24-C23
      D41=D32-C31
      D42=C33-C32
      D51=D42-D41
      GO TO (210,220),INC
C
C      INTERPOLATION SECTION
C      FORM BESSEL COEFFICIENTS
210   P=(XP-X(K))/(X(K+1)-X(K))
      B2=P*(P-1.0D0)
      B3=B2*(P-0.5D0)
      B4=B2*(P+1.0D0)*(P-2.0D0)

```

```

B5=B4*(P-0.500)
B2=B2/4.000
B3=B3/6.000
B4=B4/48.000
B5=B5/120.000
C
C      THE FORMULA
C      YP=Y(K)+P*D13+B2*(D22+D23)+B3*D32+B4*(D41+D42)+B5*D51
C      GO TO 300
C
C      INVERSE INTERPOLATION SECTION
220  DC 230 I=1,20
      FORM BESSEL COEFFICIENTS
      B2=P*(P-1.000)
      B3=B2*(P-0.500)
      B4=B2*(P+1.000)*(P-2.000)
      B5=B4*(P-0.500)
      B2=B2/4.000
      B3=B3/6.000
      B4=B4/48.000
      B5=B5/120.000
C      THE INVERSE FORMULA
      P=(YP-Y(K)-B2*(D22+D23)-B3*D32-B4*(D41+D42)-B5*D51)/D13
230  CCNTINUE
      XP=X(K)+P*(X(K+1)-X(K))
C
300  RETURN
END
SUBROUTINE FILLUP(NCPTS,Z)
C
C      DIMENSION Z(1)
CCMPLX Z,CZERO
CZERO=CMPLX(0.0,0.0)
AN=NCPTS-2
N=ALOG10(AN)/ALOG10(2.0)+1.0
N1=(2*N)+1
N2=2*(N+1)
NIM1=N1-1
DC 1 I=2,NIM1
NN=N2-I+2
Z(NN)=CCNJG(Z(I))
CCNTINUE
Z(N1)=CZERO
RETURN
1
ENC
C      * * * * * * * * * * * * * * * * * * * * * * * * * * * * *
C
C      NEW CARGRF
C
C      FROM THE CALL CARGRF(X,Y,N) THIS PACKAGE FLITS N POINTS
C      THE CARTESIAN CO-ORDINATES OF THE ITH POINT BEING SPECIFIED AS
C      X(I),Y(I)
C
C      THE OPTIONS ARE SET BY USING THE COMMON -
C
C      COMMON /GRFF/ TITLE(20), XMAX, XMIN, YMAX, YMIN, INDX, INDY, INC,
C      IIDOT, ANSTR1, IF, XLIMIT, YLIMIT, SCALX, SCALY
C
C      THE TITLE ARRAY CARRIES INFORMATION FOR ANNOTATING THE OUTPUT
C      GRAPH. THIS ARRAY MUST BE SET UP AS FOLLOWS -
C
C      TITLE(1) -)
C      . )CONTAINS 24 HOLLERITH CHARACTERS GIVING THE UNITS
C      TITLE(3) -)OF THE ABSCISSAE
C
C      TITLE(4) )CONTAINS 16 HOLLERITH CHARACTERS GIVING THE UNITS
C      TITLE(5) )OF THE ORDINATE
C
C      TITLE(6) -)
C      . )CONTAINS 80 HOLLERITH CHARACTERS GIVING A TITLE TO
C      . )THE GRAPH
C      TITLE(15) -)
C
C      TITLE(16) -CONTAINS 8 HOLLERITH CHARACTERS GIVING DATE OF
C      PROCESSING
C      TITLE(17) -CONTAINS 8 HOLLERITH CHARACTERS GIVING TIME OF
C      PROCESSING
C      TITLE(18) -)
C      . )UNUSED
C      TITLE(20) -)
C
C      XMAX )SET BOTH EQUAL IF PROGRAM TO CHOOSE THE ABSCISSAE
C      XMIN )SCALE. OTHERWISE SET TO CHOSEN LIMITS OF ABSCISSAE SCALE
C
C      YMAX )SET BOTH EQUAL IF PROGRAM TO CHOOSE THE ORDINATE SCALE
C      YMIN )OTHERWISE SET TO CHOSEN VALUES OF ORDINATE SCALE

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```

C      INDEX IS AN INDICATOR FOR PLOTTING THE ABSISSAE ON A LOG SCALE
C      INDEX=1 ABSISSAE ON LINEAR SCALE
C      INDEX=2 ABSISSAE ON LOG SCALE
C
C      INDY IS A SIMILAR INDICATOR FOR THE ORDINATE SCALE
C
C      N.B. CONTENTS OF ARRAYS ARE MODIFIED USING LOG SCALE
C
C      INO IS AN INDICATOR FOR CONTROLLING FRAME CALLS -
C      INO=1 CARGRF CALLS ADVFLM AND PLOTS ON A NEW FRAME
C      =2 CARGRF PLOTS ON THE CURRENT FRAME
C
C      IDOT IS THE SC4020 CODE OF THE REQUIRED PLOTTING SYMBOL
C
C      ANSTRI INDICATES WHETHER THE PLOTTED POINTS HAVE TO BE JOINED UP
C      ANSTRI=1. POINTS NOT JOINED
C      =2. POINTS JOINED
C
C      IF SPECIFIES TYPE OF OUTPUT
C      IF=1 OUTPLT ON MICROFILM
C
C      REWRITTEN BY J.B.YOUNG FOR THE IBM 370/168 ON 01/07/74
C
C
C      SUBROUTINE GRAFIX,X,Y,N)
C      ENTRY CARGRF(X,Y,N)
C
C      DIMENSION X(N), Y(N)
C
C      COMMON /GRFF/ TITLE(20), XMAX, XMIN, YMAX, YMIN, INDEX, INDY, INC,
C      IECCT, ANSTRI, IF, XLIMIT, YLIMIT, SCALX, SCALY, XFACTR, YFACTR
C
C      REAL*8 TITLE,CATE
C
C      REAL*4 INSTR1,JCIN/4HJOIN/,BLANK/4H      /
C
C      INTEGER*4 PLACEX,PLACEY,XPLCT1,XPLCT2,YPLCT1,YPLCT2,XPCS,YPOS
C
C
C      CALL DATIM(UATE,TITLE(17))
C      IF(IF#2,2,1
C      IF(IF-4)3,3,2
C      IF=2
C
C
C
C      IF(IND.NE.2)IND=1
C      IF(INDX.NE.2)INDX=1
C      IF(INDY.NE.2)INDY=1
C      IF(IDCT.GT.63)IDCT=48
C      INSTR1=JCIN
C      IF(ANSTRI.EQ.1.)INSTR1=BLANK
C
C      GC TO (30,10),INDEX
C      PCSXT=PMIN(X,N)*0.8
C      DC 20 I=1,N
C      IF(X(I).LT.POSXT)X(I)=POSXT
C      X(I)= ALOG10(X(I))
C      CCNTINUE
C      GC TO (60,40),INDY
C      PCSYT=PMIN(Y,N)*0.8
C      DC 50 I=1,N
C      IF(Y(I).LT.POSYT)Y(I)=POSYT
C      Y(I)= ALOG10(Y(I))
C      CCNTINUE
C      GC TO (100,200),IND
C
C
C      100 IF(XMAX-XMIN)110,120,110
C      110 XMX=XMAX
C      XMN=XMIN
C      GC TO 130
C      120 CALL AMAX(X,N,XMX)
C      CALL AMIN(X,N,XMN)
C      130 IF(YMAX-YMIN)140,150,140
C      140 YMX=YMAX
C      YMN=YMIN
C      GC TO 160
C      150 CALL AMAX(Y,N,YMX)
C      CALL AMIN(Y,N,YMN)
C      160 CALL ADVFLM(IF)
C
C
C      200 CALL SCALEN(X,XLIMIT,SCALX,PLACEX,XFACTR,N,XMX,XMN)
C      CALL SCALEN(Y,YLIMIT,SCALY,PLACEY,YFACTR,N,YMX,YMN)
C      XPLCT1=(X(I)-XLIMIT)*SCALX+123.
C      YPLCT1=923.-(Y(I)-YLIMIT)*SCALY
C      CALL PLOT(XPLCT1,IECT,YPLCT1)
C      DC 230 I=2,N
C      XPLCT2=(X(I)-XLIMIT)*SCALX+123.

```

```

YFLOT2=923.-{Y(I)-YLIMIT}*SCALY
CALL PLOT(XPLOT2,ICCT,YPLOT2)
IFI(INSTR1-JOIN)220,210,220
210 CALL VECTOR(XPLCT1,YPLOT1,XPLOT2,YFLOT2)
220 YPLOT1=YPLOT2
XPLOT1=XPLOT2
230 CCNTINUE
C
GC TO (300,400),IND
C
C
300 CALL VECTOR(115,923,1003,923)
CALL VECTOR(123,931,123,43)
DC 310 I=1,11
XFCS=203+(I-1)*80
YFOS=43+(I-1)*60
CALL VECTOR(XPCS,923,XPOS,931)
CALL VECTOR(115,YPOS,123,YPICS)
310 CCNTINUE
DC 370 I=1,3
XLIM=XLIMIT+FLCAT(I-1)*XFACTR*4.
GC TO (330,320),INDX
320 XFCS=92+(I-1)*320
CALL TSP(XFOS,48,942)
CALL C4020E(10.**XLIM,11,4)
GC TO 340
330 XPCS=20+PLACEX*8+(I-1)*320
CALL TSP(XPJS,48,942)
CALL C4020F(XLIM,13,PLACEX)
340 YFCS=915-(I-1)*320
YLIM=YLIMIT+FLCAT(I-1)*YFACTR*4.
GC TO (360,350),INDY
350 CALL TSP(28,48,YPICS)
CALL C4020E(10.**YLIM,11,4)
GC TO 370
360 CALL TSP(12,48,YPGS)
CALL C4020F(YLIM,13,PLACEY)
370 CCNTINUE
C
IF(TITLE(16).NE.DATE)GO TO 400
CALL TSP(760,48,958)
CALL HGRAM(TITLE(1),24)
CALL TSP(48,48,291)
CALL VERAM(TITLE(4),16)
CALL TSP(130,48,23)

C
CALL HGRAM(TITLE(6),80)
C
400 RETURN
ENC
C
* * * * * * * * * * * * * * * * * * * * *
C
C
SUBROUTINE SCALEN(X,XLIMIT,SCALX,IPLACE,FACTCR,N,XMAX,XMIN)
C
CCMPUTES SCALING VALUES FOR CARCRF
C
C
DIMENSION X(N)
DCLBLE PRECISION XRG,R,FACT,S
C
XRG=XMAX-XMIN
IF(XRG.LT..0000000001)XRG=1.000
C
R=C.000
1 IF(XRG.LT.(10.000**R*.0000000001)) GO TO 2
R=R+1.000
GC TO 1
2 FACT=(10.000**R-1.000)*.00000000125
S=C.000
3 IF(XRG.LE.FACT*(2.000**S)) GC TO 4
S=S+1.000
GC TO 3
4 FACTOR=(FACT*(2.000**S))*10.00-2
C
XLIMIT=FLOAT(IFIX(XMIN/FACTCR))*FACTOR
IF(XMIN.LT.XLIMIT)XLIMIT=XLIMIT-FACTOR
SCALX=80./FACTCR
IPLACE=13.-R
IF(IPLACE.LT.1)IPLACE=1
RETURN
ENC
C
* * * * * * * * * * * * * * * * * * * * *
C
C
FUNCTION PMIN (X,N)
C
FINDS MINIMUM POSITIVE VALUE OF ARRAY X

```

```

C
C      DIMENSION X(N)
C
C      DC 1 KQ=1,N
C      IF(X(KQ).LE.0.0)GO TO 1
C      GC TO 5
C      1 CCNTINUE
C      PMIN=1.25
C      GC TO 6
C      5 KP=KQ
C      2 IF(KQ-N)3,4,4
C      3 KQ=KQ+1
C          IF(X(KQ).LE.0.0)GO TO 2
C          IF(X(KP)=X(KQ))2,5,5
C      4 PMIN=X(KP)
C      6 RETURN
C      END
C
C      * * * * *
C
C      SUBROUTINE CHAN(N,NC,IF,IND)
C
C      THIS PACKAGE PLOTS UP TO 20 CHANNELS OF A DOUBLE SUBSCRIPTED
C      ARRAY, X(I,J) WHERE J DEFINES THE CHANNEL NUMBER AND I THE SAMPLE
C      NUMBER IN THE JTH CHANNEL. THE DATA IS ASSUMED TO BE SAMPLED AT
C      EQUAL INTERVALS.
C
C      FIVE CHANNELS ARE PLOTTED TO A FRAME, THE TIME AXIS IS PARALLEL
C      TO THE Y AXIS OF THE PLOTTER.
C
C      THE PACKAGE USES THE COMMONS -
C
C      COMMON /OUT/    X(2048,5)
C
C      COMMON /GRAPH/ TITLE(31), DELA
C
C      X IS THE ARRAY TO BE PLOTTED, TITLE IS AN ARRAY FOR ANNOTATING
C      THE OUTPUT AND DELA IS THE SAMPLING INTERVAL OF THE TIME SERIES.
C      THE TITLE ARRAY IS MADE UP AS FOLLOWS -
C
C      TITLE(1)  -)
C              *
C              -)
C
C      TITLE(J)  -)
C              .
C              -) EACH ELEMENT CARRIES AN 8 CHARACTER TITLE
C              .
C              -) DESCRIBING THE DATA IN THE CHANNEL
C              .
C              -)
C      TITLE(20) -)
C
C      TITLE(21) -)
C              .
C              -) CARRIES 80 HOLLERITH CHARACTERS GIVING A TITLE TO
C              .
C              -) THE OUTPUT
C      TITLE(30) -)
C
C      TITLE(31) - CARRIES 8 HOLLERITH CHARACTERS GIVING UNITS OF THE
C                  TIME SERIES
C
C      IF IS AN INDICATOR TO SPECIFY THE OUTPUT REQUIRED
C
C      IF IF =1 OUTPUT IS ON MICROFILM
C          IF =2 OUTPUT IS ON HARD COPY
C          IF =3 OUTPUT IS ON BOTH MICROFILM AND HARD COPY
C
C      IND IS AN INDICATOR IF SET TO 1 THE MAXIMUM AMPLITUDE IN
C      EACH CHANNEL IS SCALED TO THE FULL RANGE AVAILABLE, IF SET TO 2
C      THE MAXIMUM RANGE OF THE X ARRAY IS SCALED TO THE FULL RANGE
C      AVAILABLE.
C      SETTING IND TO 1 DESTROYS THE ORIGINAL DATA IN THE X ARRAY.
C      PLOTTING USING CHAN SHOULD THEREFORE BE DONE ONLY WHEN ALL
C      REQUIRED COMPUTATION HAS BEEN CARRIED OUT ON X - THIS RESTRICTION
C      DOES NOT APPLY IF IND IS 2.
C
C      SUBROUTINE CHAN(N,NC,IF,IND)
C
C      COMMON /OUT/    X(2048,5)
C
C      COMMON /GRAPH/ TITLE(31), DELA
C      REAL*8 TITLE
C
C      COMMON/PLCT/NT,NXL,RANGE,CONST,AINTER,
C      ITT(2048),XX,BMAX(5),BMIN(5)
C
C      GC TO (10,20),IND
C      10 XMAX=1.
C          XMIN=0.
C

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```

      SUBROUTINE SCHAN(XMAX,XMIN,N)
C
C      COMMON /GRAPH/ TITLE(31), DELA
C      REAL*8 TITLE
C
C      CLMMCN/POLT/NT,NXL,RANGE,CCNST,AINTER,
C      ITT(2048),XX,BMAX(5),BMIN(5)
C      REAL*8 SECS/BYSECCNDS /
C
C      XRG=XMAX-XMIN
C      XX=XMIN
C      RANGE=200./XRG
C      IF(DELA.EQ..04444.AND.TITLE(31).EQ.SECS)GO TO 3
C      S=6.
C      IF(N.LE.100)S=7.
C      R=C.
C      1 IF(DELA.LT.(10.*R*.CC00001))GO TO 2
C      R=R+1.
C      GO TO 1
C      2 IF(R.LT.1.)GO TO 99
C      INTER=10.**(8.-R)*DELA+0.5
C      AINTER=FLCAT(INTER)/(10.**(S-R))
C      ANXL=(8.*AIINTER)/DELA
C      GO TO 4
C
C      3 AINTER=5.
C      ANXL=1125.
C
C      4 NXL=ANXL
C      CCNST=1000./ANXL
C      NT=N/NXL+1
C
C 99  RETURN
C
C      * * * * * * * * * * * * * * * * * * * * *
C
C      SUBROUTINE PEN(X,IEND,JA,XMIN,RANGE,CONST)
C
C      DIMENSION X(IEND)
C

```

```

      INTEGER XPLOT1, XPLCT2, TPLCT1, TPLOT2
C
C      AJ=812. - FLOAT(JA-1)*200.
C      XPLOT1=AJ + (X(1) - XMIN)*RANGE
C      TPLOT1=19.
C
C      DO 15 I=2,IEND
C      XPLCT2=AJ + (X(I) - XMIN)*RANGE
C      TPLCT2=FLOAT(I-1)*CCNST + 19.
C      CALL VECTOR(XPLOT1,TPLCT1,XPLCT2,TPLOT2)
C      XPLCT1=XPLCT2
C      TPLCT1=TPLCT2
C 15  CONTINUE
C      RETURN
C
C      * * * * * * * * * * * * * * * * * * * * *
C
C      SUBROUTINE TCHAN(N,DELA)
C
C      CLMMCN/POLT/NT,NXL,RANGE,CCNST,AINTER,
C      ITT(2048),XX,BMAX(5),BMIN(5)
C
C      DO 1 I=1,N
C      TT(I)=0.
C 1  CONTINUE
C
C      LT=(FLOAT(N)*DELA)/AIINTER+1.
C      TT(2)=25.
C      AD=AIINTER/DELA
C
C      DO 2 I=1,LT
C      LL=FLCAT(I-1)*AD+1.
C      TT(LL)=25.
C 2  CONTINUE
C
C      RETURN
C
C      * * * * * * * * * * * * * * * * * * * * *

```

```

C      SLROUTINE AMAX (X,N,XMAX)
C      FINDS MAXIMUM VALUE OF ARRAY X
C
C      DIMENSION X(N)
C
C      KC = 1
2     KF = KC
5     IF(KQ-N)3,4,4
3     KC = KC + 1
     IF(X(KP) - X(KC))2,5,5
4     XMAX = X(KP)
     RETURN
     END
C
C      * * * * * * * * * * * * * * * * * * * * *
C
C      SLROUTINE AMIN (X,N,XMIN)
C      FINDS MINIMUM VALUE OF ARRAY X
C
C      DIMENSION X(N)
C
C      KC = 1
5     KF = KC
2     IF(KQ-N)3,4,4
3     KC = KC + 1
     IF(X(KP) - X(KC))2,5,5
4     XMIN = X(KP)
     RETURN
     END
C
C      * * * * * * * * * * * * * * * * * * * * *
C
C      SLROUTINE CLNTUR(A,NX,NY,N,CSTEP,CLOW,CHIGH,IF)
DIMENSION A(N,N)
CALL ADVFLM(IF)
C
HX=10.2/FLCAT(NX)
HY=10.2/FLCAT(NY)

C
C      QX=J+.02
QY=0.02
DC=CSTEP
C3=CLCW
C4=CHIGH
C1=C4+DC
C2=C1+DC
C
CALL CB07A(A,DC,C1,C2,C3,C4,NX,NY,FX,HY,CX,CY,0.,1,N)
C
RETURN
END
C
C      * * * * * * * * * * * * * * * * * * * * *
C
C      SLROUTINE DB07A(F,CC,C1,C2,C3,C4,NX,NY,HX,HY,CX,CY,COSG,NG,DF)
DIMENSION F(IDF,ICDF)
COMMON /CCNT/ CX,CY,COSG,SING,DX,DY,CX,CY,X,Y,A,B,C,D,CCR,IHL,IKH
C
IHL=1
IKH=2
IFC=3
CEN=100.
DX = QX
DY = QY
CCSG = COSG
DX = HX
DY = HY
IX = NX -1
IY = NY -1
AA = CX * FLOAT(IX)
BB = CY * FLOAT(IY)
CX = 0.5 * DX
CY = 0.5 * DY
SING = SQRT(1.-COSG*COSG)
DELR = 1.0/DC
IF (CCSG) 101,102,102
101 QX = DX - DY*FLCAT(IY)*CCSG
102 IF (NG) 105,105,104
104 XC = CEN*(CX)
YC = CEN*(CY)
CALL QUACK(XD,YD,IHL)
XD = CEN*(CX+AA)
CALL QUACK(XD,YD,IKH)

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```

XC = CEN*(CX+A*B*C*CSG)
YC = CEN*(CY+B*SING)
CALL QUACK(XD,YD,IHK)
XC = CEN*(DX+B*E*CCSG)
CALL QUACK(XD,YD,IHK)
XC = CEN*(CX)
YC = CEN*(CY)
CALL QUACK(XD,YD,IHK)
IF (NCL-1) 105,105,106
106 CCNTINUE
IX=IX-1
IY=IY-1
DC 107 J=1,IY1
DC 108 I=1,IX1
X = FLCAT(I) * CX
Y = FLCAT(J) * CY
XC = CEN*(DX+X+Y*COSG)
YC = CEN*(CY+Y+SING)
108 CALL QUACK(XD,YC,IHC)
107 CCNTINUE
105 CCNTINUE
SMALL=1.E-6
DC 112 J=1,IY
DC 113 I=1,IX
C
C FOR REASONS WHICH WILL BECOME APPARENT, CCNTURE VALUES SHOULD NOT
C EXACTLY COINCIDE WITH FIELD VALUES. TO TAKE AN EXAMPLE, SUPPOSE
C FIELD VALUES ARE READ IN AS A=25.3 B=25.4 C=29.4 D=26.5 AND
C THE CCNTURES ARE REQUESTED BY PUNCHING C1=20.4 C2=38.4 DC=4.5 .
C THERE IS THEN THE DANGER THAT CCNTURE 29.4 MIGHT BE IDENTIFIED AS
C INTERSECTING SIDE BC (SEE LINE OF EXECUT-
C 302 IF ((B-CCN)*(C-CCN).LT.0) 303,304 ). .
C IF BY CHANCE WE GO TO 303, WE WILL GET TC 402,404,410,CR 412 AND
C GET OVERFLOW IN DIVIDING BY (C-B).
C AS ANOTHER EXAMPLE, A MALFUNCTION CAN OCCUR WHEN ONLY ONE OF
C THE 4 FIELD VALUES IS EQUAL TO A CCNTURE LEVEL. SUPPOSE A=25.3,
C B=29.4, C=30.0, D=26.4, CCNTURE=29.4 . CENTRE POINT E IS 27.78 AND
C CCNTURE SHOULD BE DRAWN FROM SIDE CD TO SEMIDIAGONAL CE TO CORNER
C B. HOWEVER, THE COMPUTER MIGHT FIND THAT BOTH AB AND BC ARE
C INTERSECTED BY THE CCNTURE. SINCE CD IS INTERSECTED THE LOGIC
C MUST ASSUME THAT AD IS ALSO INTERSECTED. A WILD LINE WILL BE
C DRAWN FROM A POINT WELL OUTSIDE THE GRID-BOX, LYING ON
C EXTRAPOLATED LINE AD.
C THE FOLLOWING TRANSFORMATION REDUCES ALL SUCH RISKS TO A

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C PRACTICAL ZERO. MODIFY THE 4 FIELD VALUES (Z) TO
C      Z(NEW) = Z(OLD) + CZ WHERE
C      CZ = Z * 10**5 + DELBIT   (FCR Z.GE.0)
C OR     CZ = Z * 10**5 - DELBIT   (FCR Z.LT.0) .
C THE DISCONTINUITY OF 2*DELBIT IS INTRODUCED IN CASE Z IS SMALL,
C BECAUSE THE TRANSFORMATION MIGHT THEN DEGENERATE TO AN IDENTITY
C MAPPING.
C
C A = F(I,J)
C A= 1.00001*A + SIGN(SMALL,A)
C B = F(I+1,J)
C B= 1.00001*B + SIGN(SMALL,B)
C C = F(I+1,J+1)
C C= 1.00001*C + SIGN(SMALL,C)
C D = F(I,J+1)
C D= 1.00001*D + SIGN(SMALL,D)
C X = DX * FLOAT(I-1)
C Y = DY * FLOAT(J-1)
C
C
C TC DETERMINE WHICH CCNTURES (IF ANY) ENTER THE BOX, APPLY INTEGRAL
C PARTS TEST. TC DO THIS CORRECTLY & OPERATE UPON SHIFTED FIELD
C VALUES AND RETURN TC PURE FIELD AFTER
C
C 103 DS = SIGN (DC,C1)
C EMCD = C1 - DS*AINTE (ABS (C1*DELR))
C JA = IFIX((A-EMOD)*DELR)
C JB = IFIX((B-EMOD)*DELR)
C JC = IFIX((C-EMOD)*DELR)
C JD = IFIX((D-EMOD)*DELR)
C J1 = MAX0(JA,JB,JC,JD)
C J3 = MINC(JA,JB,JC,JD)
C A1 = FLCAT(J1)
C A3 = FLOAT(J3)
C IF(J3.EQ.J1) GC TO 123
C
C JUMP ON IF NO CCNTURES EXIST, OTHERWISE FIND WHAT THEY ARE
C J3 = J3 + 1
C AJC1 = EMOD + AMAX1(C1-EMOD,A3*CC)
C AJC2 = EMOD + AMIN1(C2-EMOD,A1*CC) + 0.01*DC + SMALL
C CCN=AJC1
C
C BROKEN CCNTURE
41 CALL EXECUT(1)
CCN=CCN+DC

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```

C      IF(CON-AJC2)41,41,123
123  DS = SIGN (DC,C3)
      EMOD = C3 - DS*AIN1 (ABS (C3*DELR))
      JA = IFIX((A-EMOD)*CELR)
      JB = IFIX((B-EMOD)*CELR)
      JC = IFIX((C-EMOD)*CELR)
      JD = IFIX((D-EMOD)*CELR)
      J1 = MAX0(JA,JB,JC,JD)
      J2 = MIN0(JA,JB,JC,JD)
      A1 = FLCAT(J1)
      A3 = FLOAT(J3)
      IF(J3.EQ.J1) GC TO 113
C
C      JUMP OUT IF NO CONTCURS, OTHERWISE FIND THEM
      J3 = J3 + 1
      AJC3 = EMOD + AMAX1(C3-EMOD,A3*DC)
      AJC4 = EMOD + AMIN1(C4-EMOD,A1*DC) + 0.01*DC + SMALL
      CCN=AJC3
C
C      FULL CONTOUR
42   CALL EXECLT(2)
      CCN=CCN+EC
      IF(CON-AJC4)42,42,113
113  CCNCONTINUE
112  CONTINUE
      RETURN
      END
C
C      * * * * * * * * * * * * * * * * * * * * *
C
C      SUBROUTINE QUACK(PX,PY,IND)
      GC TO (2,3,1,5),IND
1     CALL PLOT(PX,42,PY)
      GC TO 5
2     IXS=IFIX(PX)
      IYS=IFIX(PY)
      GC TO 5
3     IXF=IFIX(PX)
      IYF=IFIX(PY)
      IF((IXS-IXF)**2+(IYS-IYF)**2)5,5,4
4     CALL VECTOR(IXS,IYS,IXF,IYF)
      IXS=IXF
      IYS=IYF
C
C      RETURN
      END
C
C      * * * * * * * * * * * * * * * * * * * * *
C
C      SUBROUTINE EXECUT(KLINK)
      CCMMCN /CCNT/ CX,CY,COSG,SING,DY,CX,CY,X,Y,A,B,C,D,CCN,IHL,IHK
      REAL I
      I=1.
      CEN = 0.25 * (A+B+C+D)
      PIP = CEN - CCN
      KZ = 16
      IF ((A-CCN)*(B-CCN).LT.0.) KZ = KZ - 8
      IF ((B-CCN)*(C-CCN).LT.0.) KZ = KZ - 4
      IF ((C-CCN)*(D-CCN).LT.0.) KZ = KZ - 2
      IF ((A-CCN)*PIP.LT.0.) KZ = KZ - 1
      GC TO (401,402,403,404,405,406,407,408,409,410,411,412,413,414,
1 415,416),KZ
401  CALL QUICK(X,Y+CY*(CCN-A)/(C-A),IHL)
      P = PIP/(CEN-A)
      CALL QUICK(X+CX*(I-P),Y+CY*(I-P),IHK)
      IF(KLINK.NE.2) GO TO 201
      CALL QUICK(X+DX*(CON-A)/(B-A),Y,IHK)
      CALL QUICK(X+DX*(CCN-D)/(C-D),Y+CY,IHL)
      P = PIP/(CEN-C)
      CALL QUICK(X+CX*(I+P),Y+CY*(I+P),IHK)
      IF(KLINK.NE.2) GO TO 202
      CALL QUICK(X+DX*(CON-B)/(C-B),IHK)
202  RETURN
402  CALL QUICK(X,Y+CY*(CON-A)/(C-A),IHL)
      P = PIP/(CEN-D)
      CALL QUICK(X+CX*(I-P),Y+CY*(I+P),IHK)
      IF(KLINK.NE.2) GO TO 203
      CALL QUICK(X+DX*(CCN-D)/(C-D),Y+CY,IHK)
      CALL QUICK(X+DX*(CON-A)/(B-A),Y,IHL)
      P = PIP/(CEN-B)
      CALL QUICK(X+CX*(I+P),Y+CY*(I-P),IHK)
      IF(KLINK.NE.2) GO TO 204
      CALL QUICK(X+DX,Y+DY*(CON-B)/(C-B),IHK)
204  RETURN
403  CALL QUICK(X+DX*(CCN-A)/(B-A),Y,IHL)
      P = PIP/(CEN-D)
      CALL QUICK(X+CX*(I-P),Y+CY*(I+P),IHK)
      IF(KLINK.NE.2) GO TO 205

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```

205 CALL QUICK(X+DX,Y+CY*(CON-B)/(C-B),IHK)
206 RETURN
404 CALL QUICK(X+DX*(CCN-A)/(B-A),Y,IHL)
P = PIP/(CEN-B)
CALL QUICK(X+CX*(I+P),Y+CY*(1-P),IHK)
IF(KLINK.NE.2) GO TO 206
CALL QUICK(X+DX,Y+CY*(CON-B)/(C-B),IHK)
206 RETURN
405 P = PIP/(CEN-D)
Q = PIP/(CEN-A)
GC TO (0501,0502),KLINK
0501 CALL QUICK(X+CX*(I-0.5*(P+Q)),Y+CY*(I+0.5*(P-Q)),IHL)
GC TO 0503
0502 CALL QUICK(X+DX*(CCN-D)/(C-C),Y+CY,IHL)
CALL QUICK(X+CX*(I-P),Y+CY*(I+P),IHK)
0503 CALL QUICK(X+CX*(I+C),Y+CY*(I-Q),IHK)
CALL QUICK(X+DX*(CON-A)/(B-A),Y,IHK)
RETURN
406 P = PIP/(CEN-C)
Q = PIP/(CEN-B)
GC TO (0601,0602),KLINK
0601 CALL QUICK(X+CX*(I+0.5*(P+Q)),Y+CY*(I+0.5*(P-Q)),IHL)
GC TO 0603
0602 CALL QUICK(X+DX*(CCN-C)/(C-C),Y+EY,IHL)
CALL QUICK(X+CX*(I+P),Y+CY*(I+P),IHK)
0603 CALL QUICK(X+CX*(I+C),Y+CY*(I-Q),IHK)
CALL QUICK(X+DX*(CON-A)/(B-A),Y,IHK)
RETURN
407 CALL QUICK(X,Y+CY*(CCN-A)/(C-A),IHL)
P = PIP/(CEN-A)
CALL QUICK(X+CX*(I-P),Y+CY*(I-P),IHK)
IF(KLINK.NE.2) GO TO 207
CALL QUICK(X+DX*(CCN-A)/(B-A),Y,IHK)
207 RETURN
408 CALL QUICK(X,Y+CY*(CCN-A)/(C-A),IHL)
P = PIP/(CEN-C)
CALL QUICK(X+CX*(I+P),Y+CY*(I+P),IHK)
IF(KLINK.NE.2) GO TO 208
CALL QUICK(X+DX*(CCN-A)/(B-A),Y,IHK)
208 RETURN
409 CALL QUICK(X+DX*(CCN-D)/(C-D),Y+CY,IHL)
P = PIP/(CEN-A)
CALL QUICK(X+CX*(I-P),Y+CY*(I-P),IHK)
IF(KLINK.NE.2) GO TO 209
CALL QUICK(X+DX,Y+DY*(CON-B)/(C-B),IHK)

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```

209 RETURN
410 CALL QUICK(X+DX*(CCN-D)/(C-D),Y+CY,IHL)
P = PIP/(CEN-C)
CALL QUICK(X+CX*(I+P),Y+CY*(I+P),IHK)
IF(KLINK.NE.2) GO TO 210
CALL QUICK(X+DX,Y+DY*(CON-B)/(C-B),IHK)
210 RETURN
411 P = PIP/(CEN-A)
Q = PIP/(CEN-B)
GC TO (1101,1102),KLINK
1101 CALL QUICK(X+CX*(I-0.5*(P-Q)),Y+CY*(I-0.5*(P+Q)),IHL)
GC TO 1103
1102 CALL QUICK(X,Y+DY*(CCN-A)/(D-A),IHL)
CALL QUICK(X+CX*(I-P),Y+CY*(I-P),IHK)
1103 CALL QUICK(X+CX*(I+C),Y+CY*(I-Q),IHK)
CALL QUICK(X+DX,Y+DY*(CON-B)/(C-B),IHK)
RETURN
412 P = PIP/(CEN-D)
Q = PIP/(CEN-C)
GC TO (1201,1202),KLINK
1201 CALL QUICK(X+CX*(I-0.5*(P-Q)),Y+CY*(I+0.5*(P+Q)),IHL)
GC TO 1203
1202 CALL QUICK(X,Y+CY*(CCN-A)/(C-A),IHL)
CALL QUICK(X+CX*(I-P),Y+CY*(I+P),IHK)
1203 CALL QUICK(X+CX*(I+C),Y+CY*(I+U),IHK)
CALL QUICK(X+DX,Y+DY*(CON-B)/(C-B),IHK)
RETURN
413 CALL QUICK(X,Y+DY*(CCN-A)/(D-A),IHL)
P = PIP/(CEN-B)
CALL QUICK(X+CX*(I+P),Y+CY*(I-P),IHK)
IF(KLINK.NE.2) GO TO 211
CALL QUICK(X+DX*(CCN-D)/(C-D),Y+CY,IHL)
211 RETURN
414 CALL QUICK(X,Y+CY*(CCN-A)/(C-A),IHL)
P = PIP/(CEN-D)
CALL QUICK(X+CX*(I-P),Y+CY*(I+P),IHK)
IF(KLINK.NE.2) GO TO 212
CALL QUICK(X+DX*(CCN-D)/(C-D),Y+CY,IHK)
212 RETURN
415 CCNTINUE
416 CCNTINUE
RETURN
END

```

C

* * * * *

```

C
C
C      SLROUTINE QUICK(XINC,YINC,IND)
C      COMMON /CCNT/ CX,CY,CCSG,SING,DY,CX,CY,X,Y,A,B,C,D,CON,IHL,IHK
C      PX=100.*((CX+XINC+YINC*COSG)
C      PY=100.*((CY+YINC*SING)
C      CALL QUACK(PX,PY,IND)
C      RETURN
C      END
C
C      * * * * *
C
C      SLROUTINE GRFGPV(N,X,Y)
C
C      GRAPHS OUT GROUP VELOCITY VALUES
C
C      COMMON /GRFF/ ATITLE(20), XMAX, XMIN, YMAX, YMINT, INDX, INDY, INC,
C      IICCT, ANSTR1, IF, XLIMIT, YLIMIT, SCALX, SCALY, XFACTR, YFACTR
C      DIMENSION X(1),Y(1)
C
C      DIMENSION TITLE(20)
C      DIMENSION TITLX(20)
C
C      REAL*8 ATITLE,TITLE,TITLX
C
C      DATA TITLE/8HPERIOD 1,8HN SECND,8HS ,8HGRP.VEL.,8H KM/SEC ,
C      18HGRAPH OF,8HGROUP VE,8HLUCITY (,8HKM/SEC) ,8HAGAINST ,8HPERIOD (,
C      28HSEC) FOR,8H SEISMCG,8HRAM 1 ,8H ,8HDATE ,8HTIME ,
C      38H ,8H ,8H /
C      DATA TITLX/8HPERIOD 1,8HN SECND,8HS ,8HGRP.VEL.,8H KM/SEC ,
C      18HGRAPH OF,8HGROUP VE,8HLUCITY (,8HKM/SEC) ,8HAGAINST ,8HPERIOD (,
C      28HSEC) FOR,8H SEISMCG,8HRAM 2 ,8H ,8HDATE ,8HTIME ,
C      38H ,8H ,8H /
C
C      DATA NH/0/
C
C
C      CALL DATIM(TITLE(16),TITLE(17))
C      CALL DATIM(TITLX(16),TITLX(17))
C
C      NH=NH+1
C      GC TO (1,3),NH
C

```

```

1      DC 2 I=1,16
2      ATITLE(I)=TITLE(I)
3      CCNTINUE
4      GC TO 5
C
3      DC 4 I=1,16
4      ATITLE(I)=TITLX(I)
5      CCNTINUE
NH=0
C
5      XMAX=0.0
XMIN=0.0
YMAX=0.0
YMINT=0.0
INDX=1
INCY=1
IND=1
IICCT=42
ANSTR1=2.0
IF=3
CALL CARGRF(X,Y,N)
C
RETURN
END
C
* * * * *
C
C      SLROUTINE COOLIN,XX,SIGN1)
C
C      A SPECIAL VERSION USING THE DOUBLE PRECISION CCOL PROGRAMME
C
C      N.B. ARRAY XX MUST HAVE TWICE AS MUCH STORAGE ALLOCATED AS USED
C
C
DIMENSION XX(1)
C
NX=2**N+1
NXD=NX/2
DC 1 I=1,NX
J=NX-I+1
JC=NXD-I*2+1
XX(JD)=XX(J)
XX(JD+1)=0.
C
C
C      CCNTINUE
1

```

```

C      CALL DCOLC(N,XX,SIGNI)
C
C      DC 2 J=1,NX
C      JC=J*2-1
C      XX(J)=XX(JD)
C      CCNTINUE
2
C      RETURN
C      END
C
C      * * * * *
C
C      SUBROUTINE DCLCL(N,XX,SIGNI)
C
C      THIS SUBROUTINE WAS PROGRAMMED BY I.MACLEOD, DEPT. OF
C      ENGINEERING PHYSICS,A.N.U. AND HAS BEEN BORROWED FROM C. MCCOWAN'S
C      CCOL AND IBM'S HARM.
C
C      DOUBLE PRECISION VERSION MODIFIED BY J.B.YOUNG FOR THE 360/75.
C
C
C      DIMENSION K(14),XX(1),NBIT(20),JAT(20)
C
C
C      DCLBLE PRECISION XX,RCOT2,PI2,CCN1,ARG,K,CSSQ1A,CSSQ2A,CSSQ3A,
C      1A0R,A0I,AIR,A1I,A2R,A2I,A3R,A3I,A4R,A4I,A5R,A5I,A6R,A6I,A7R,A7I,
C      2A8R,A8I,XK0WR,XK0WI,XK1WR,XK1WI,XK2WR,XK2WI,XK3WR,XK3WI,
C      3XK4WR,XK4WI,XK5WR,XK5WI,XK6WR,XK6WI,XK7WR,XK7WI,HCLCR,HCLDI
C
C      INTEGER OFFSET
C
C      DATA NX/0/
C
C      IF(NX.GT.0)GO TO 100
C      RCOT2=DSQRT(2.0D0)
C      PI2=8.0D0*COTAN(1.0D0)
C
100  NX=2**N
      NX2=NX+NX

```

```

      NX2LS1=NX2-1
      NX2LS2=NX2-2
      NXCN8=NX/8
      NXCN4=NXCN8+NXCNB
      NXCN2=NXCN4+NXCN4
      CCN1=PI2/DFLJAT(NX)
      IF(SIGNI.GT.0).CIGC TO 120
C
      DC 110 K=1,NX2LS1,2
      XX(K+1)=-XX(K+1)
      CCNTINUE
110
C
      120 DC 130 K=1,N
      JAT(K)=2**-(N-K)
      CCNTINUE
C
      LSTART=N-N/3*3+1
      IF(LSTART.EQ.1)GO TO 200
      IF(LSTART.EQ.2)GO TO 150
      LBLOK2=NXCN2
      L2BLOK=LBLOK2-1
C
      DC 140 K0=1,L2BLOK,2
      K1=K0+LBLOK2
      K2=K1+LBLOK2
      K3=K2+LBLOK2
      ACR=XX(K0)+XX(K2)
      A0I=XX(K0+1)+XX(K2+1)
      A1R=XX(K0)-XX(K2)
      A1I=XX(K0+1)-XX(K2+1)
      A2R=XX(K1)+XX(K3)
      A2I=XX(K1+1)+XX(K3+1)
      A3R=XX(K1)-XX(K3)
      A3I=XX(K1+1)-XX(K3+1)
      XX(K0)=A0R+A2R
      XX(K0+1)=A0I+A2I
      XX(K1)=A0R-A2R
      XX(K1+1)=A0I-A2I
      XX(K2)=A1R-A3I
      XX(K2+1)=A1I+A3R
      XX(K3)=A1R+A3I
      XX(K3+1)=A1I-A3R
140  CCNTINUE
      GC TO 200
C

```

```

150  LBL0K2=NX
      L2BLOK=LBL0K2-1
      DO 160 K0=1,L2BLOK,2
      K1=K0+LBL0K2
      AIR=XX(K1)
      AII=XX(K1+1)
      XX(K1)=XX(K0)-AIR
      XX(K1+1)=XX(K0+1)-AII
      XX(K0)=XX(K0)+AIR
      XX(K0+1)=XX(K0+1)+AII
160  CCNTINUE
C
C
200  DC 300 M=LSTART,N,3
      LBL0K2=NX/2*(M+1)
      L2BLOK=LBL0K2-1
      LBLCK1=L2BLOK-1
      LBLCK8=LBLCK2*8
      LBLAST=NX2-LBLCK8+1
C
      DC 210 K=4,N
      NBIT(K)=0
210  CCNTINUE
C
      NW=0
C
      DC 290 OFFSET=1,LBLAST,LBL0K8
      IF(OFFSET.EQ.1)GO TO 220
      ARG=CCN1*DFLOAT(NW)
      W(1)=CCCS(ARG)
      W(2)=DSIN(ARG)
      CSSQA=W(1)*W(1)
      W(3)=CSSQA+CSSQA-1.0D0
      W(4)=W(1)*W(2)
      W(5)=W(4)+W(4)
      W(6)=W(3)*W(1)-W(4)*W(2)
      W(7)=W(4)*W(1)+W(3)*W(2)
      CSSQ2A=W(3)*W(3)
      W(8)=CSSQ2A+CSSQ2A-1.0D0
      W(9)=W(4)*W(3)
      W(10)=W(8)+W(8)
      W(11)=W(7)*W(1)-W(9)*W(2)
      W(12)=W(8)*W(1)+W(7)*W(2)
      CSSQ3A=W(5)*W(5)
      W(13)=CSSQ3A+CSSQ3A-1.0D0
      W(14)=W(6)*W(5)

      W(12)=W(6)*W(5)
      W(12)=W(12)+W(12)
      W(13)=W(7)*W(5)-W(8)*W(6)
      W(14)=W(8)*W(5)+W(7)*W(6)
220  LBL0K0=OFFSET+LBLCK1
C
      DC 260 K0=OFFSET,LBL0KJ,2
      K1=K0+LBL0K2
      K2=K1+LBL0K2
      K3=K2+LBL0K2
      K4=K3+LBL0K2
      K5=K4+LBL0K2
      K6=K5+LBL0K2
      K7=K6+LBL0K2
      XK0WR=XX(K0)
      XK0WI=XX(K0+1)
      IF(OFFSET.NE.1) GO TO 240
      XK1WR=XX(K1)
      XK1WI=XX(K1+1)
      XK2WR=XX(K2)
      XK2WI=XX(K2+1)
      XK3WR=XX(K3)
      XK3WI=XX(K3+1)
      XK4WR=XX(K4)
      XK4WI=XX(K4+1)
      XK5WR=XX(K5)
      XK5WI=XX(K5+1)
      XK6WR=XX(K6)
      XK6WI=XX(K6+1)
      XK7WR=XX(K7)
      XK7WI=XX(K7+1)
      GC TO 250
240  XK1WR=XX(K1)*W(1)-XX(K1+1)*W(2)
      XK1WI=XX(K1)*W(2)+XX(K1+1)*W(1)
      XK2WR=XX(K2)*W(3)-XX(K2+1)*W(4)
      XK2WI=XX(K2)*W(4)+XX(K2+1)*W(3)
      XK3WR=XX(K3)*W(5)-XX(K3+1)*W(6)
      XK3WI=XX(K3)*W(6)+XX(K3+1)*W(5)
      XK4WR=XX(K4)*W(7)-XX(K4+1)*W(8)
      XK4WI=XX(K4)*W(8)+XX(K4+1)*W(7)
      XK5WR=XX(K5)*W(9)-XX(K5+1)*W(10)
      XK5WI=XX(K5)*W(10)+XX(K5+1)*W(9)
      XK6WR=XX(K6)*W(11)-XX(K6+1)*W(12)
      XK6WI=XX(K6)*W(12)+XX(K6+1)*W(11)
      XK7WR=XX(K7)*W(13)-XX(K7+1)*W(14)

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```

      XK7WI=XX(K7)*w(14)+XX(K7+1)*w(13)
250   ACR=XK0WR+XK4WR
      ACI=XK3WI+XK4WI
      A1R=XK1WR+XK5wR
      A1I=XK1WI+XK5WI
      A2R=XK2WR+XK6wR
      A2I=XK2WI+XK6WI
      A3R=XK3WR+XK7wR
      A3I=XK3WI+XK7WI
      A4R=A0R+A2R
      A4I=A0I+A2I
      A5R=A0R-A2R
      A5I=A0I-A2I
      A6R=A1R+A3R
      A6I=A1I+A3I
      A7R=A3I-A1I
      A7I=A1R-A3R
      XX(K0)=A4R+A6R
      XX(K0+1)=A4I+A6I
      XX(K1)=A4R-A6R
      XX(K1+1)=A4I-A6I
      XX(K2)=A5R+A7R
      XX(K2+1)=A5I+A7I
      XX(K3)=A5R-A7R
      XX(K3+1)=A5I-A7I
      ACR=XK0WR-XK4WR
      ACI=XK0WI-XK4WI
      A6R=XK1WR-XK5wR
      A6I=XK1WI-XK5WI
      A1R=A8R-A8I
      A1I=A8R+A8I
      A2R=XK6WI-XK2WI
      A2I=XK2WR-XK6wR
      A8R=XK3WR-XK7wR
      A8I=XK3WI-XK7WI
      A3R=AER-A3I
      A3I=A8R+A8I
      A4R=A0R+A2R
      A4I=A0I+A2I
      A5R=ACR-A2R
      A5I=ACI-A2I
      A6R=(A1R-A3I)/FOOT2
      A6I=(A1I+A3I)/FOOT2
      A7R=(A3R-A1I)/FOOT2
      A7I=(A3I+A1R)/FOOT2

```

```

      XX(K4)=A4R+A6R
      XX(K4+1)=A4I+A6I
      XX(K5)=A4R-A6R
      XX(K5+1)=A4I-A6I
      XX(K6)=A5R+A7R
      XX(K6+1)=A5I+A7I
      XX(K7)=A5R-A7R
      XX(K7+1)=A5I-A7I
260   CCNTINUE
C
      DC 280 K=4,N
      IF(NBIT(K).NE.0)GO TO 270
      NBIT(K)=1
      NW=NW+JNT(K)
      GO TO 290
270   NBIT(K)=0
      NW=NW-JNT(K)
280   CCNTINUE
C
      290  CCNTINUE
      300  CCNTINUE
C
      NW=0
C
      DC 310 K=1,N
      JNT(K)=JNT(K)+JNT(K)
      NBIT(K)=0
310   CCNTINUE
C
      K=0
      IF(NW.LE.K1GO TO 320
      HCLDR=XX(NW+1)
      HCLDI=XX(NW+2)
      XX(NW+1)=XX(1)
      XX(NW+2)=XX(2)
      XX(1)=HOLDI
      XX(2)=HOLDR
C
      320  DC 340 M=1,N
      IF(NBIT(M).NE.0)GO TO 330
      NBIT(M)=1
      NW=NW+JNT(M)
      GO TO 350
330   NBIT(M)=0

```

```

      NW=NW-JNT(M)
340  CCNTINUE
C
350  DC 39C K=2,NX2LS2,2
      IF(NW.LE.K1G3) TO 360
      HCLDR=XX(NW+1)
      HCLDI=XX(NW+2)
      XX(NW+1)=XX(K+1)
      XX(NW+2)=XX(K+2)
      XX(K+1)=HCLDR
      XX(K+2)=HLDI
C
360  DC 380 M=1,N
      IF(NBIT(M).NE.0)GO TO 370
      NBIT(M)=1
      NW=NW-JNT(M)
      GC TO 390
370  NBIT(M)=0
      NW=NW-JNT(M)
380  CCNTINUE
C
390  CCNTINUE
C
      IF(SIGNI.GT.0.0)GO TO 420
C
400  DC 410 K=1,NX2LS1,2
      XX(K+1)=-XX(K+1)
410  CCNTINUE
C
C
420  RETURN
END
C
C
C
* * * * * * * * * * * * * * * * * * * * * * * * * * *
C          GENERAL USER SUBROUTINE TIMER AND CHECK
C
C
C
C      FROM THE CALL - CALL TIMER
C      THE ELAPSED TIME AND CPU TIMES FROM THE LAST CALL TIMER ARE PRINTED OUT
C      THE FIRST CALL SETS UP TIMER
C
C

```

```

C      FROM THE CALL - CALL CHECK(8,...)
C      TIMES ARE PRINTED OUT AS FOR CALL TIMER BUT WHEN THE CPUAV
C      IS LARGER THAN THE CPU TIME LEFT CONTROL IS RETURNED TO
C      STATEMENT NUMBER .... IN THE CALLING PROGRAM
C
C
C      SUBROUTINE TIMER
C      DATA DIFF/0./
C      IND=1
C      IF(DIFF) 2,1,2
C
C      ENTRY CHECK(*)
C      IND=2
C      IF(DIFF) 2,1,2
C
C      1      CALL CLOCK(DIFF)
C              DIFF=DIFF*60.
C              CALL TXLIBR(CTIME)
C              CTIME=CTIME*0.01
C              CFLAV=CTIME*0.2
C              RETURN
C
C      2      CALL CLOCK(TIME)
C              TIME=TIME*60.
C              DIFF=TIME-DIFF
C              CALL TXLIBR(CPU)
C              CPU=CPU*0.01
C              CTIME=CTIME-CPU
C              CFLAV=CPUAV*0.8+CTIME*0.2
C              PRINT 3, DIFF,CTIME,CPU
C
C      3      FCRMAT(41HFROM LAST TIMER CALL  1) TIME ELAPSED =,F8.3,29H SECON
C              1DS  2) CPU TIME USED =,F8.3,29H SECONDS  3) CPU TIME LEFT =,F8.3
C              2,8H SECONDS/)
C              DIFF=TIME
C              CTIME=CPU
C
C              GO TO (6,4),IND
C
C      4      IF(CPUAV-CPU)6,6,5
C
C      5      RETURN 1
C
C      6      RETURN
END
C
* * * * * * * * * * * * * * * * * * * * * * * * * * *

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DOCUMENT CONTROL SHEET

Overall security classification of sheet Unclassified.....

(As far as possible this sheet should contain only unclassified information. If it is necessary to enter classified information, the box concerned must be marked to indicate the classification eg (R), (C) or (S)).

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Abstract The program described determines the phase velocity of a dispersed seismic surface wave as a function of period between a pair of stations from their digitized seismograms. The cross-multiplication technique of Bloch and Hales is used to compute the phase velocity curve.			

